

Spring 2015

信號與系統
Signals and Systems

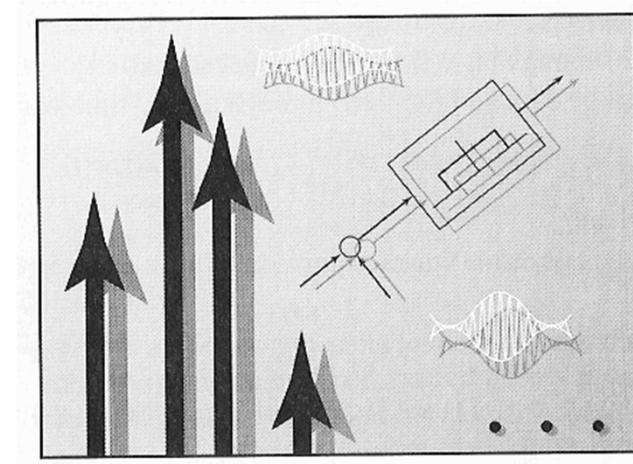
Chapter SS-8
Communication Systems

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NTU-EE

Feb15 – Jun15

Figures and images used in these lecture notes are adopted from
“Signals & Systems” by Alan V. Oppenheim and Alan S. Willsky, 1997



Introduction

[\(Chap 1\)](#)

LTI & Convolution

[\(Chap 2\)](#)

Bounded/Convergent

Periodic

FS

[\(Chap 3\)](#)

CT
DT

Aperiodic

FT

CT
DT

[\(Chap 4\)](#)
[\(Chap 5\)](#)

Unbounded/Non-convergent

LT

CT [\(Chap 9\)](#)

zT

DT [\(Chap 10\)](#)

Time-Frequency [\(Chap 6\)](#)

CT-DT

[\(Chap 7\)](#)

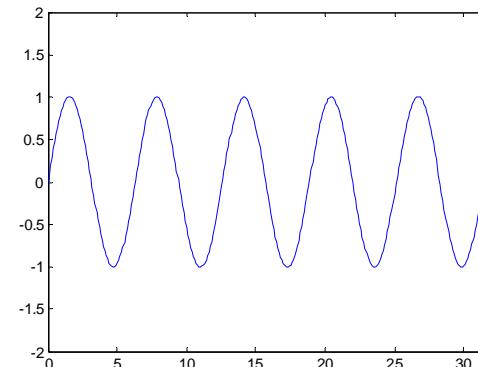
Communication [\(Chap 8\)](#)

Control

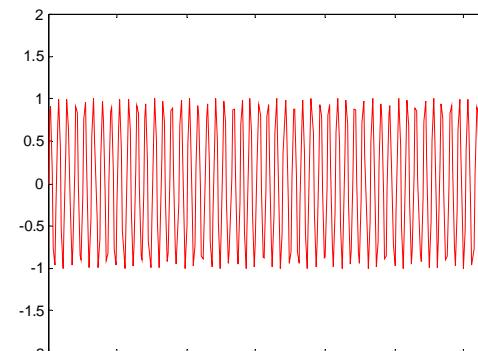
[\(Chap 11\)](#)

Digital
Signal
Processing
[\(dsp-8\)](#)

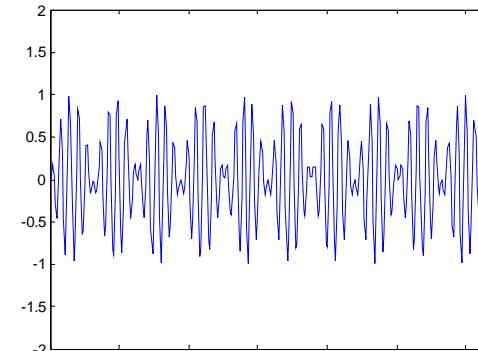
Introduction



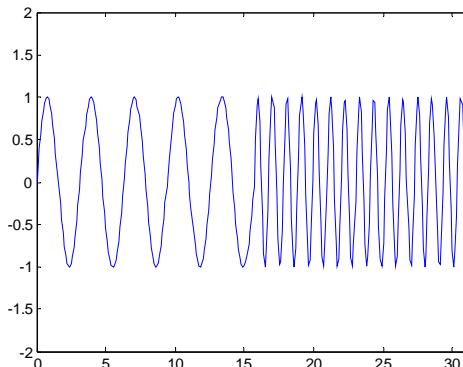
$$x(t) = \sin(1 t)$$



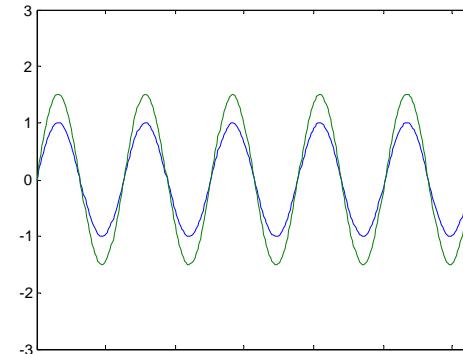
$$c(t) = \sin(10 t)$$



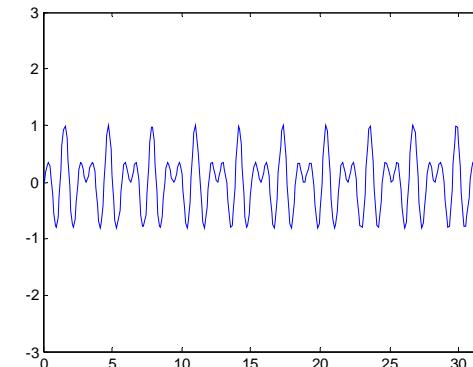
$$\sin(10 t) \cdot \sin(1 t)$$



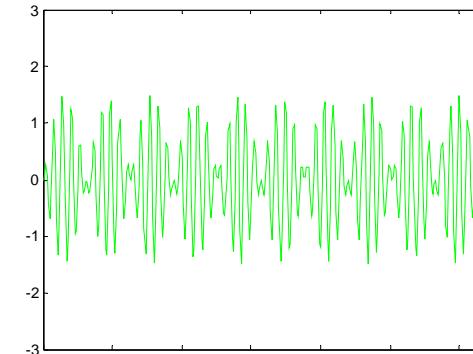
$$\sin(2 t) + \sin(6 t)$$



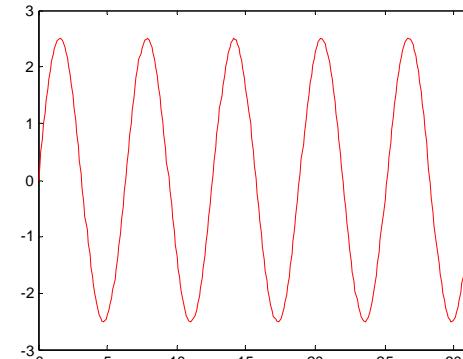
$$1 \sin(t) + 1.5 \sin(t)$$



$$z_1 = 1 \cdot \sin(t) \cdot \sin(5 t)$$



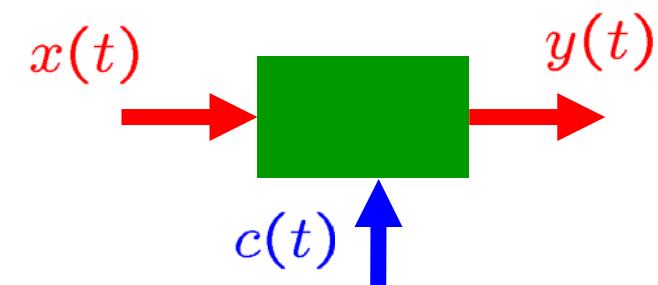
$$z_2 = 1.5 \cdot \sin(t) \cdot \sin(10 t)$$



$$z_1 + z_2$$

■ Modulation & Demodulation:

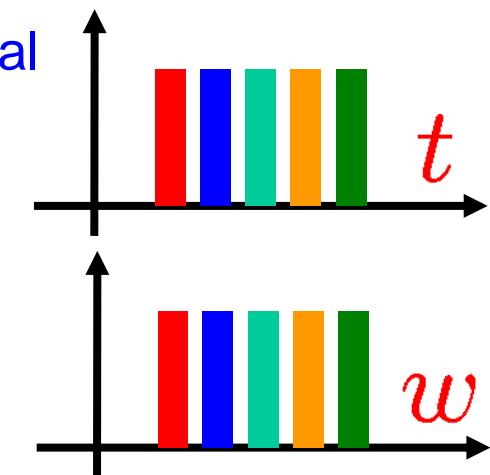
- M: Embedding an information-bearing signal into a second signal
- D: Extracting the information-bearing signal
- Methods:
 - > Amplitude Modulation (AM)
 - > Frequency Modulation (FM)



$$c(t) = A(t) \cos(w(t) \cdot t + \theta(t))$$

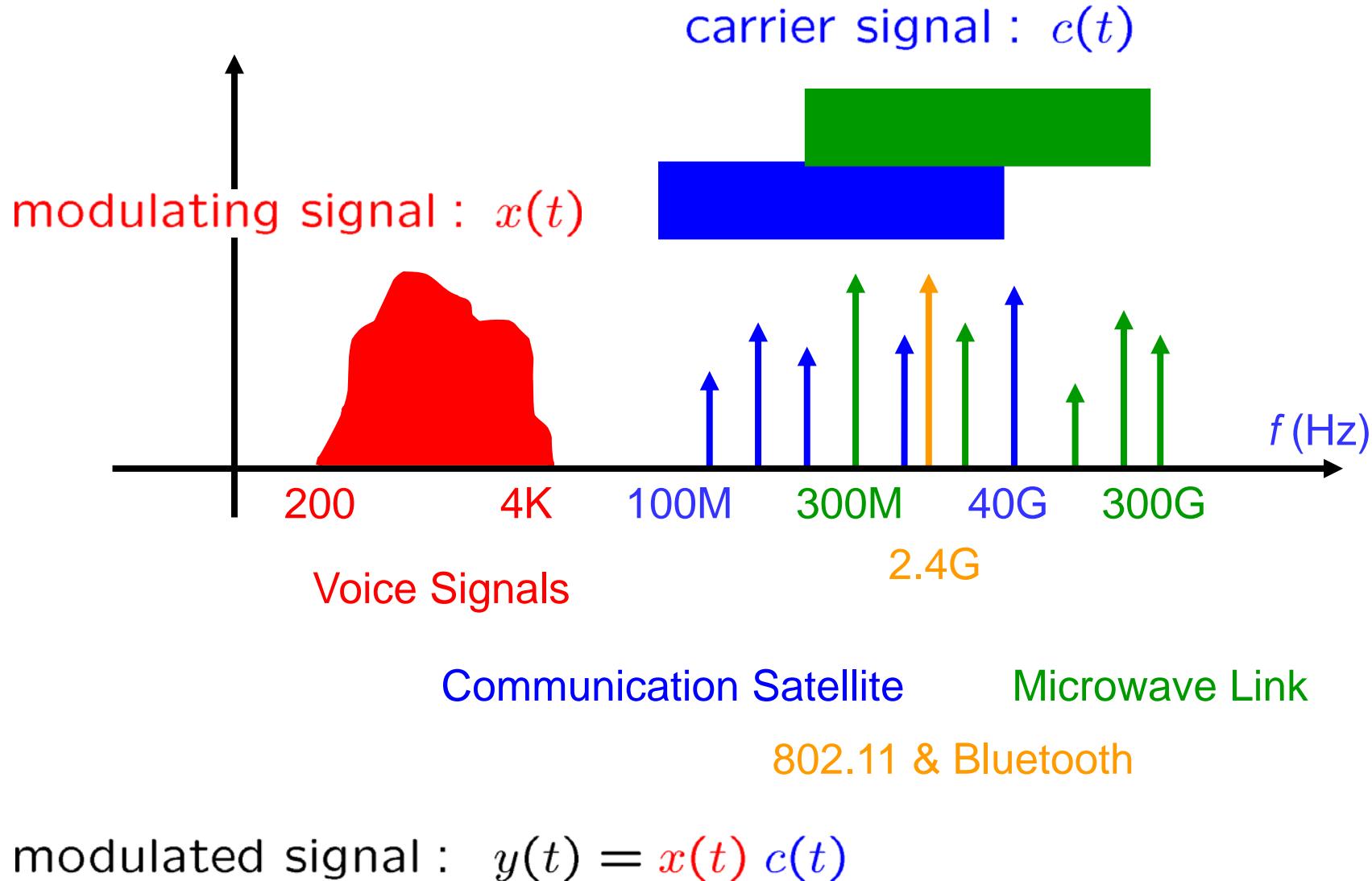
■ Multiplexing & Demultiplexing:

- Simultaneous transmission of more than one signal with overlapping spectra over the same channel
- Methods:
 - > Time-Division Multiplexing (TDM)
 - > Frequency-Division Multiplexing (FDM)



- Complex Exponential & Sinusoidal
Amplitude Modulation & Demodulation
- Frequency-Division Multiplexing
- Single-Sideband Sinusoidal Amplitude Modulation
- Amplitude Modulation with a Pulse-Train Carrier
 - » Time-Division Multiplexing
- Pulse-Amplitude Modulation
- Sinusoidal Frequency Modulation
- Discrete-Time Modulation

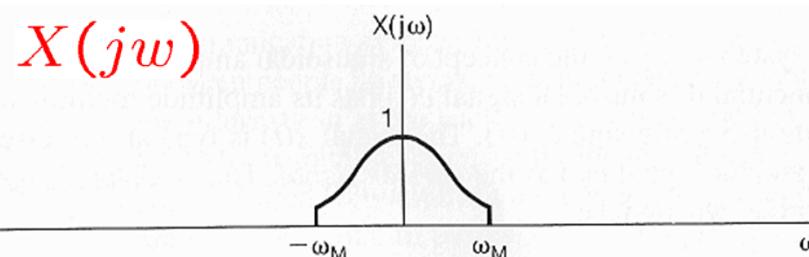
■ Signal Frequency Characteristics:



■ AM with a Complex Exponential Carrier:

$$x(t) \xrightarrow{\times} y(t)$$

$$e^{j(w_c t + \theta_c)}$$



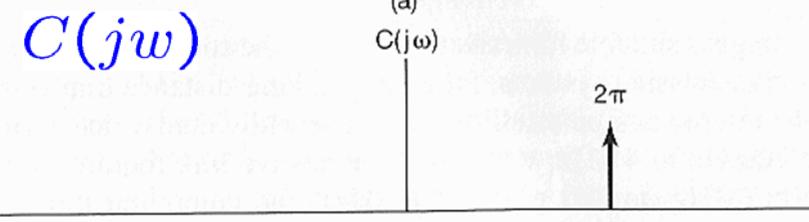
$$X(j\omega)$$

w_c : carrier frequency

$$c(t) = e^{j(w_c t + \theta_c)}$$

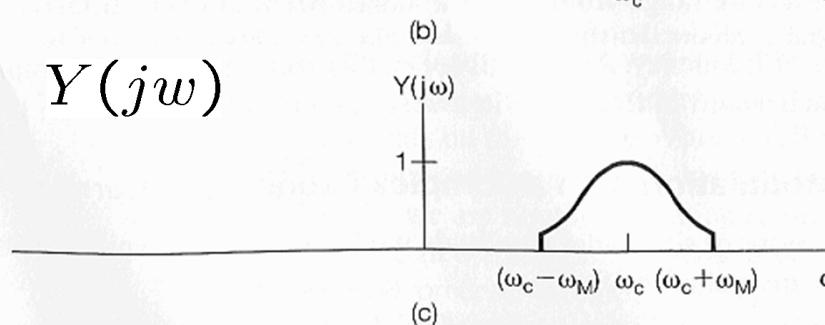
$$y(t) = x(t) c(t) = x(t) e^{j w_c t}$$

$$\theta_c = 0$$



$$C(j\omega) = 2\pi \delta(\omega - \omega_c)$$

2π



$$Y(j\omega) = X(j(\omega - \omega_c))$$

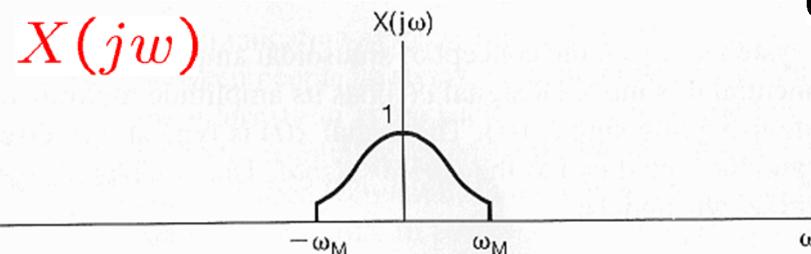
$$Y(j\omega) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(j\theta) C(j(\omega - \theta)) d\theta$$

■ AM with a Complex Exponential Carrier:

