Final Exam, Control Systems, 110-1 (2021)姓名:Date: Friday, January 7, 2022. Time: 9:10am-11:10am.學號:Closed books, closed notes, no calculators.条級:Only pens and erasers are allowed.

[100%] Write down proper description for the following problems.

(1) (20%=5%+5%+10%), (By B07901004 陳恩庭)
For the characteristic equation:

1 + K
K
(s + 5) (s + 7)

(a) Draw the real-axis segments of the corresponding root locus.
(b) Sketch the asymptotes of the locus for K → ∞.
(c) Sketch the locus.

Solution:

(a) The characteristic function has five poles: s = 0, 0, 0, -5, -7 and no zeros. For Rule 2, the locus is on the real axis to the left of an odd number of poles and zeros.

That is, at -5 < s < 0 and s < -7, as the two red lines shown in the following figure.



(b)
For Rule 3, n = 5, m = 0.
Thus,

$$\phi_{l} = \frac{180^{\circ} + 360^{\circ} (l - 1)}{n - m} = \frac{180^{\circ} + 360^{\circ} (l - 1)}{5}$$

$$= \pm 36^{\circ}, \pm 108^{\circ}, 180^{\circ},$$

$$\alpha = \frac{\sum p_{i} - \sum z_{i}}{n - m} = \frac{0 + 0 + 0 + (-5) + (-7) - 0}{5} = -2.4$$

There are five asymptotes centered at s = -2.4 and at the angles $\pm 36^{\circ}$, $\pm 108^{\circ}$, 180° . As the five red lines shown in the following figure.



(c) For Rule 4, the branches depart from the pole at s = 0 (multiplicity = 3) at the angles: $q \phi_{l,dep} = \sum \psi_i - \sum_{i \neq l,dep} \phi_i - 180^o - 360^o(l-1)$ $3 \phi_{l,dep} = -180^o - 360^o(l-1)$ $\phi_{l,dep} = \pm 60^o, 180^o$ Another branch departs from s = -5 (multiplicity = 1) at the angle: $\phi_{l,dep} = 3 \times 180^o - 180^o - 360^o(l-1)$ $= 0^o,$ The other branch departs from s = -7 (multiplicity = 1) at the angle:

$$\phi_{l,dep} = 4 \times 180^{\circ} - 180^{\circ} - 360^{\circ}(l-1)$$

= 180°,

The locus is shown in the following figure.

-30

-20

Root Locus

-10

0

Real Axis (seconds⁻¹)

10

20

(2) (20%=4%+4%+4%+8%), (By B08901120 鍾銀香)

Consider the following four functions:

$$D_1(s) = (s+10)$$

 $D_2(s) = (s+100)$
 $D_3(s) = (s^2+0.8s+3600)$
 $D_4(s) = (s+60)^2$

(a) Please sketch the Bode plots of $D_1(s)$ and $D_2(s)$.

ode plot of
$$D_a(s) = \frac{D_1(s)}{D_2(s)}$$

(b) Please sketch the Bode plot of

Is it a lead or lad compensator? Justify your answer.

$$D_b(s) = \frac{D_2(s)}{D_1(s)}$$

(c) Please sketch the Bode plot of

Is it a lead or lad compensator? Justify your answer.

(d) Please plot the Bode plots of $D_3(s) = D_4(s)$ and

$$D_c(s) = \frac{D_3(s)}{D_4(s)}$$

What is the special name for the $D_c(s)$ compensator?

(a) (b)

The Bode plots of D1(s), D2(s), Da(s) are shown in the following plots. Da(s) is a lead compensator because it can increase phase margin.



(a) (c)

The Bode plots of D1(s), D2(s), Db(s) are shown in the following plots. Da(s) is a lag compensator because it can decrease phase margin.



(d)

The Bode plots of D3(s), D4(s), Dc(s) are shown in the following plots. Dc(s) is a notch compensator because it is cable of filtering one specific frequency of oscillation, i.e., at 60 rad/sec in this case.



(3) (20%=5%+5%+10%), (By B08901111 簡宏哲)

Consider the following block diagram:



where

$$G(s) = \frac{10}{s (s^2 + 15s + 10)}$$

(a) We design a lead compensator as follows:

$$D_c(s) = K \frac{s+z}{s+5z}, K > 0.$$

Please find the minimum value of K, such that the velocity constant is more than (or equal) 10, i.e., $K_v \ge 10$.