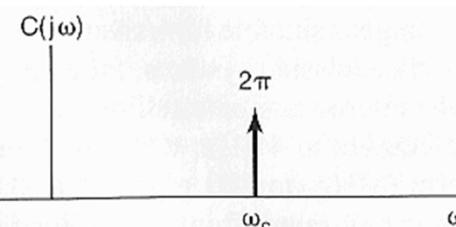
$$x(t) \rightarrow \textcircled{x} \rightarrow y(t)$$

$$c_m(t) = e^{j(w_c t + \theta_c)}$$

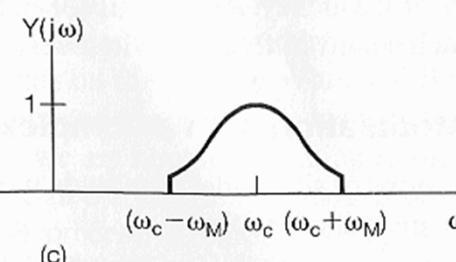
(a)



$$C_m(jw)$$



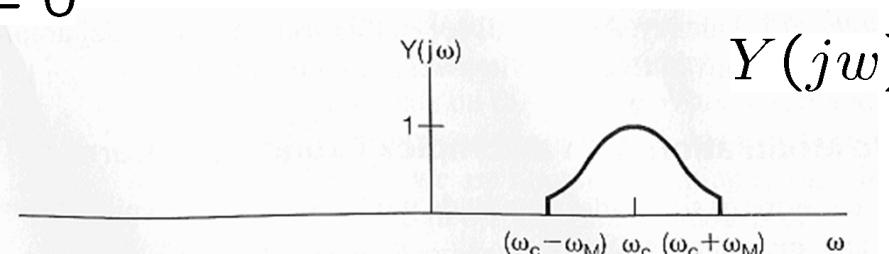
$$Y(jw)$$



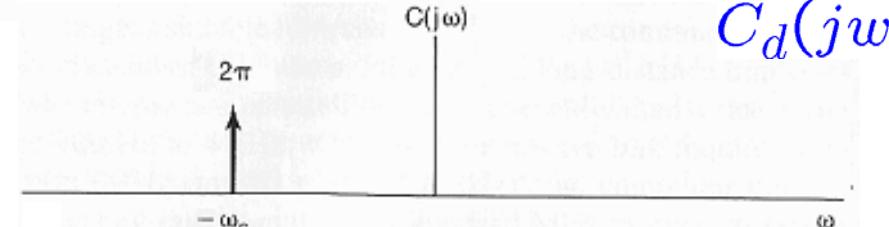
$$y(t) \rightarrow \textcircled{x} \rightarrow w(t)$$

$$c_d(t) = e^{-j(w_c t + \theta_c)}$$

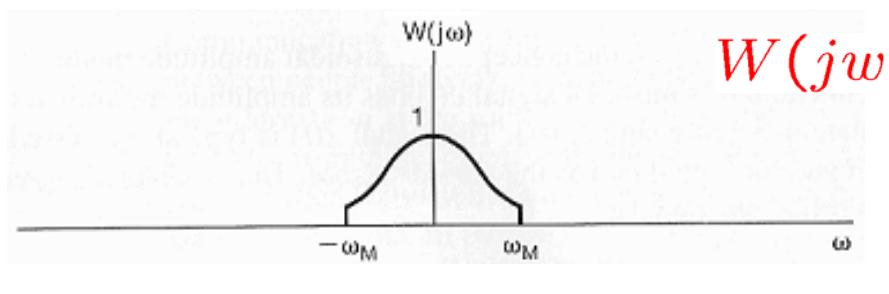
(b)



$$C_d(jw)$$



$$W(jw)$$



$$Y(j\omega) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(j\theta) C(j(\omega - \theta)) d\theta$$

■ AM with a Complex Exponential Carrier:



$$c_m(t) = e^{j(w_c t + \theta_c)}$$

$$\theta_c = 0$$



$$c_d(t) = e^{-j(w_c t + \theta_c)}$$

$$y(t) = x(t) c_m(t)$$

$$w(t) = y(t) c_d(t)$$

$$= x(t) e^{jw_c t}$$

$$= y(t) e^{-jw_c t}$$

$$= x(t) e^{jw_c t} e^{-jw_c t}$$

$$\Rightarrow w(t) = x(t)$$

$$Y(jw) = X(j(w - w_c))$$

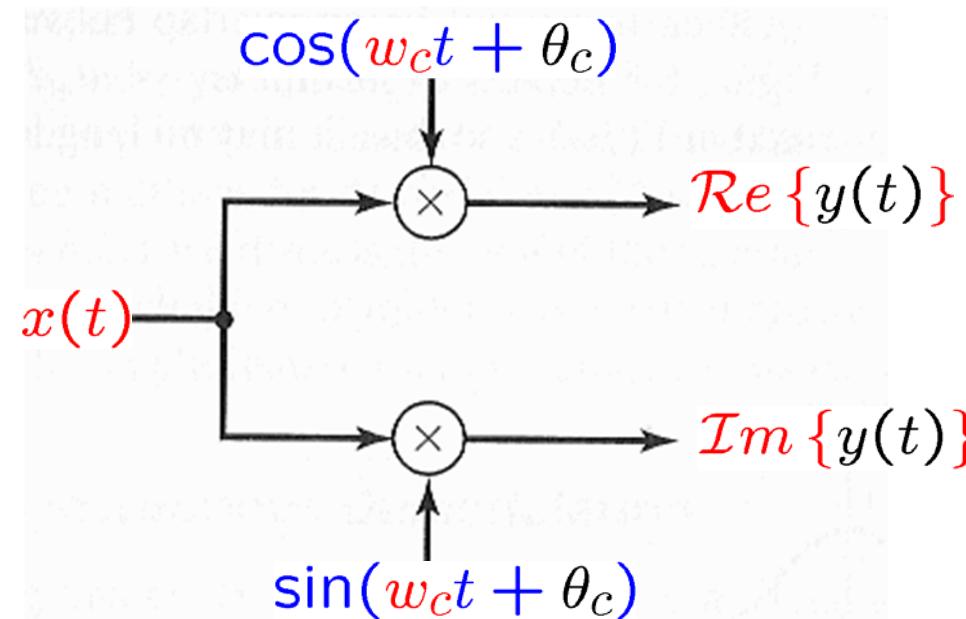
$$W(jw) = Y(j(w + w_c))$$

$$\Rightarrow W(jw) = X(jw)$$

- AM with Sinusoidal Carriers:

$$c(t) = e^{jw_ct} = \cos(w_ct) + j \sin(w_ct)$$

$$\Rightarrow y(t) = x(t) \cos(w_ct) + j x(t) \sin(w_ct)$$



phase difference of $c_1(\cdot), c_2(\cdot)$?

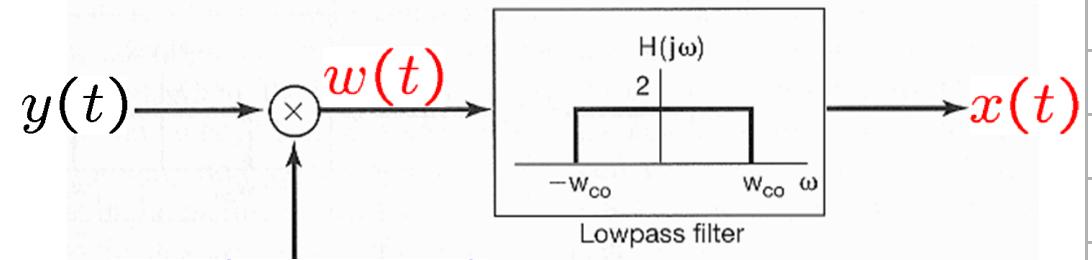
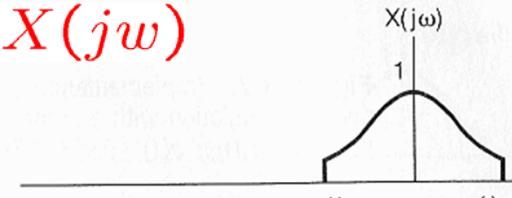
■ AM with a Sinusoidal Carrier:

$$Y(jw) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(j\theta) C(j(w - \theta)) d\theta$$



$$\cos(w_ct + \theta_c) \quad \theta_c = 0$$

$$X(jw)$$

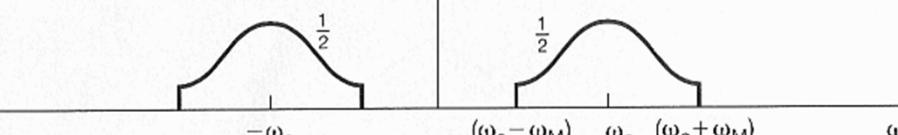


$$\cos(w_ct + \theta_c)$$

$$Y(jw)$$

$$Y(j\omega)$$

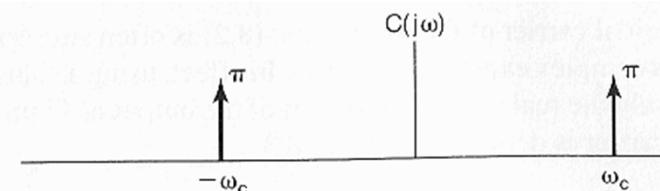
Lowpass filter



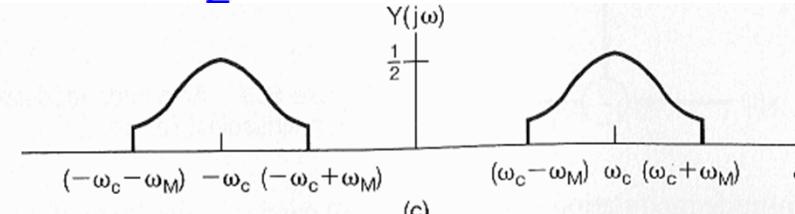
$$(a)$$

$$C(jw) = \pi [\delta(w - w_c) + \delta(w + w_c)]$$

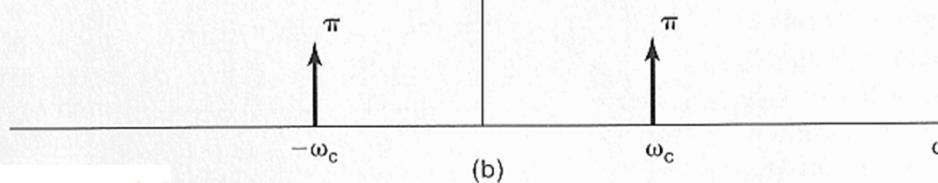
$$C(j\omega)$$



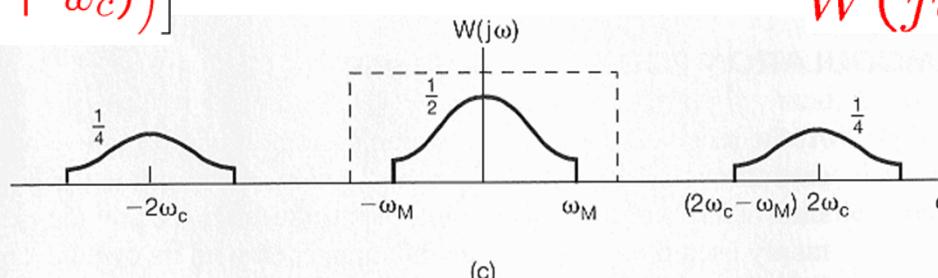
$$Y(jw) = \frac{1}{2} [X(j(w - w_c)) + X(j(w + w_c))]$$



$$(c)$$



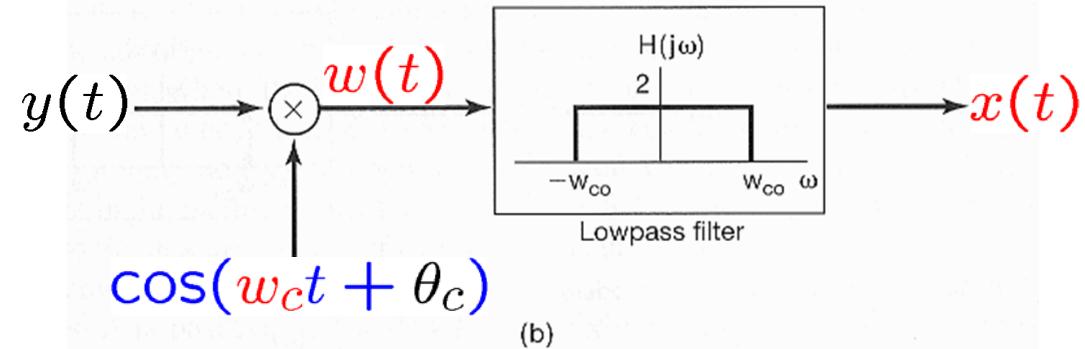
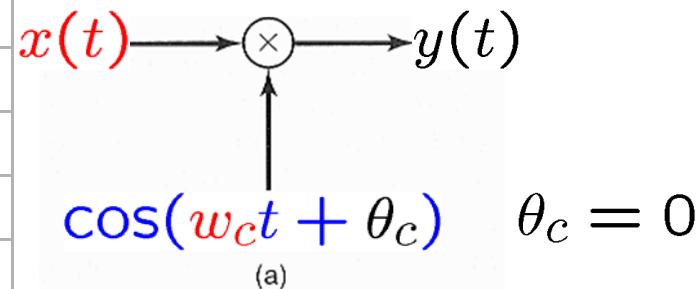
$$(b)$$



$$(c)$$

$$W(jw)$$

■ AM with a Sinusoidal Carrier:



$$y(t) = x(t) \cos(w_ct)$$

$$w(t) = y(t) \cos(w_ct)$$

$$\Rightarrow w(t) = x(t) \cos^2(w_ct)$$

$$= x(t) \left[\frac{1}{2} + \frac{1}{2} \cos(2w_ct) \right]$$

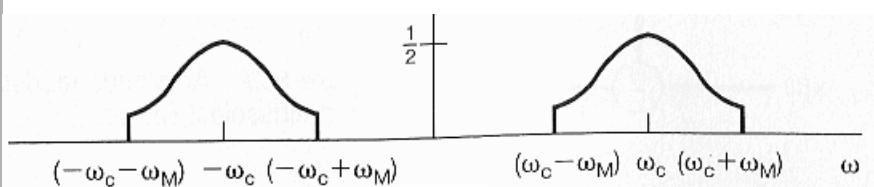
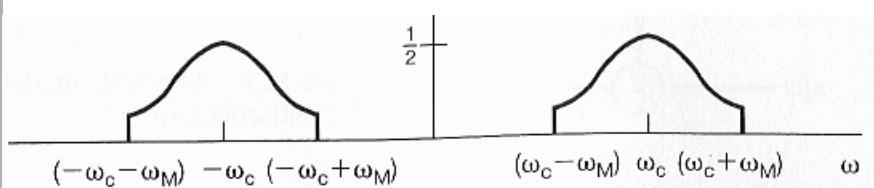
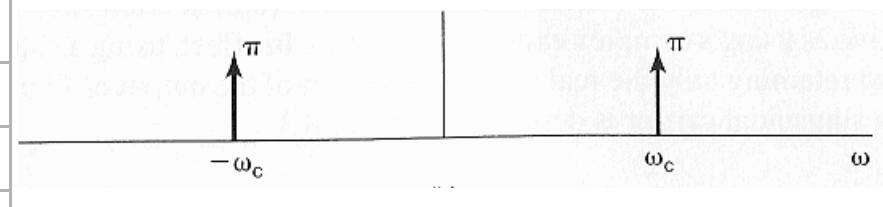
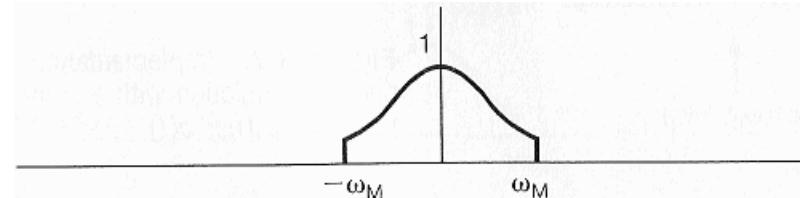
$$= \frac{1}{2}x(t) + \frac{1}{2}x(t) \cos(2w_ct)$$

Complex Exponential & Sinusoidal Amplitude Modulation & Demodulation

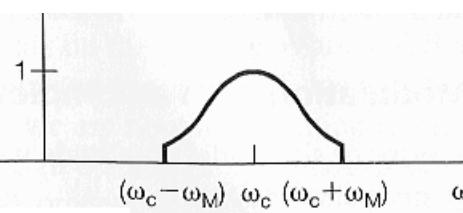
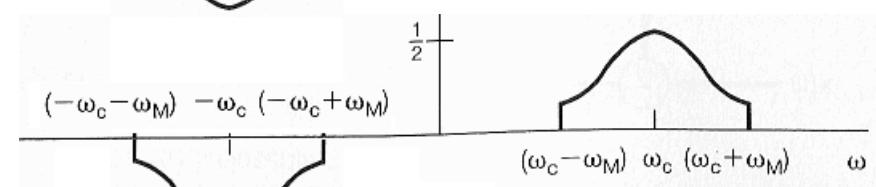
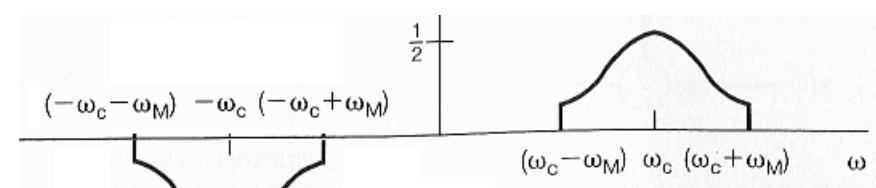
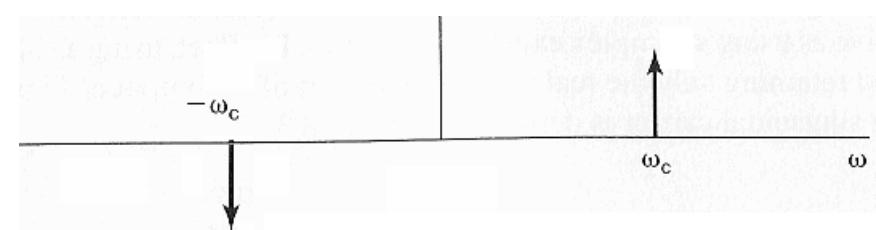
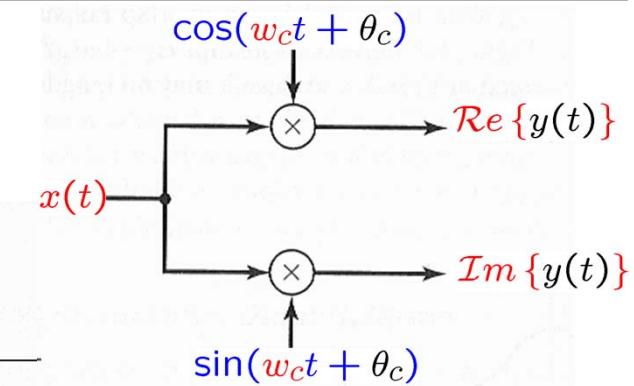
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$$c(t) = e^{j\omega_c t} = \cos(\omega_c t) + j \sin(\omega_c t)$$

$$y(t) = x(t) \cos(\omega_c t) + j x(t) \sin(\omega_c t)$$

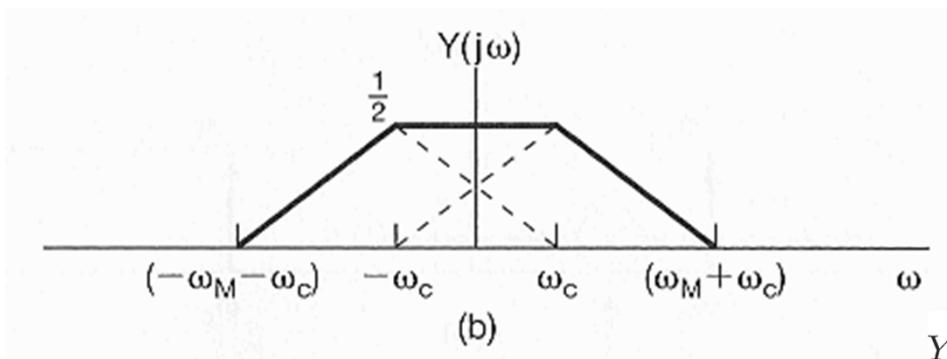
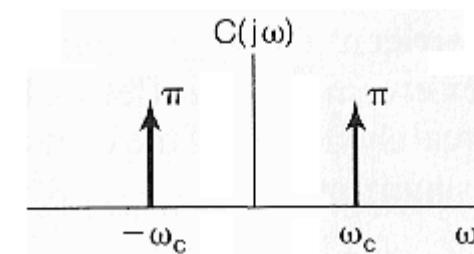
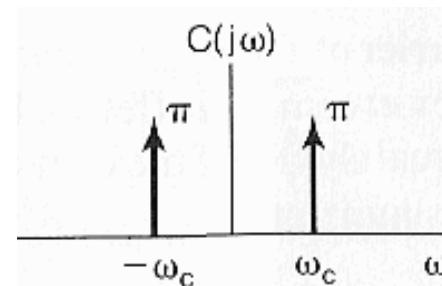
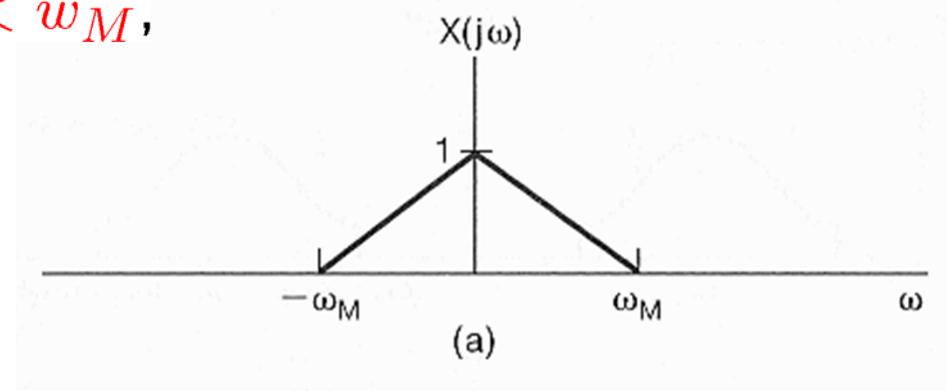


$$Y(jw) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(j\theta) C(j(w - \theta)) d\theta$$



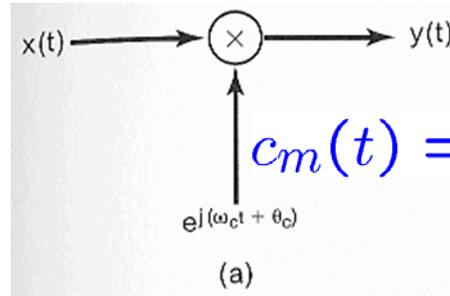
■ Overlapping of AM with a Sinusoidal Carrier:

- If $w_c < w_M$,

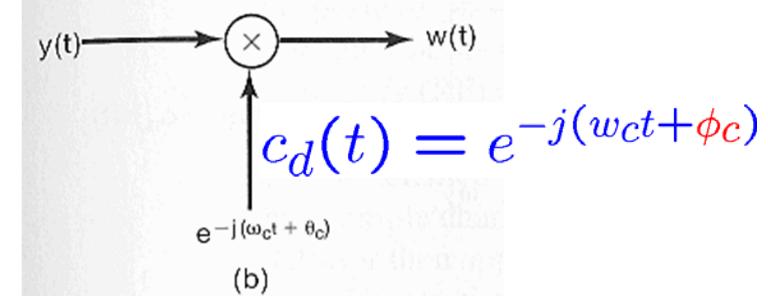


$$Y(jw) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(j\theta) C(j(w - \theta)) d\theta$$

■ Not Synchronized in Phase:



$$\theta_c \neq \phi_c$$



$$y(t) = x(t) c_m(t)$$

$$= x(t) e^{j(\omega_c t + \theta_c)}$$

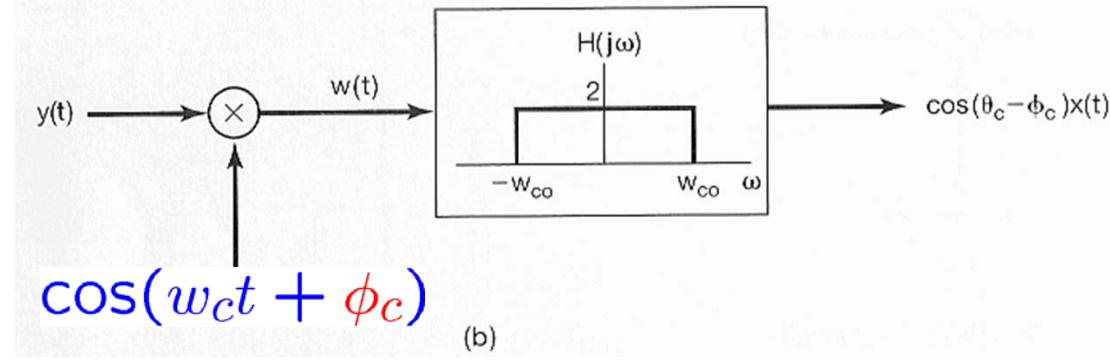
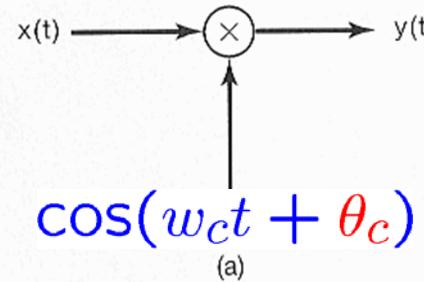
$$w(t) = y(t) c_d(t)$$

$$= y(t) e^{-j(\omega_c t + \theta_c)}$$

$$= x(t) e^{j(\theta_c - \phi_c)}$$

\Rightarrow ONLY $|x(t)| = |w(t)|$

■ Not Synchronized in Phase:



$$y(t) = x(t) \cos(w_ct + \theta_c)$$

$$w(t) = y(t) \cos(w_ct + \phi_c)$$

$$\Rightarrow w(t) = x(t) \cos(w_ct + \theta_c) \cos(w_ct + \phi_c)$$

$$= x(t) \left[\frac{1}{2} \cos(\theta_c - \phi_c) + \frac{1}{2} \cos(2w_ct + \theta_c + \phi_c) \right]$$

$$= \frac{1}{2} \cos(\theta_c - \phi_c) x(t) + \frac{1}{2} x(t) \cos(2w_ct + \theta_c + \phi_c)$$

■ Asynchronous Demodulation:

- $w_c \gg w_M$

- $x(t) > 0, \forall t$

- In audio transmission

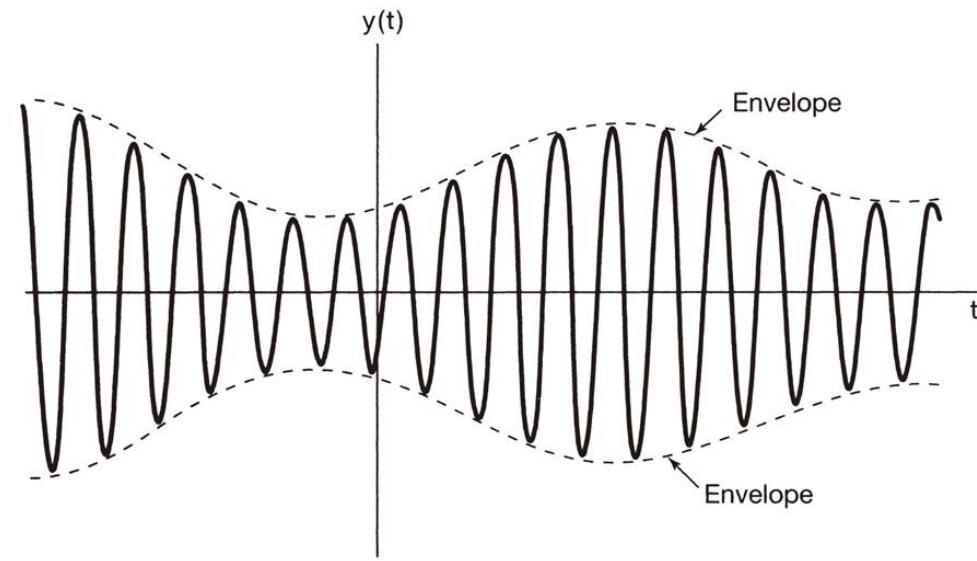
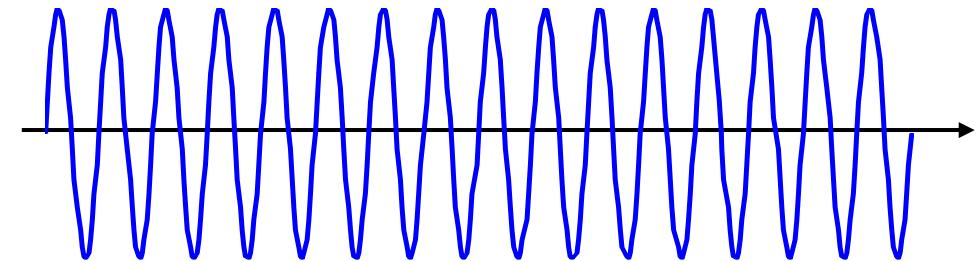
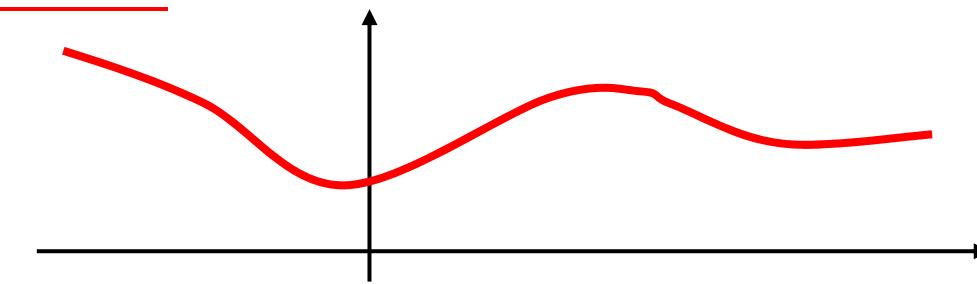
- over a RF channel

- $> w_M: 15 - 20 \text{ Hz}$

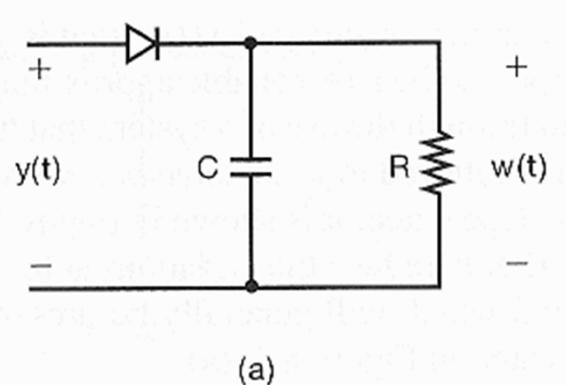
- $> w_c/2\pi: 500\text{kHz} - 2 \text{ MHz}$

$$y(t) = x(t) \cos(w_ct + \theta_c)$$

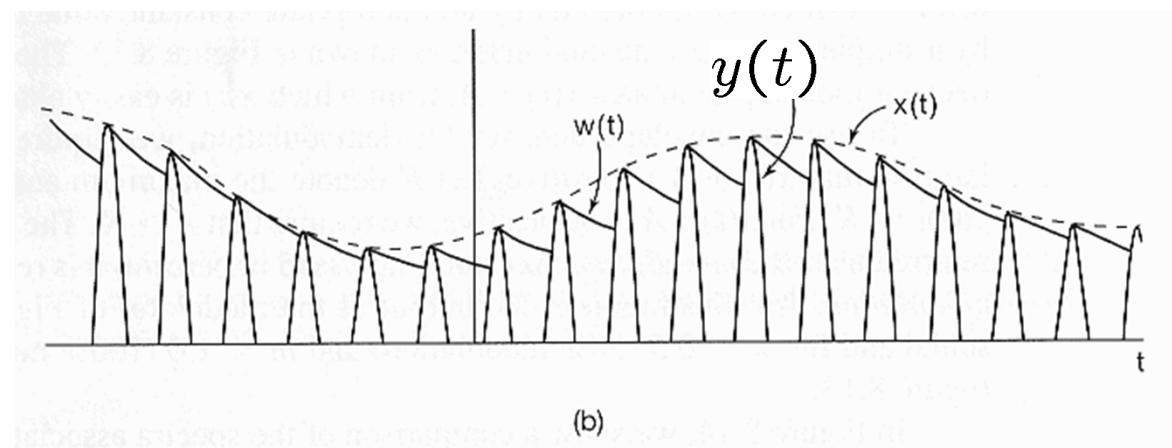
$$\approx x(t)$$



■ Envelope Detector:

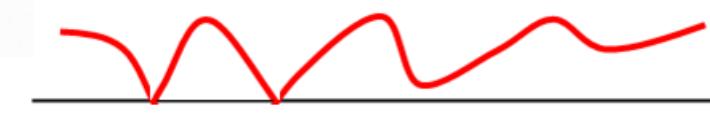
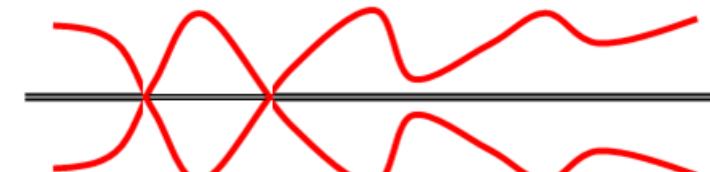
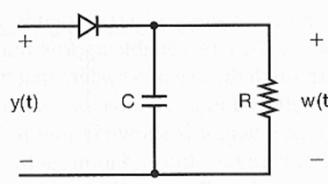
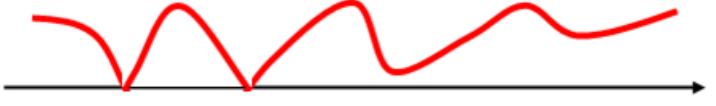
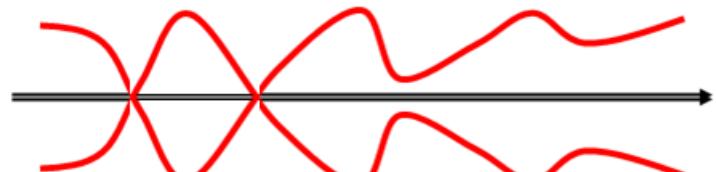
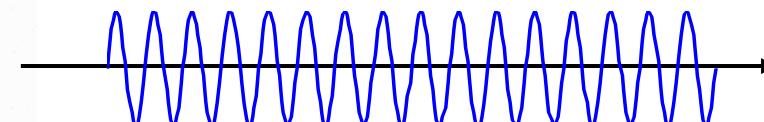
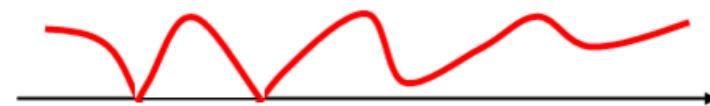
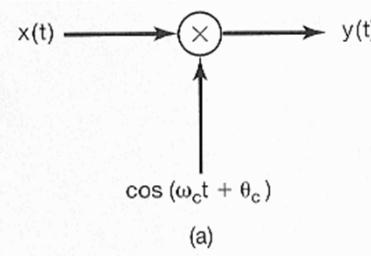
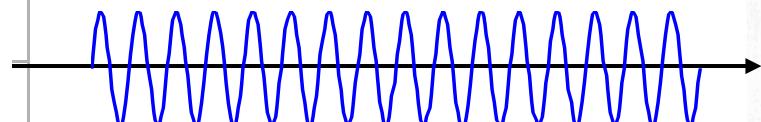
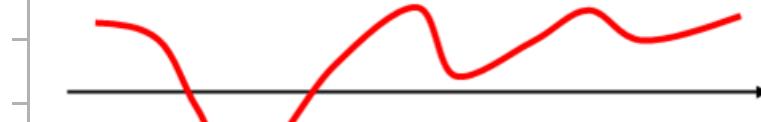


(a)



(b)

■ Asynchronous Demodulation:



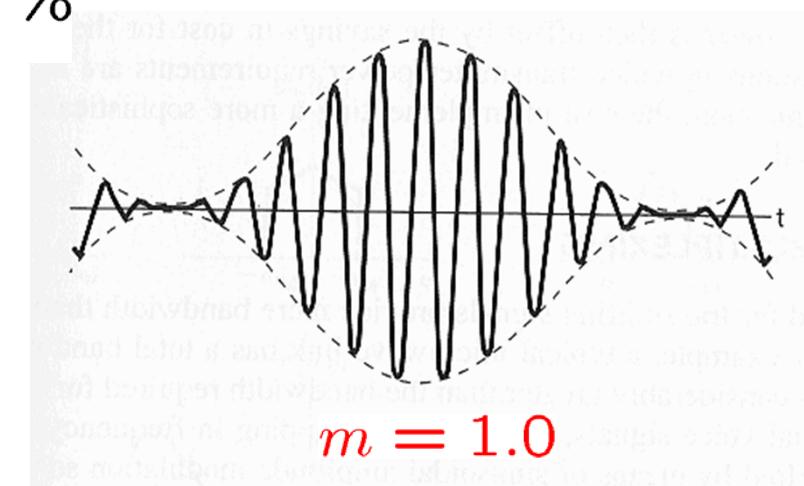
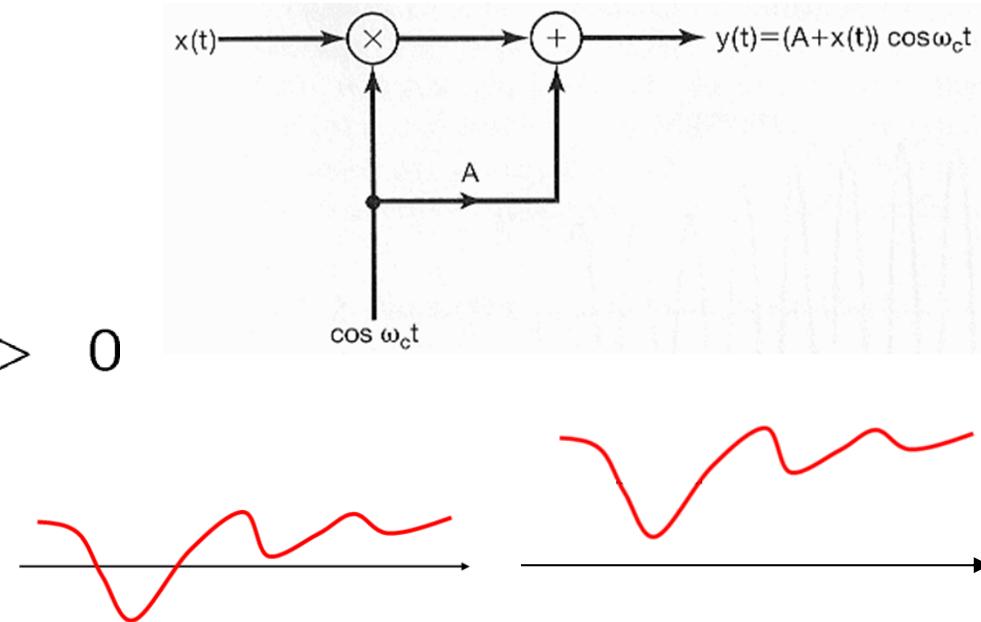
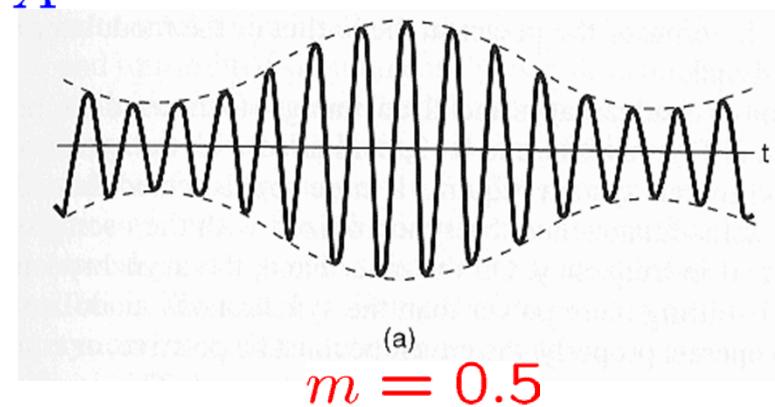
■ Asynchronous Demodulation:

- $w_c \gg w_M$
- $x(t) > 0, \forall t$

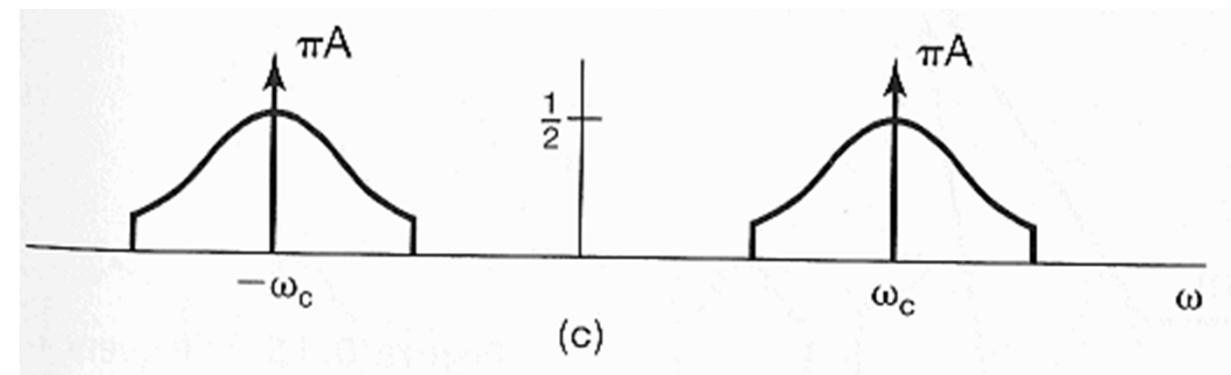
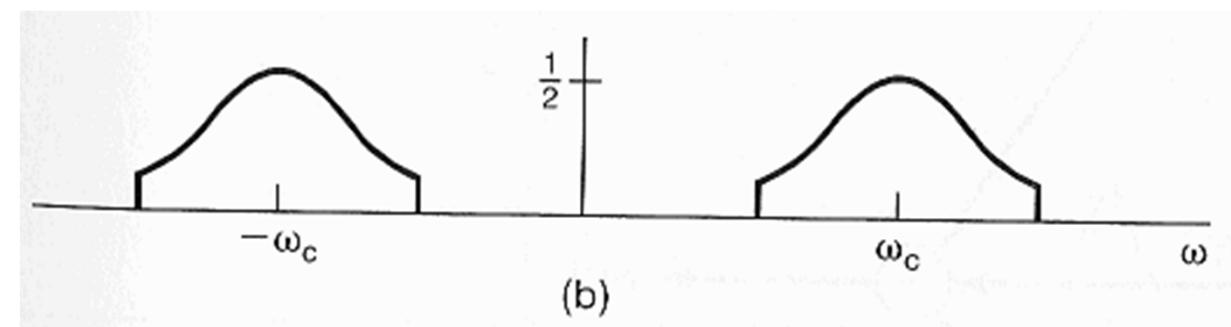
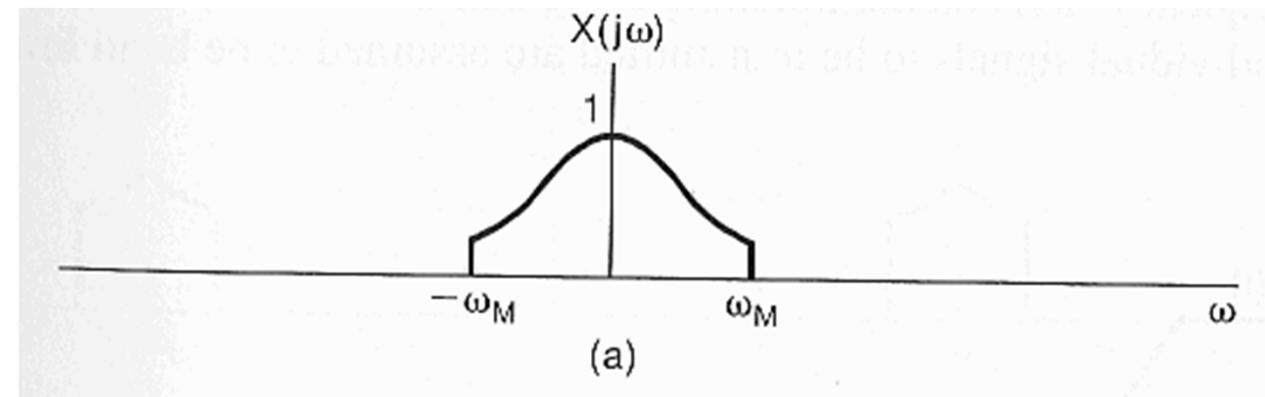
If not, $x(t) \rightarrow x(t) + A > 0$

$$A \geq K, |x(t)| \leq K$$

- $\frac{K}{A}$: modulation index m , in %



■ Synchronous & Asynchronous Demodulation:

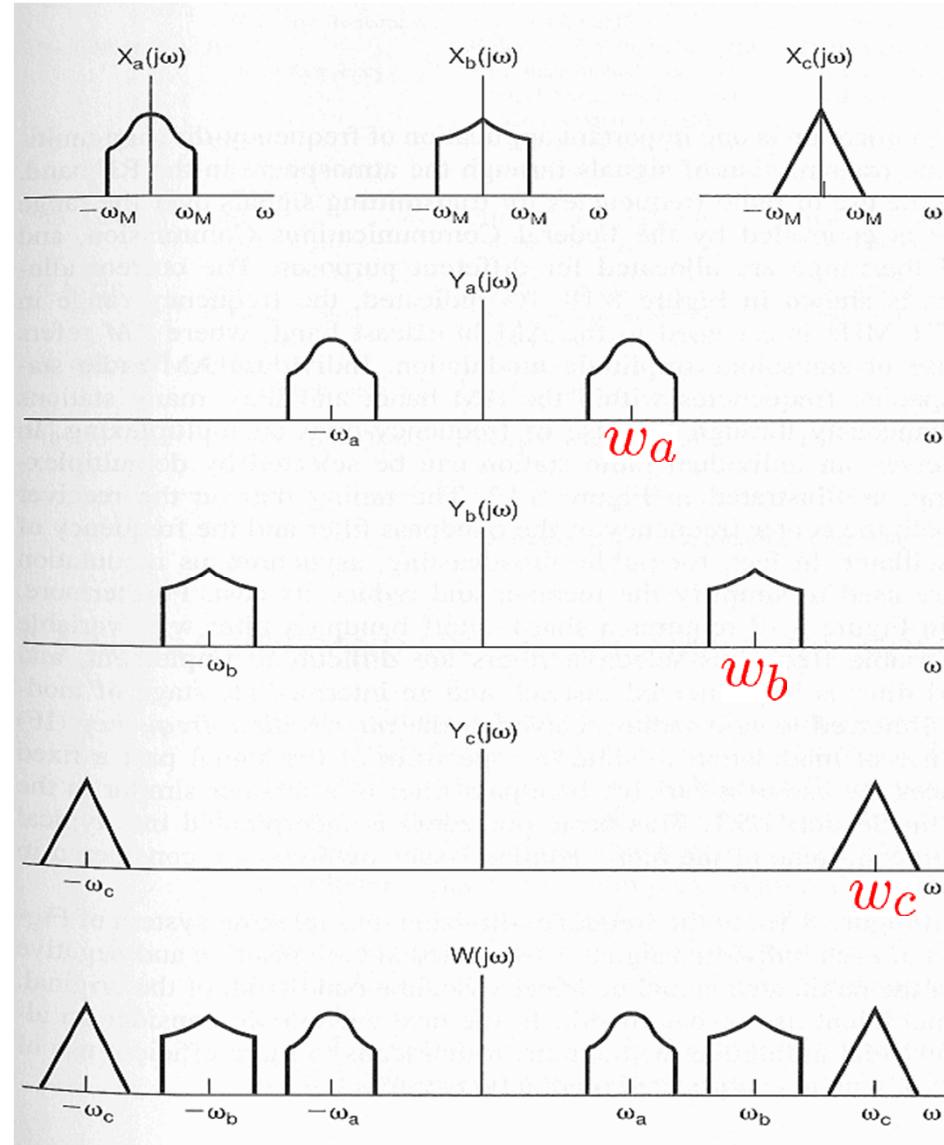
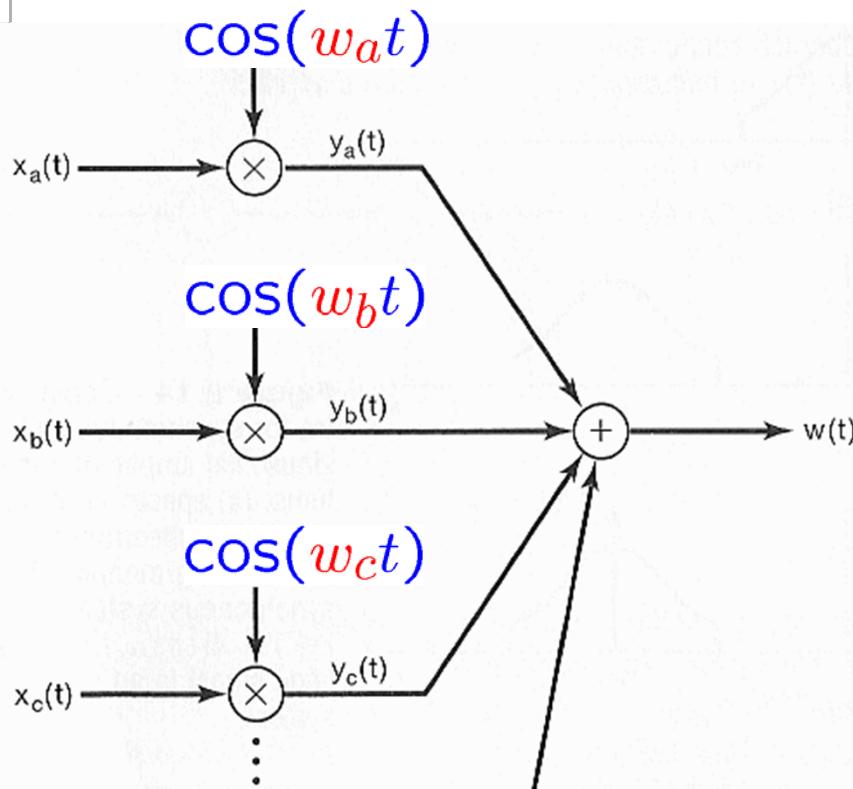


$x(t) \cos(\omega_{ct})$

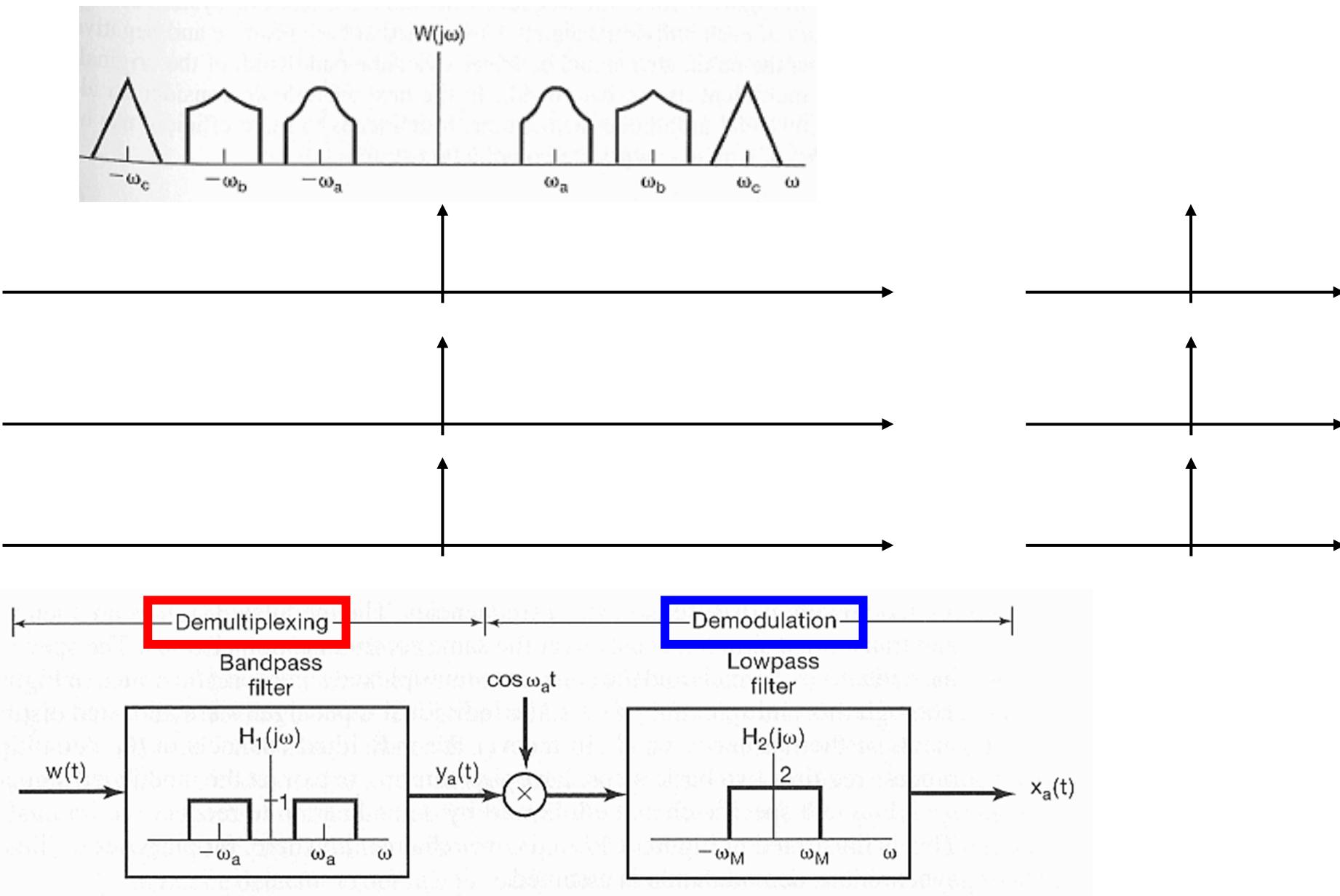
$[x(t) + A] \cos(\omega_{ct})$

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FDM Using Sinusoidal AM:



■ Demultiplexing and Demodulation:



Allocation of Frequencies in the RF Spectrum

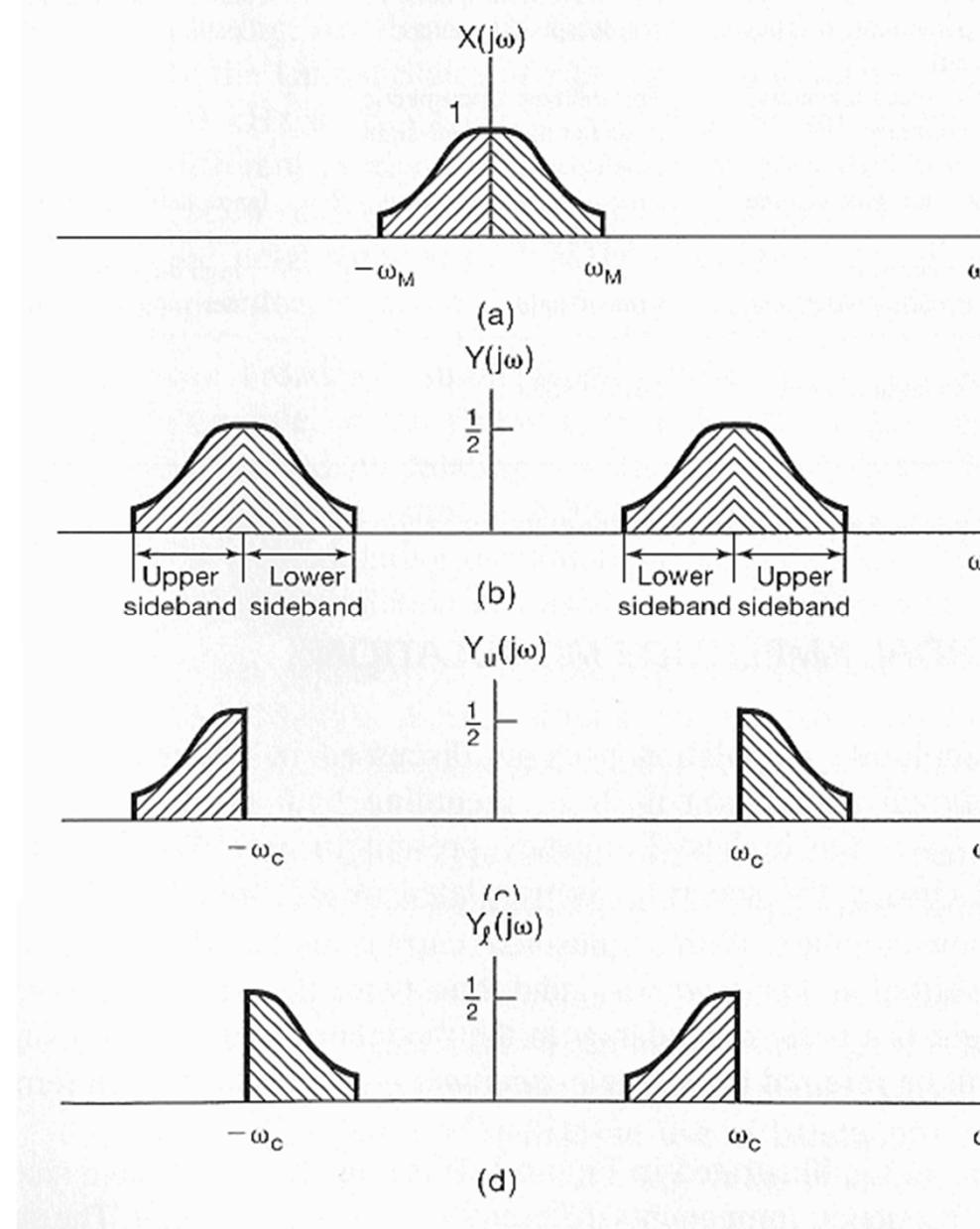
| Frequency range | Designation | Typical uses | Propagation method | Channel features |
|---------------------|--------------------------------------|--|--|--|
| 30–300 Hz | ELF (extremely low frequency) | Macrowave, submarine communication | Megametric waves | Penetration of conducting earth and seawater |
| 0.3–3 kHz | VF (voice frequency) | Data terminals, telephony | Copper wire | |
| 3–30 kHz | VLF (very low frequency) | Navigation, telephone, telegraph, frequency and timing standards | Surface ducting (ground wave) | Low attenuation, little fading, extremely stable phase and frequency, large antennas |
| 30–300 kHz | LF (low frequency) | Industrial (power line) communication, aeronautical and maritime long-range navigation, radio beacons | Mostly surface ducting | Slight fading, high atmospheric pulse |
| 0.3–3 MHz | MF (medium frequency) | Mobile, AM broadcasting, amateur, public safety | Ducting and ionospheric reflection (sky wave) | Increased fading, but reliable |
| 3–30 MHz | HF (high frequency) | Military communication, aeronautical mobile, international fixed, amateur and citizen's band, industrial | Ionospheric reflecting sky wave, 50–400 km layer altitudes | Intermittent and frequency-selective fading, multipath |
| 30–300 MHz | VHF (very high frequency) | FM and TV broadcast, land transportation (taxis, buses, railroad) | Sky wave (ionospheric and tropospheric scatter) | Fading, scattering, and multipath |
| 0.3–3 GHz | UHF (ultra high frequency) | UHF TV, space telemetry, radar, military | Transhorizon tropospheric scatter and line-of-sight relaying | |
| 3–30 GHz | SHF (super high frequency) | Satellite and space communication, common carrier (CC), microwave | Line-of-sight ionosphere penetration | Ionospheric penetration, extraterrestrial noise, high directly |
| 30–300 GHz | EHF (extremely high frequency) | Experimental, government, radio astronomy | Line of sight | Water vapor and oxygen absorption |
| 10^3 – 10^7 GHz | Infrared, visible light, ultraviolet | Optical communications | Line of sight | |

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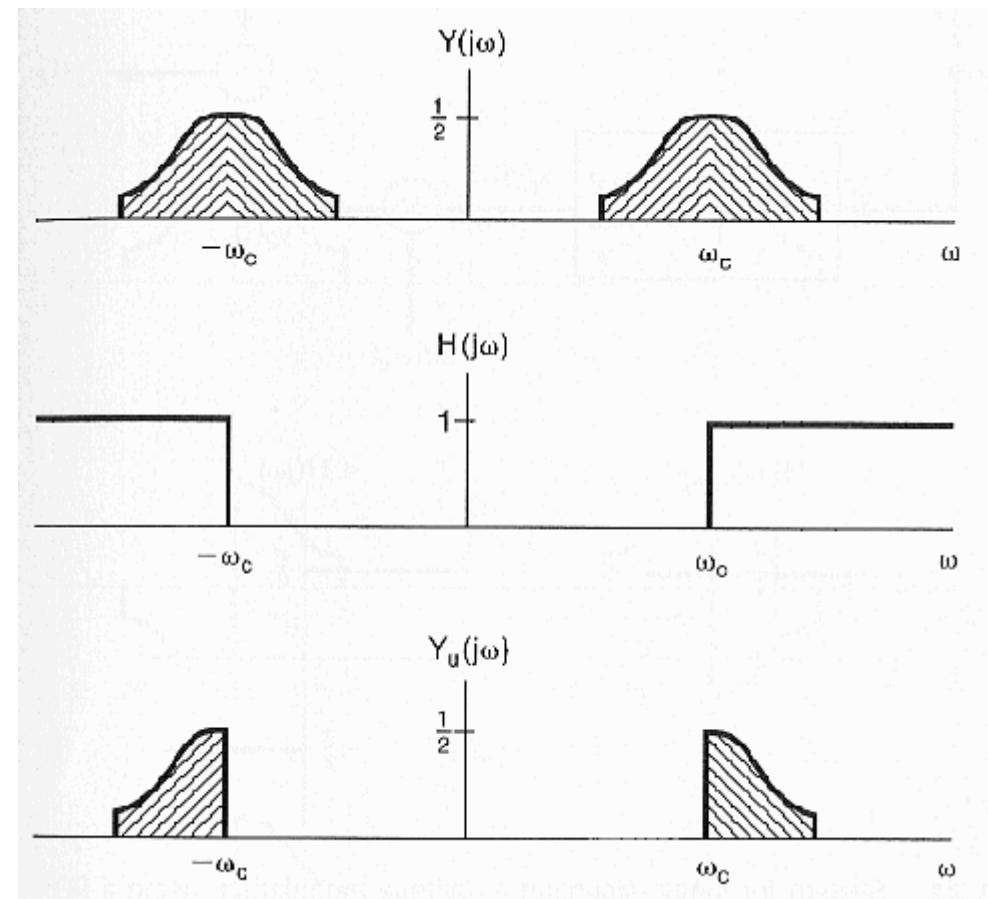
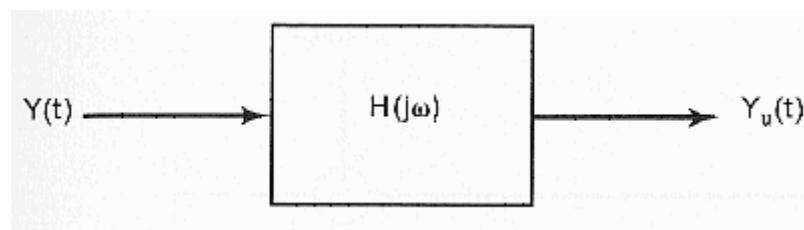
- SSB Modulation:

upper sidebands

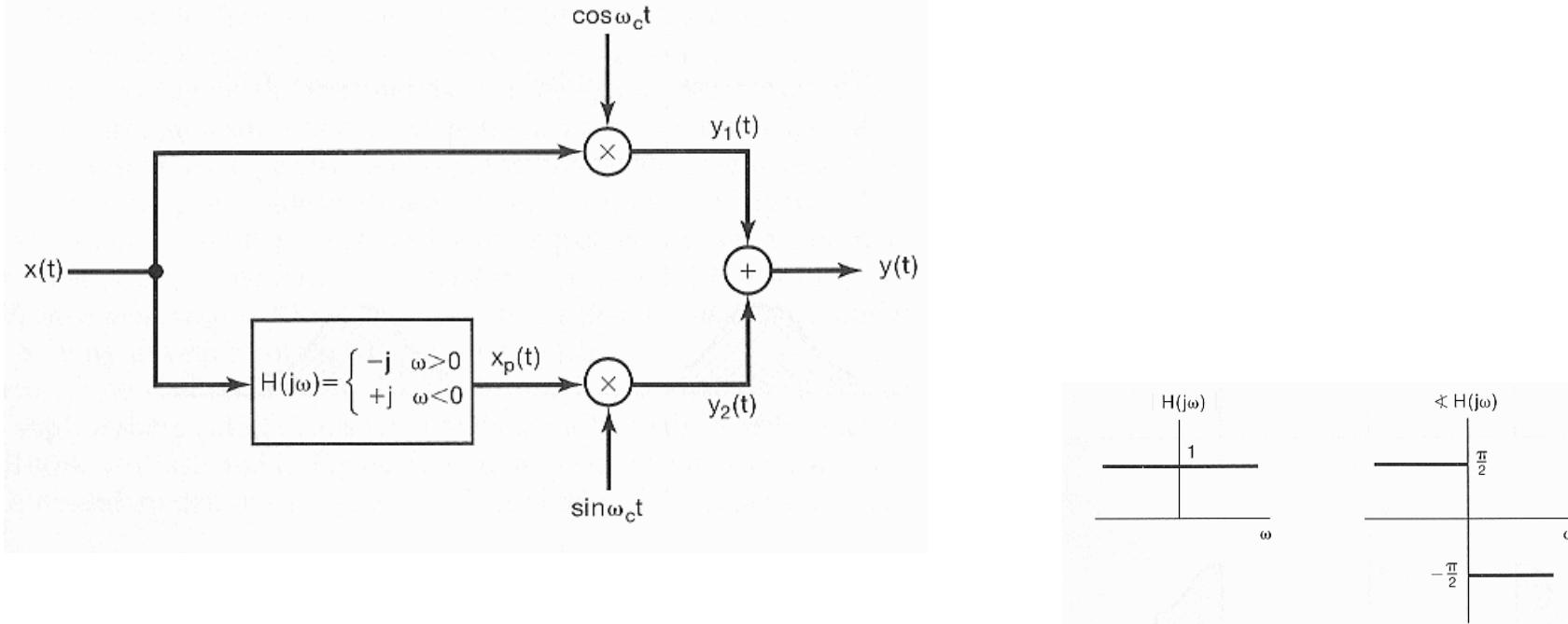
lower sidebands



- Retain Upper Sidebands Using Ideal Highpass Filter

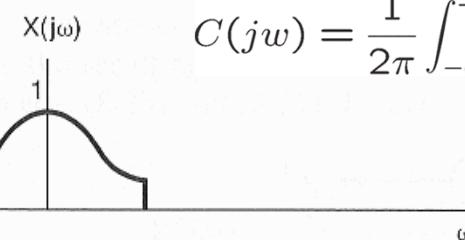


■ Retain Lower Sidebands Using Phase-Shift Network

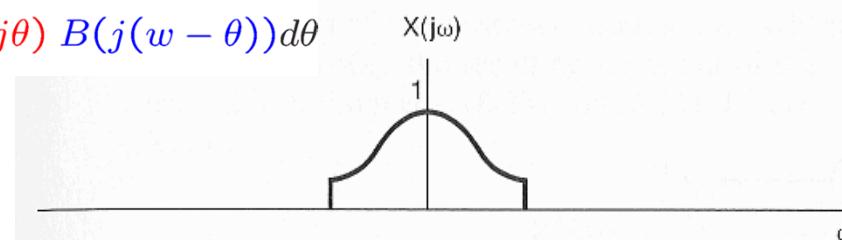


- Retain Lower Sidebands $H(j\omega) = \begin{cases} -j, & \omega > 0 \\ +j, & \omega < 0 \end{cases}$
- Retain Upper Sidebands $H(j\omega) = \begin{cases} +j, & \omega > 0 \\ -j, & \omega < 0 \end{cases}$

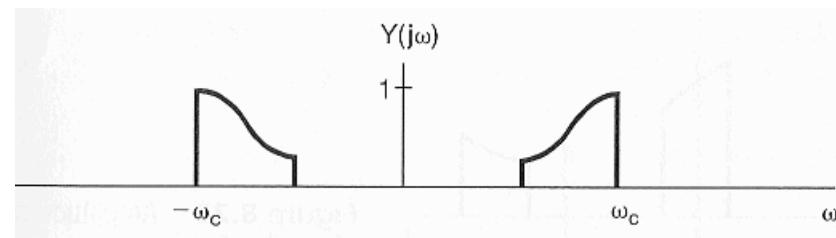
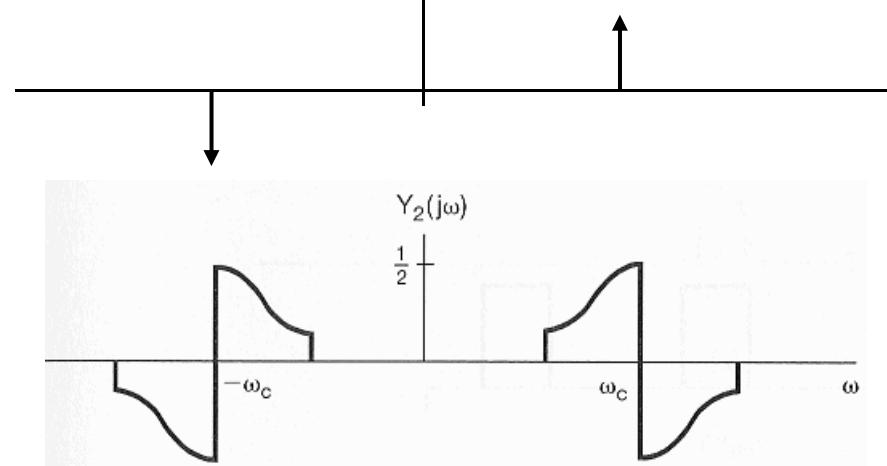
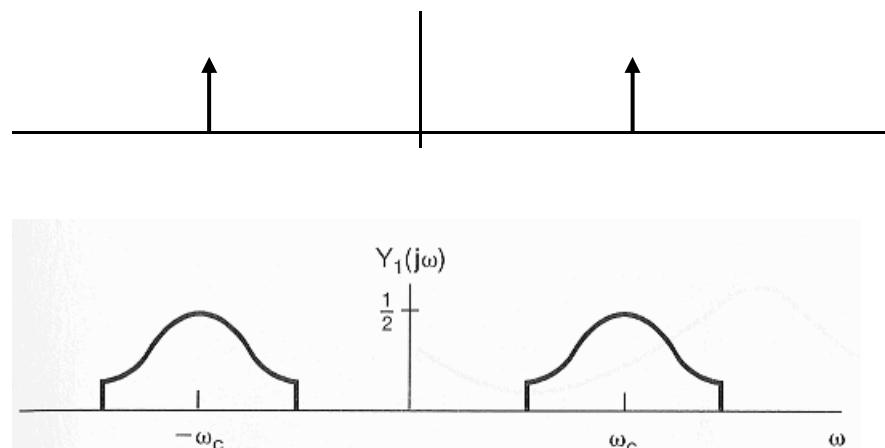
Single-Sideband Sinusoidal Amplitude Modulation



$$C(jw) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} A(j\theta) B(j(w - \theta)) d\theta$$