(b) We design a lag compensator as follows:

$$D_c(s) = K \frac{s+5p}{s+p}, K > 0.$$

Please find the minimum value of K, such that the velocity constant is more than (or equal) 10, i.e., $K_v \ge 10$.

(c) We design a PD-Type compensator as follows:

$$D_c(s) = K (1 + As), A > 1, K > 0$$

Please show that the closed-loop system is always stable using Routh's Stability Criterion.

(a)

$$K_{v} = \lim_{s \to 0} s \ D_{c}(s) \ G(s)$$

=
$$\lim_{s \to 0} s \quad K \frac{s+z}{s+5z} \quad \frac{10}{s \ (s^{2}+15s+10)}$$

=
$$\frac{K}{5} \geq 10$$

$$\Rightarrow K \geq 50$$

So, the minimum value of K is 50.

(b)

$$K_{v} = \lim_{s \to 0} s \ D_{c}(s) \ G(s)$$

=
$$\lim_{s \to 0} s \quad K \frac{s + 5p}{s + p} \quad \frac{10}{s (s^{2} + 15s + 10)}$$

=
$$5K \geq 10$$

$$\Rightarrow K \geq 2$$

So, the minimum value of K is 2.

(c)

s: 1:

The characteristic equation is:

$$1 + D_{c}(s) G(s) = 0$$

$$\Rightarrow 1 + K (1 + As) \frac{10}{s (s^{2} + 15s + 10)} = 0$$

$$\Rightarrow s^{3} + 15s^{2} + (10 + 10AK) s + 10K = 0$$

Routh's Stability Criterion:
s^{3}: 1 10 + 10 A K
s^{2}: 15 10 K
s: a1 0
1: a2 0

where

$$a1 = -\frac{1}{15} \begin{vmatrix} 1 & 10 + 10AK \\ 15 & 10K \end{vmatrix} = \frac{1}{15} (150 + K(150A - 10)),$$
$$a2 = -\frac{1}{a1} \begin{vmatrix} 15 & 10K \\ a1 & 0 \end{vmatrix} = 10K.$$

Because K > 0 and A > 1, then, the four numbers: 1, 15, a1, and a2 are all > 0. So, the closed-loop system is stable. (4) (20%=10%+10%), (By B08901095 邱泓翔)

Consider the following two transfer functions:

$$G_1(s) = \frac{s+1}{(s-1)^2}$$
 $G_2(s) = \frac{s-1}{(s+1)^2}$

The Bode plot, Nyquist plot, root locus plot of these two transfer functions are shown in the following plots. Please find the detailed answers for the following two questions.

- (a) For G1(s), please use the above plots to determine the ranges of K in K > 0 for which KG1(s) is STABLE or UNSTABLE.
- (b) For G2(s), please use the above plots to determine the ranges of K in K > 0 for which KG2(s) is STABLE or UNSTABLE.





(a) For Gl(s)

The curve is the case when K = 1 and it crosses the real axis at -0.5 and 1. From the Nyquist plot we can observe that

$(1) - \frac{1}{\kappa} < -\frac{1}{2}$

In this case, we have 0 < K < 2, N = 0, P = 2, so Z = 2. That is, when 0 < K < 2, the system is unstable and there are two closed-loop roots in RHP.

$$(2) - \frac{1}{2} < -\frac{1}{K} < 0$$

In this case, we have K > 2, N = -2, P = 2, so Z = 0. That is, when K > 2, the system is stable and there are no closed-loop roots in RHP.

(3) $0 < -\frac{1}{\kappa} < 1$

In this case, we have K < -1, N = -1, P = 2, so Z = 1. That is, when K < -1, the system is unstable and there is one closed-loop root in RHP.

(4) $1 < -\frac{1}{\kappa}$

In this case, we have -1 < K < 0, N = 0, P = 2, so Z = 2. That is, when -1 < K < 0, the system is unstable and there are two closed-loop roots in RHP. (e) We can use Routh's criterion to verify that the closed-loop system of KG_1 is stable if K > 2. The steps are shown in Figure 5.