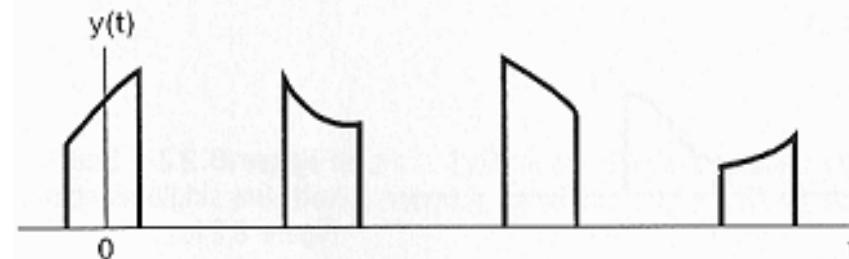
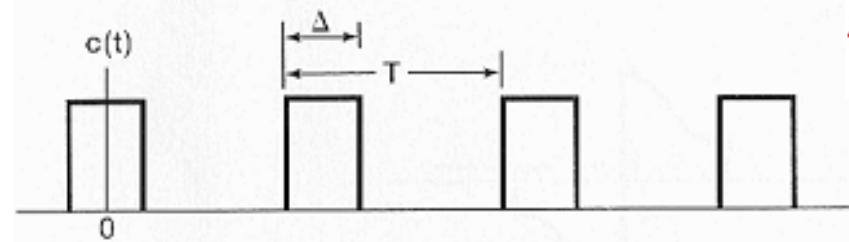
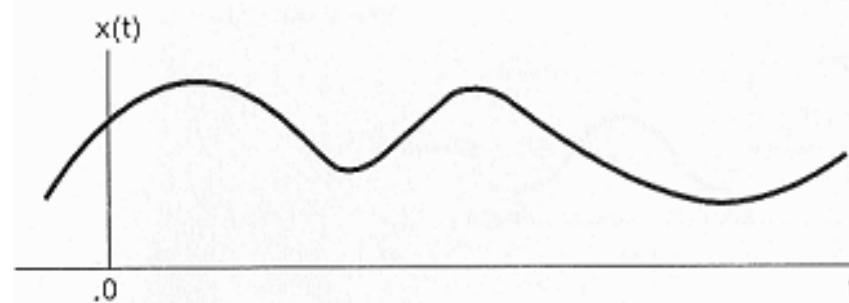
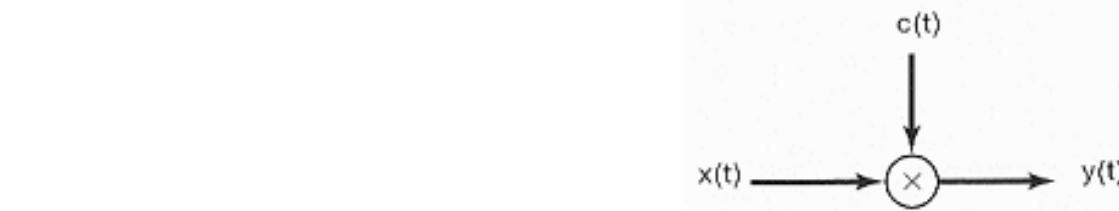


$$H(jw) = \begin{cases} -j, & w > 0 \\ +j, & w < 0 \end{cases}$$

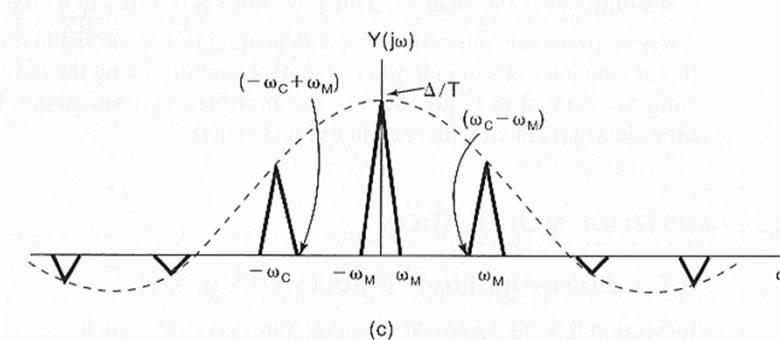
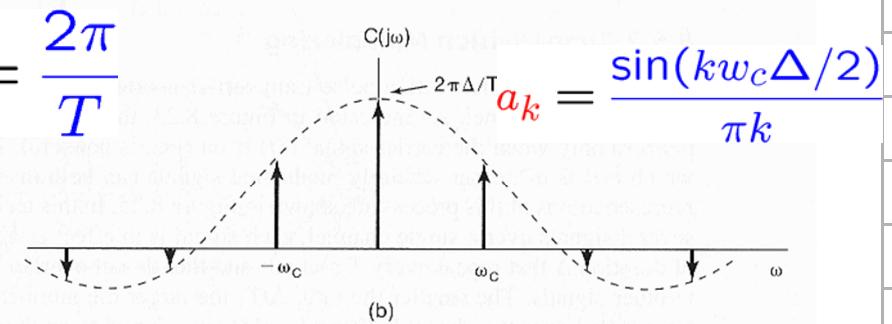
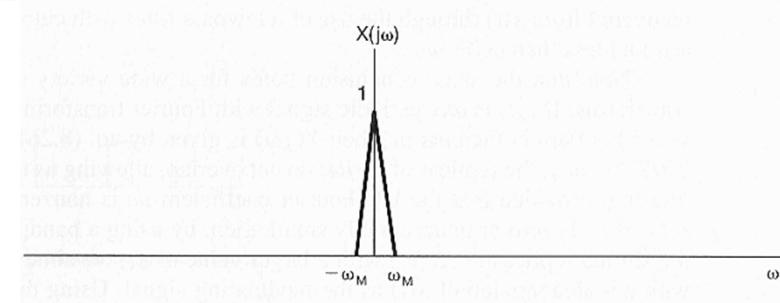


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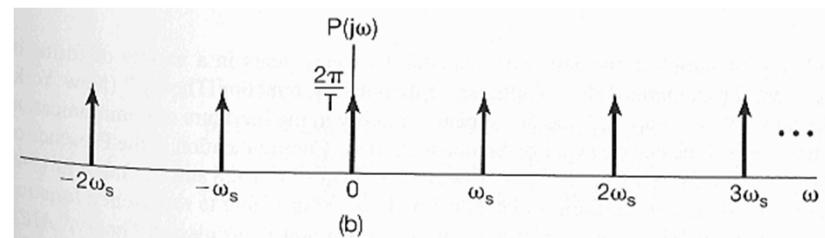
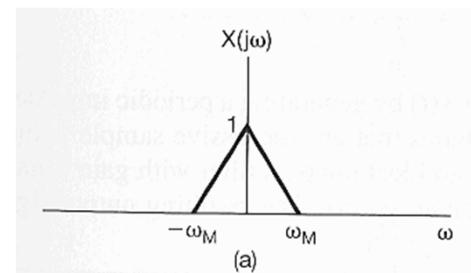
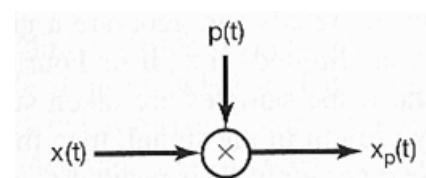
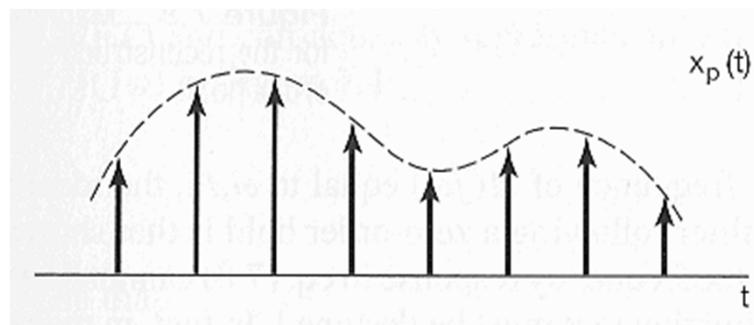
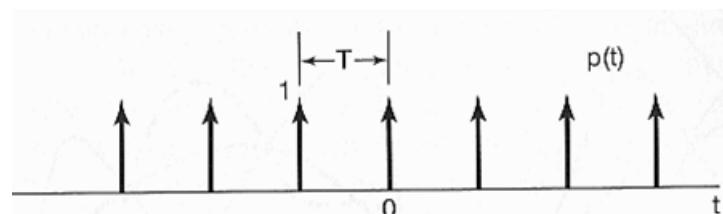
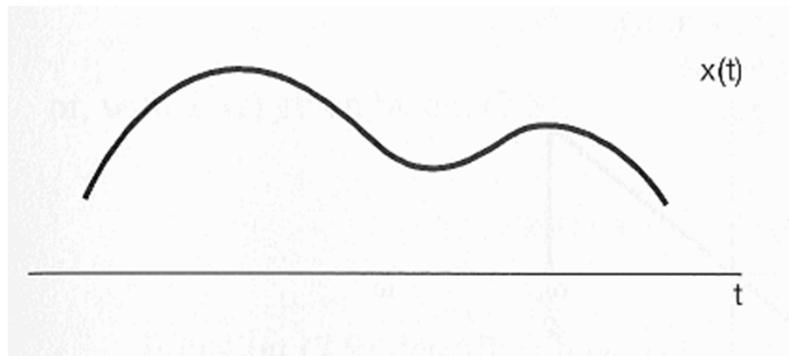
■ Modulation of a Pulse-Train Carrier:



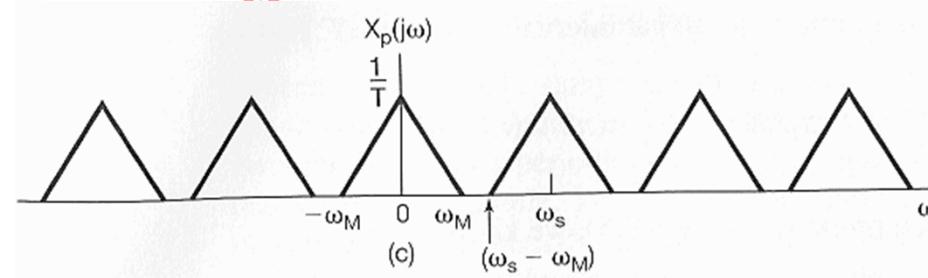
$$\omega_c = \frac{2\pi}{T}$$

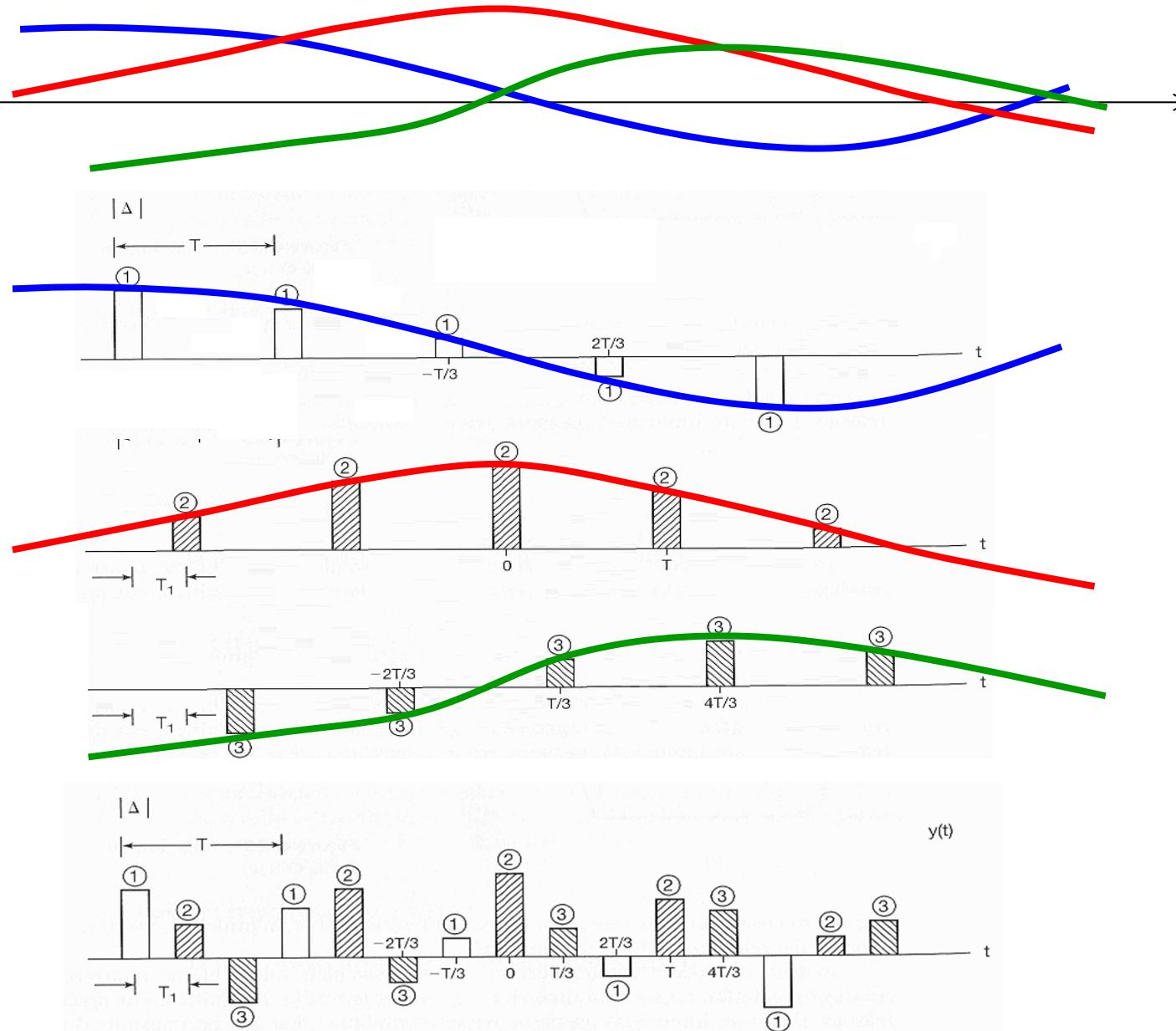


■ Impulse-Train Sampling:

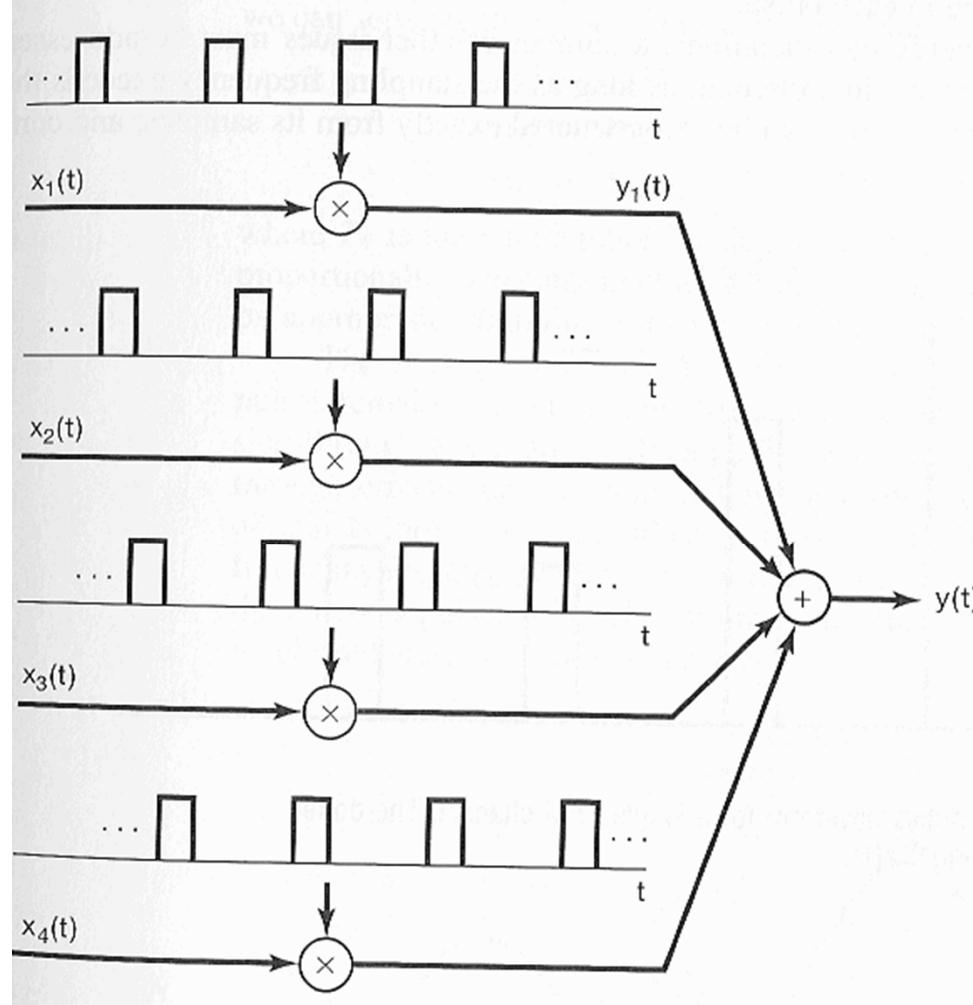


$$w_s > 2w_M$$

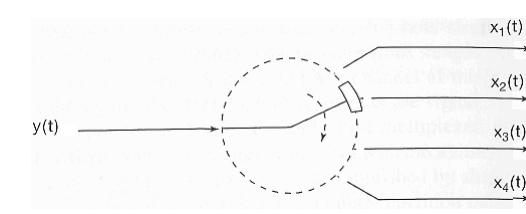
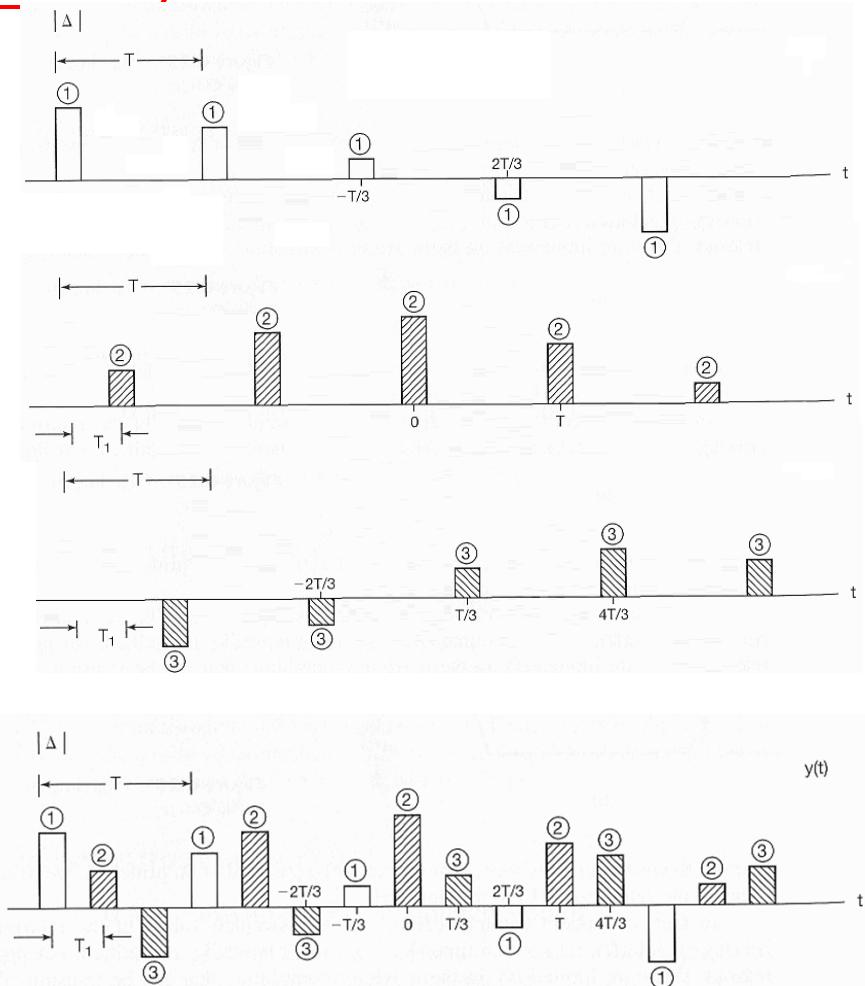
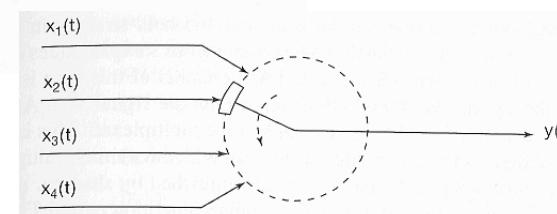


■ Time-Division Multiplexing (TDM):

■ Time-Division Multiplexing (TDM):

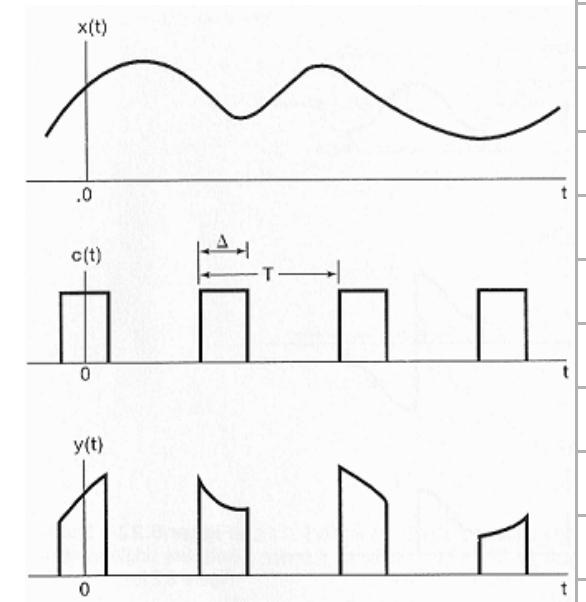
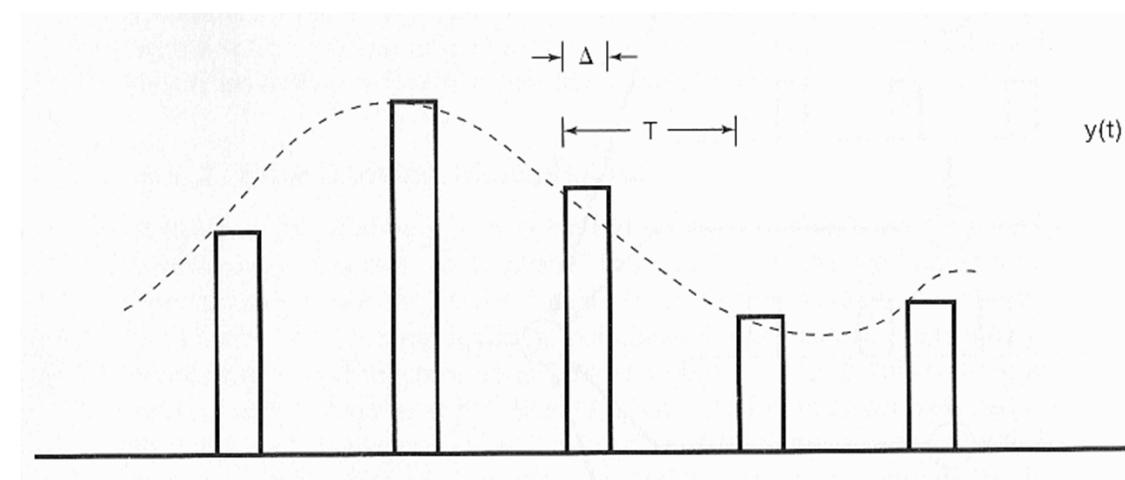


(b)

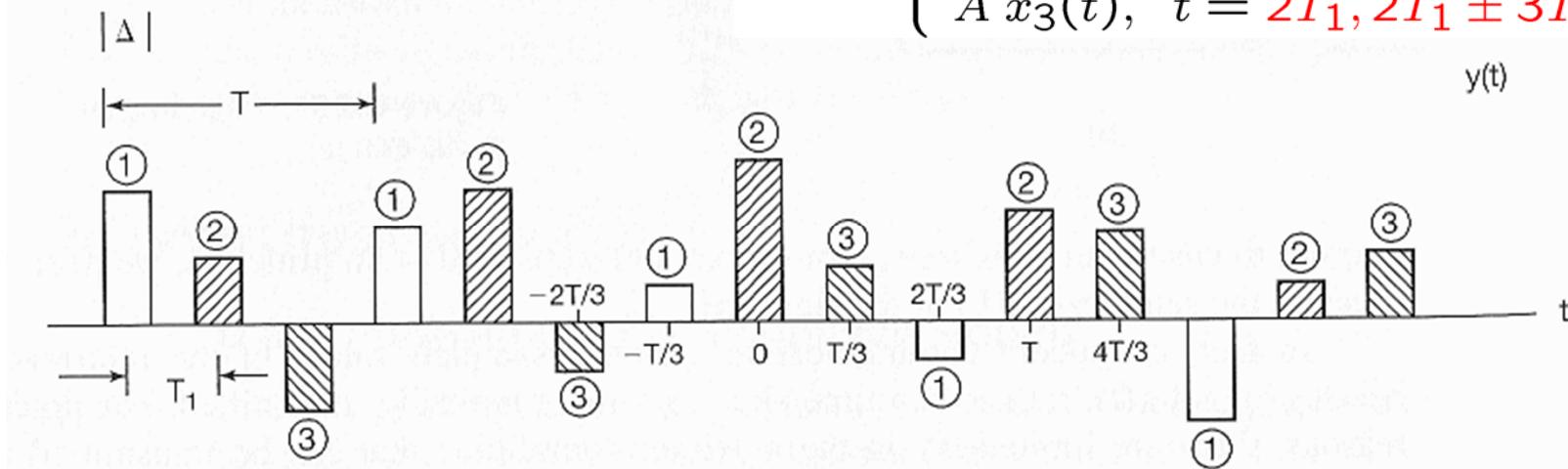


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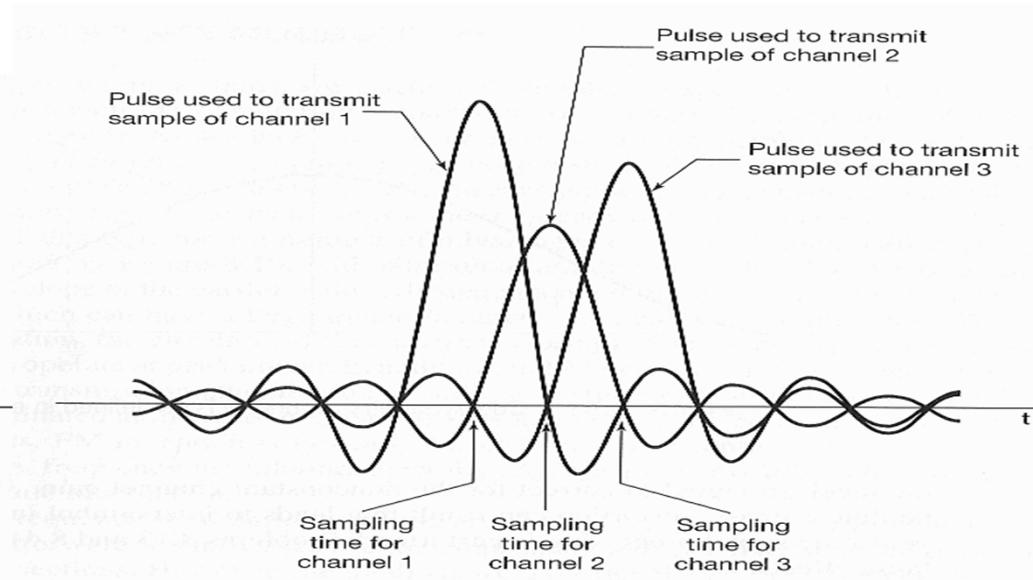
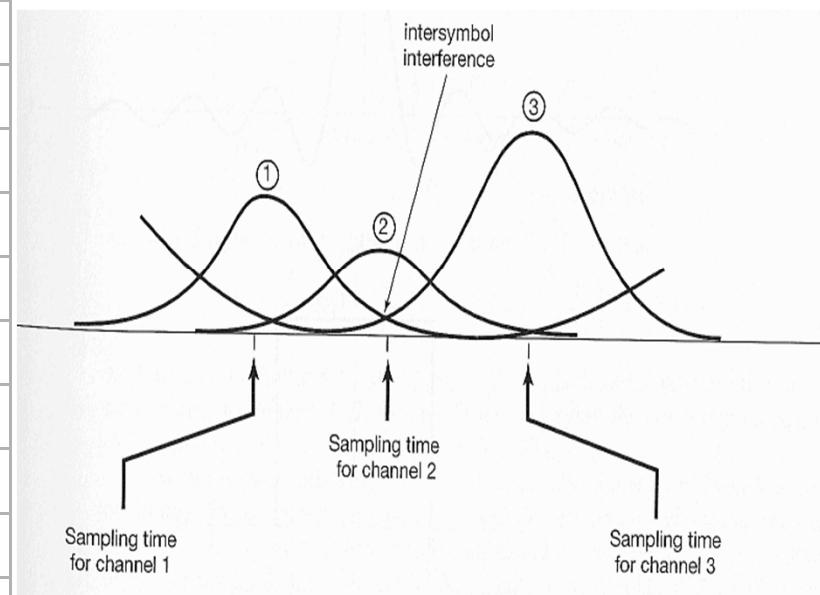
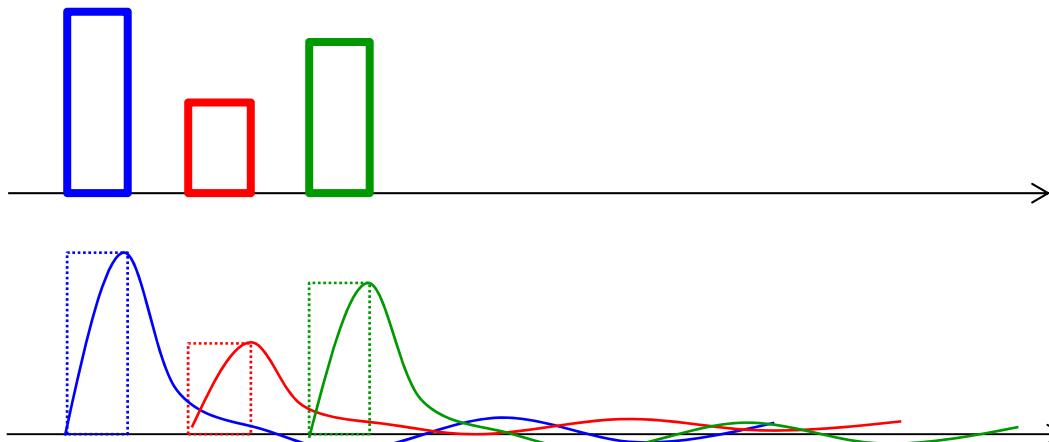
■ Pulse-Amplitude Modulated Signals:



■ TDM-PAM:



■ Intersymbol Interference in PAM Systems:

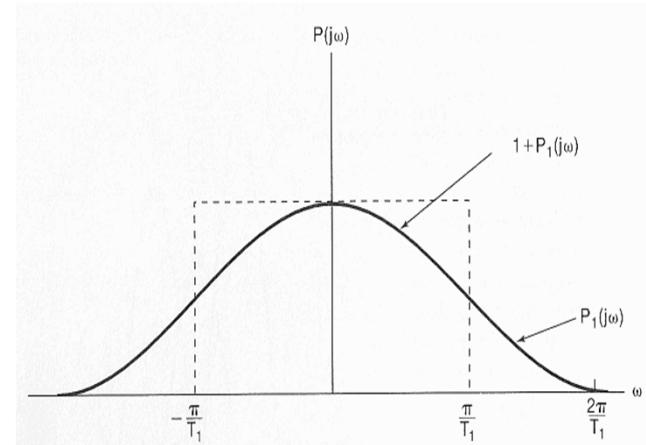
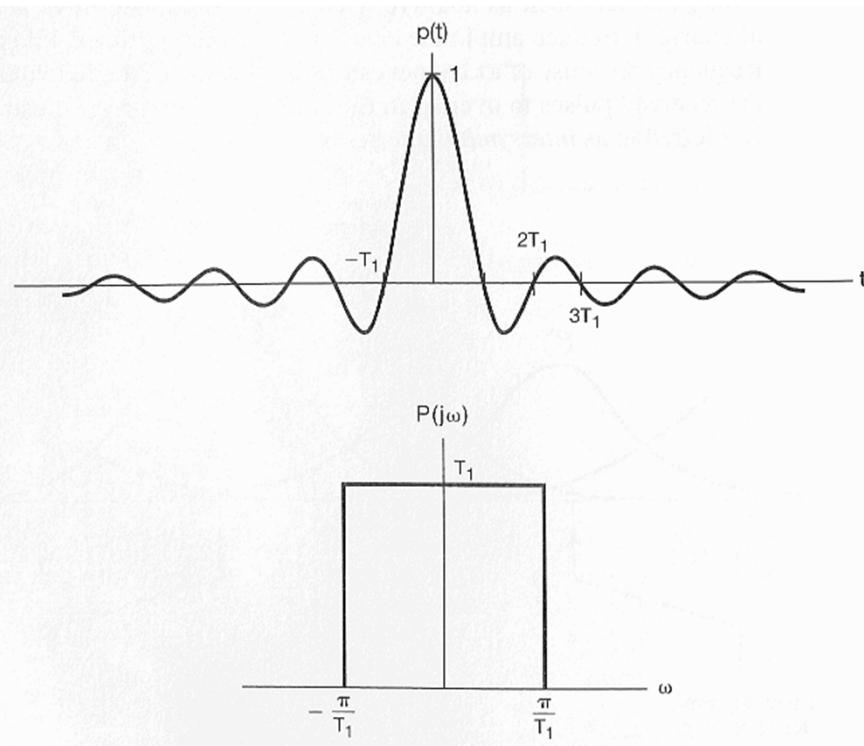


■ Avoiding Intersymbol Interference in PAM Systems:

$$p(t) = \frac{T_1 \sin(\pi t / T_1)}{\pi t}$$

$$p(\pm T_1) = 0, \quad p(\pm 2T_1) = 0, \quad p(\pm 3T_1) = 0, \dots$$

Zero-Crossing at kT_1

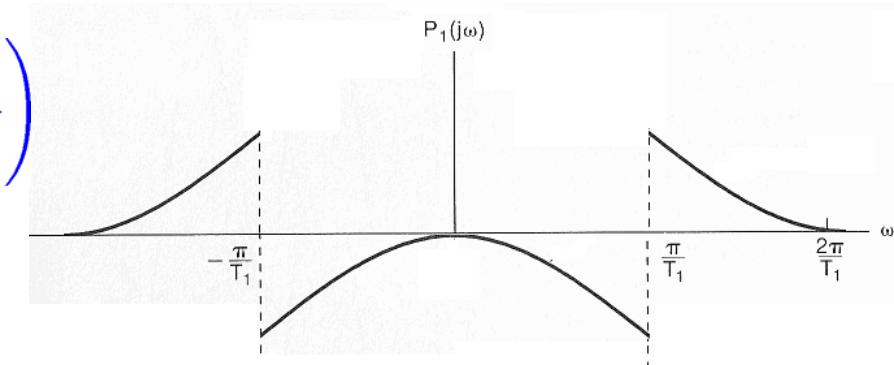


Problem 8.42

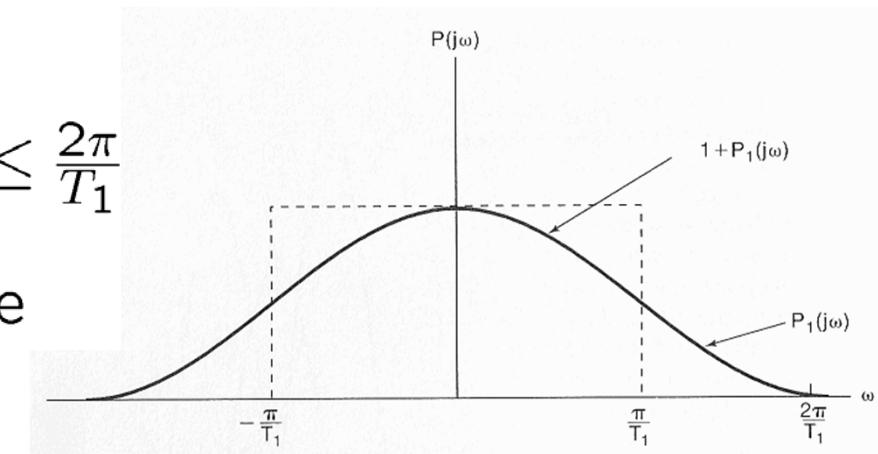
■ General Form of Band-Limited Pulseswith Time-Domain Zero-Crossing at kT_1 , $k \in \mathbb{Z}$: $P_1(jw)$: odd symmetry around π/T_1

$$P_1\left(-jw + j\frac{\pi}{T_1}\right) = -P_1\left(jw + j\frac{\pi}{T_1}\right)$$

$$0 \leq w \leq \frac{\pi}{T_1}$$



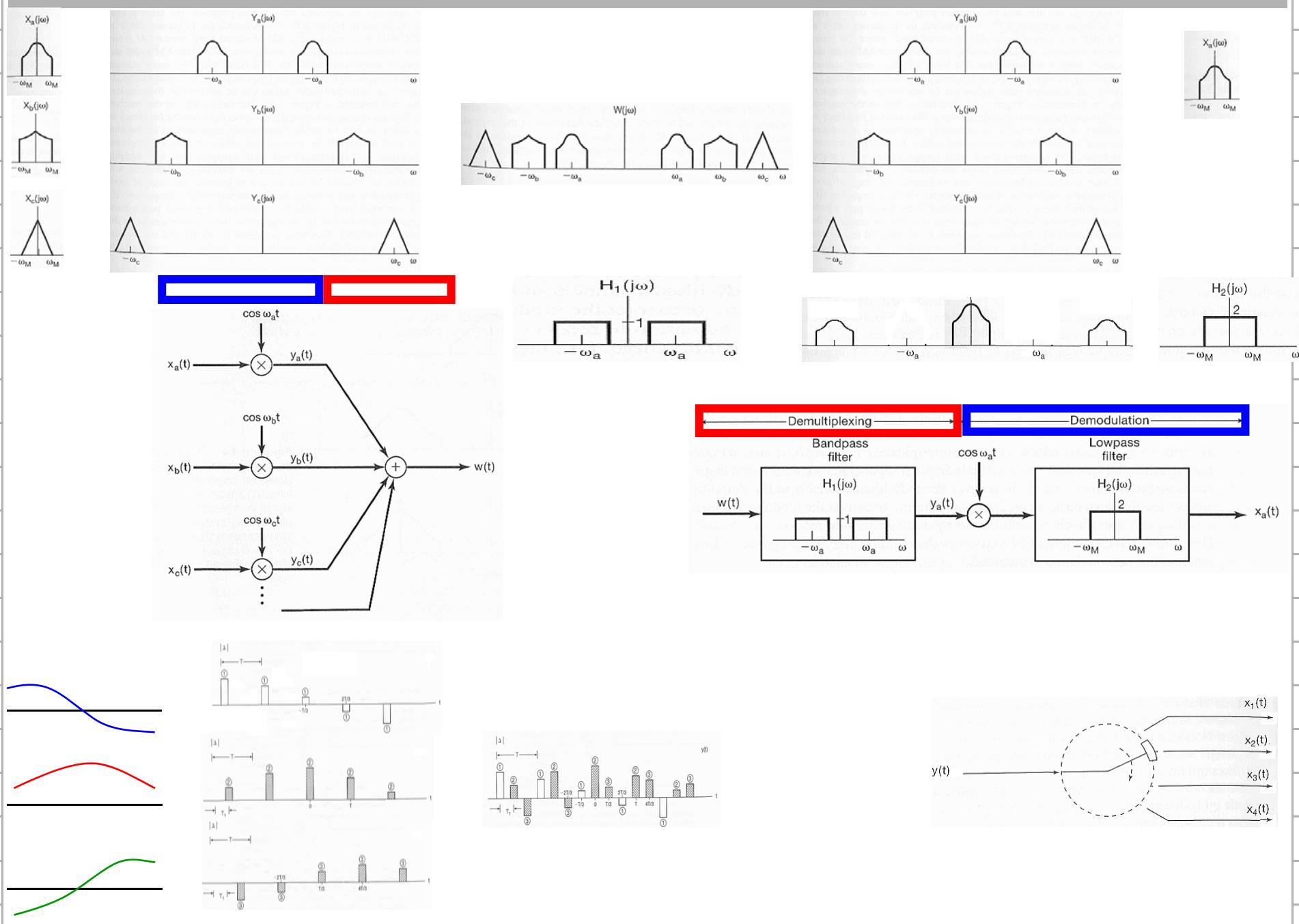
$$P(jw) = \begin{cases} 1 + P_1(jw) & |w| \leq \frac{\pi}{T_1} \\ P_1(jw) & \frac{\pi}{T_1} < |w| \leq \frac{2\pi}{T_1} \\ 0 & \text{otherwise} \end{cases}$$