Closed - loop transfer function: $\frac{KG_{1}(s)}{1+KG_{1}(s)} = \frac{K\frac{s+1}{(s-1)^{2}}}{1+K\frac{s+1}{(s-1)^{2}}} = \frac{K(s+1)}{s^{2}-(2-K)s+(1+K)}$ Characteristic equation: $s^{2}-(2-K)s+(1+K)=0$ Using Rowth's criterion: $s^{2}: 1$ [+K s': -2+K = 0 $S^{0}: 1+K$ For stability, -2+K>0 and 1+K>0. That 13, K>2 and K>-1. $\therefore K>2 = 3$ stable, otherwise = unstable. Figure 5. The steps of using Rowth's criterion to verify the condition for stability of $KG_{1}(s)$.

(b) For *G2(s)*

The curve is the case when K = 1 and it crosses the real axis at 0.5 and -1. From the Nyquist plot we can observe that

(1) 0 < K < 1

In this case, we have N = 0, P = 0, so Z = 0.

That is, the system is stable and there are no closed-loop roots in RHP.

(2) K > 1

In this case, we have N = 1, P = 0, so Z = 1.

That is, the system is unstable and there is one closed-loop root in RHP.

(3) K < -2

In this case, N = 2, P = 0, so Z = 2.

That is, the system is unstable and there are two closed-loop roots in RHP.

(4) - 2 < K < 0

In this case, we have N = 0, P = 0, so Z = 0.

That is, the system is stable and there are no closed-loop roots in RHP.

(e) We can use Routh's criterion to verify that the closed-loop system of KG_2 is stable if -2 < K < 1. The steps are shown in Figure 10.

Closed -loop transfer function: $\frac{K6_{1}(5)}{1+KG_{2}(5)} = \frac{K\frac{5-1}{(5+1)^{2}}}{1+K\frac{5-1}{(5+1)^{2}}} = \frac{K(5-1)}{s^{3}+(2+K)5+(1-K)}$ Characteristic equation: $5^{2}+(2+K)5+(1-K)=0$ Using Routh's criterion: $5^{2}+(2+K)5+(1-K)=0$ Using Routh's criterion: $s^{2} \cdot 1 - K$, $s^{1}: 2+K - 0$ $s^{0}: (-K)$ For stability, 2+K>0 and 1-K>0. That i^{3} , -2<K<1. $\therefore -2<K<1 = 3$ stable, otherwise = unstable Figure 10. The steps of using Routh's criterion to verify the condition for stability of $KG_{2}(s)$.



(a)

For
$$K_v = 5$$
, we have $K_v = \lim_{s \to 0} s K G(s) = K$.

Therefore, K = 5.

From the Bode plots, we can roughly identify the phase margin for the case of K=5 is about 5 degrees at w = 2 rad/sec.

Determine a phase lead = 40 + 10 + 5 = 55.

Looking at the plot of Max Phase Lead and $1/\alpha$,

we choose $1/\alpha = 10$ and a zero at $w\sqrt{\alpha} = 2 \times \sqrt{0.1} = 0.6$ or around z=1. Pick the pole at $(1/\alpha)^*$ zero = $10^*1 = 10$.

So, design the lead compensator as follows:

$$D_c(s) = \frac{\frac{s}{1} + 1}{\frac{s}{10} + 1} = 10 \frac{s+1}{s+10}$$

Or, aggressively, we can choose $1/\alpha=20$ to have more phase margin. The new lead compensator is as follows:

$$D_c(s) = \frac{\frac{s}{1} + 1}{\frac{s}{20} + 1} = 20 \frac{s+1}{s+20}$$

(b)

Looking at the Bode plots, to have Phase Margin = 50, it is at about w = 0.6 rad/sec. Also, the Gain at this frequency is about 15dB or we can use Gain = 20dB. The gain is selected as K = 5/10 = 0.5 to reduce the gain.

Hence, choose the zero at 0.6/10 = 0.06 rad/sec. For $K_v = 5$ $K_v = \lim_{s \to 0} s K D_c(s) G(s)$ $= \lim_{s \to 0} s K \alpha \frac{T_{I} s + 1}{\alpha T_{I} s + 1} \frac{1}{s (s+1) (\frac{s}{5} + 1)}$ $5 = K \alpha$ $\alpha = \frac{5}{0.5} = 10$

So,

Then, choose the pole at $(1/\alpha)^*$ zero = $0.1^*0.06 = 0.006$. So, design the lag compensator as follows:

$$D_c(s) = 10 \frac{\frac{s}{0.06} + 1}{\frac{s}{0.006} + 1} = 1 \frac{s + 0.06}{s + 0.006}$$