$\Rightarrow p(t)$ has zero crossing at $\pm T_1, \pm 2T_1, \dots$ i.e., $p(\pm kT_1) = 0$

(De)Modulation and (De)Multiplexing

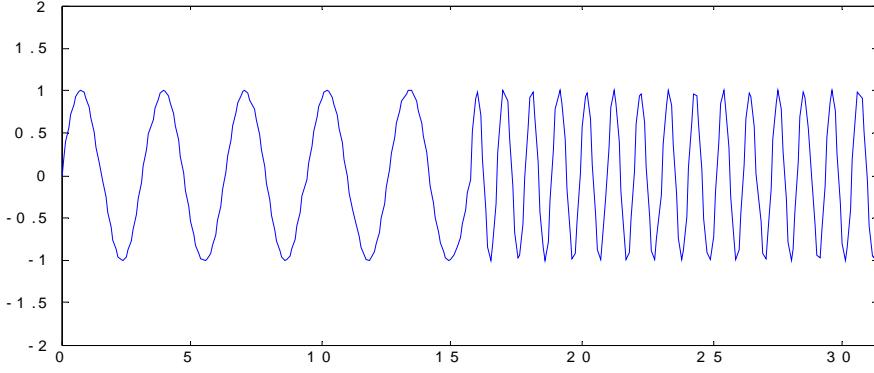
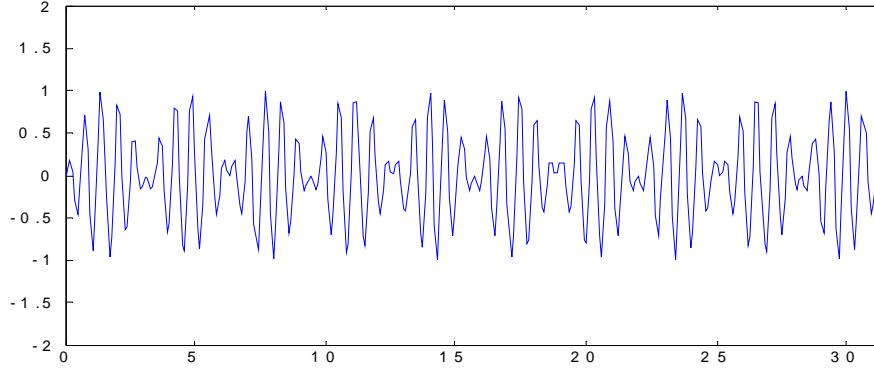
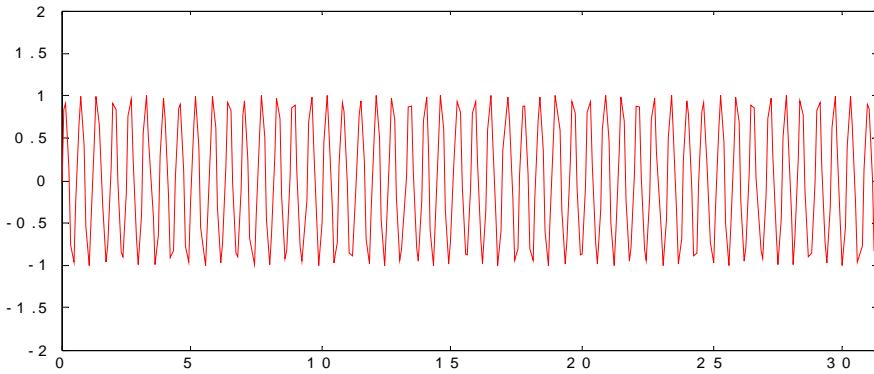
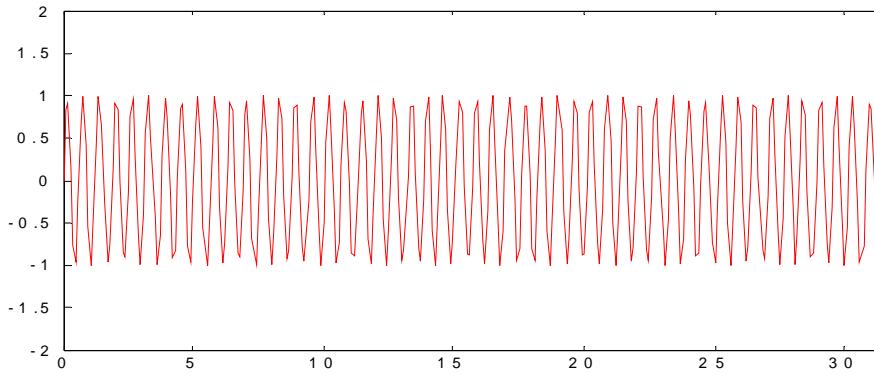
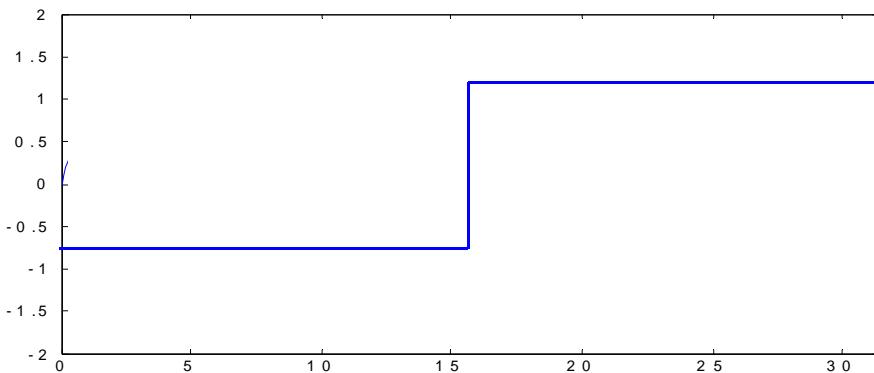
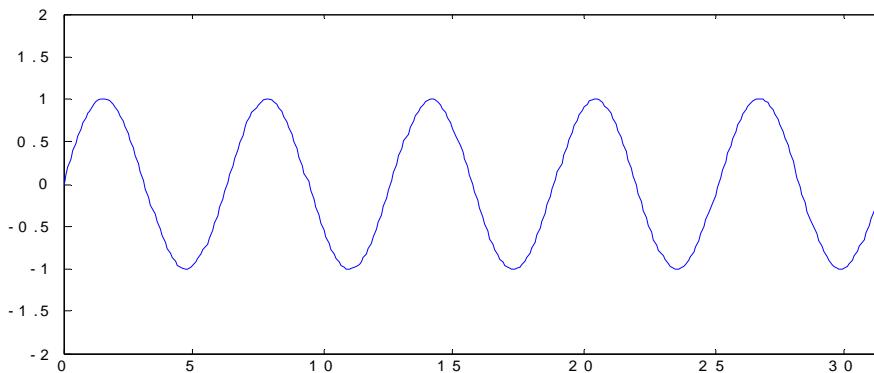
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Amplitude Modulation and Frequency Modulation

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■ Frequency Modulation (FM):

- The **modulating signals** is used to control the **frequency** of a **sinusoidal carrier**
- With sinusoidal AM, the peak amplitude of the **envelope** of the carrier directly depends on the **amplitude** of the **modulating signal $x(t)$** , which can have a large dynamic range.
- With FM, the **envelope** of the carrier is **constant**
- An **FM transmitter** can always operate at **peak power** and **amplitude variations** introduced over a transmission channel due to **additive disturbances** or **fading** can be eliminated at the receiver
- **FM** generally requires **greater bandwidth** than does sinusoidal **AM**

■ Angle Modulation:

$$c(t) = A \cos(w_c t + \theta_c) = A \cos \theta(t)$$

- **Phase Modulation:**

- Use the modulating signal $x(t)$ to vary the phase θ_c

$$y(t) = A \cos(\theta(t)) = A \cos(w_c t + \theta_c(t))$$

$$\theta_c(t) = \theta_0 + k_p x(t)$$

$$\frac{d\theta(t)}{dt} = w_c + k_p \frac{dx(t)}{dt}$$

- **Frequency Modulation:**

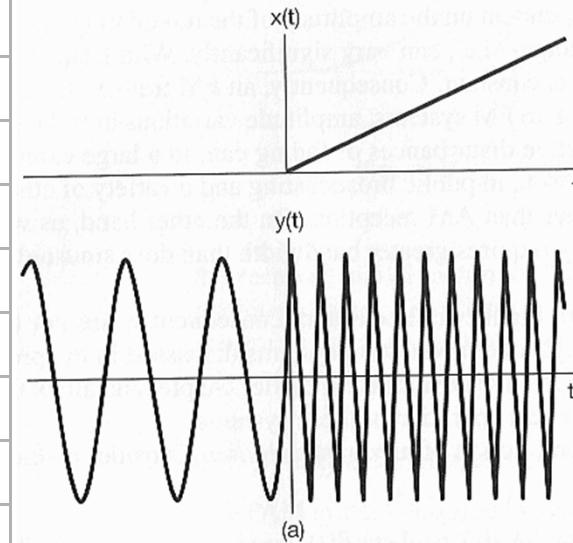
- Use the modulating signal $x(t)$ to vary the derivative of the angle

$$y(t) = A \cos(\theta(t))$$

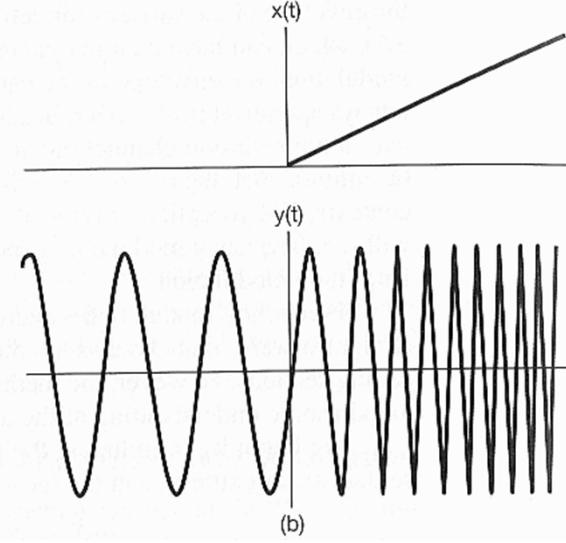
$$\frac{d\theta(t)}{dt} = w_c + k_f x(t)$$

■ Phase & Frequency Modulation:

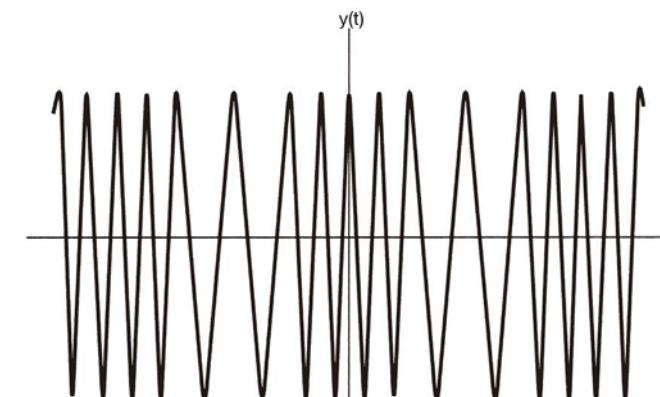
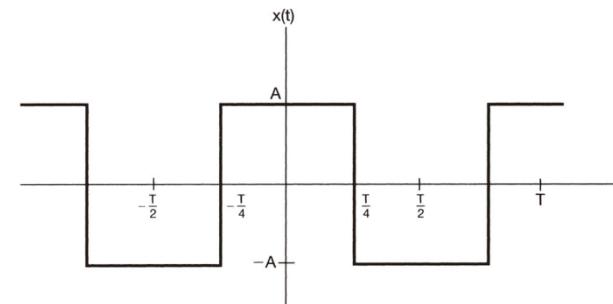
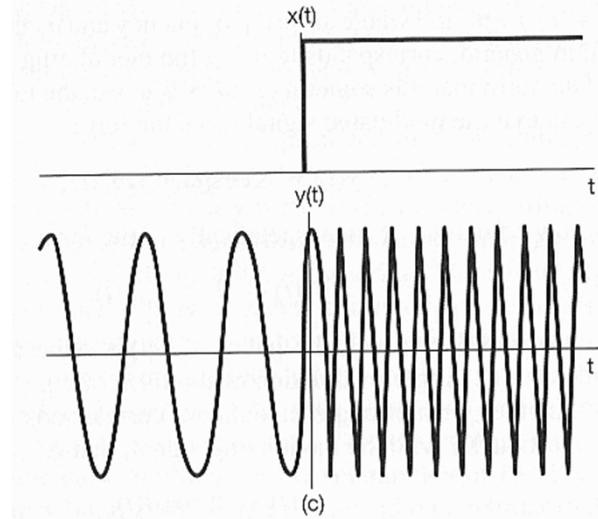
phase modulation



frequency modulation



frequency modulation



$$\frac{d\theta(t)}{dt} = w_c + k_p \frac{dx(t)}{dt}$$

$$\frac{d\theta(t)}{dt} = w_c + k_f x(t)$$

■ Instantaneous Frequency:

$$y(t) = A \cos(\theta(t)) \Rightarrow w_i = \frac{d\theta(t)}{dt}$$

- If $y(t)$ is truly sinusoidal:

$$\theta(t) = w_c t + \theta_0$$

$$w_i = w_c$$

- Phase Modulation:

$$w_i = \frac{d\theta(t)}{dt} = w_c + k_p \frac{dx(t)}{dt}$$

- Frequency Modulation:

$$w_i = \frac{d\theta(t)}{dt} = w_c + k_f x(t)$$

■ Wideband FM:

$$c(t) = A \cos(w_c t + \theta_c) = A \cos \theta(t)$$

■ Narrowband FM:

$$x(t) = A \cos(w_m t)$$

- Frequency Modulation with

$$w_i = \frac{d\theta(t)}{dt} = w_c + k_f x(t)$$

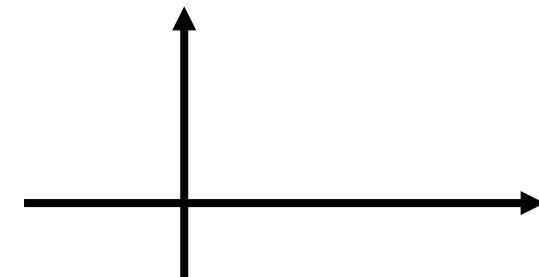
- Instantaneous Frequency:

$$w_i(t) = \frac{d\theta(t)}{dt} = w_c + k_f A \cos(w_m t)$$

$$\Rightarrow w_c - k_f A \leq w_i(t) \leq w_c + k_f A$$

$$\Rightarrow \Delta w \triangleq k_f A$$

$$\Rightarrow w_i(t) = w_c + \Delta w \cos(w_m t)$$



■ Wideband FM:

$$x(t) = A \cos(w_m t)$$

■ Narrowband FM:

$$y(t) = \cos(\theta(t)) = \cos(w_c t + \theta_c(t))$$

$$\frac{d\theta(t)}{dt} = w_c + k_f x(t)$$

$$\Delta w \triangleq k_f A$$

$$\Rightarrow y(t) = \cos\left(w_c t + k_f \int x(t) dt\right)$$

$$= \cos\left(w_c t + k_f \frac{A}{w_m} \sin(w_m t) + \theta_0\right)$$

$$= \cos\left(w_c t + \frac{\Delta w}{w_m} \sin(w_m t)\right)$$

let $\theta_0 = 0$

- Modulation Index for FM:

$$m \triangleq \frac{\Delta w}{w_m}$$

- Which m is small \rightarrow narrowband FM

■ Narrowband FM:

$$\cos(A + B) = \cos(A)\cos(B) - \sin(A)\sin(B)$$

$$\Rightarrow y(t) = \cos(w_c t + m \sin(w_m t))$$

$$\text{or } y(t) = \cos(w_c t) \cos(m \sin(w_m t)) - \sin(w_c t) \sin(m \sin(w_m t))$$

- When m is sufficiently small ($\ll \pi/2$)

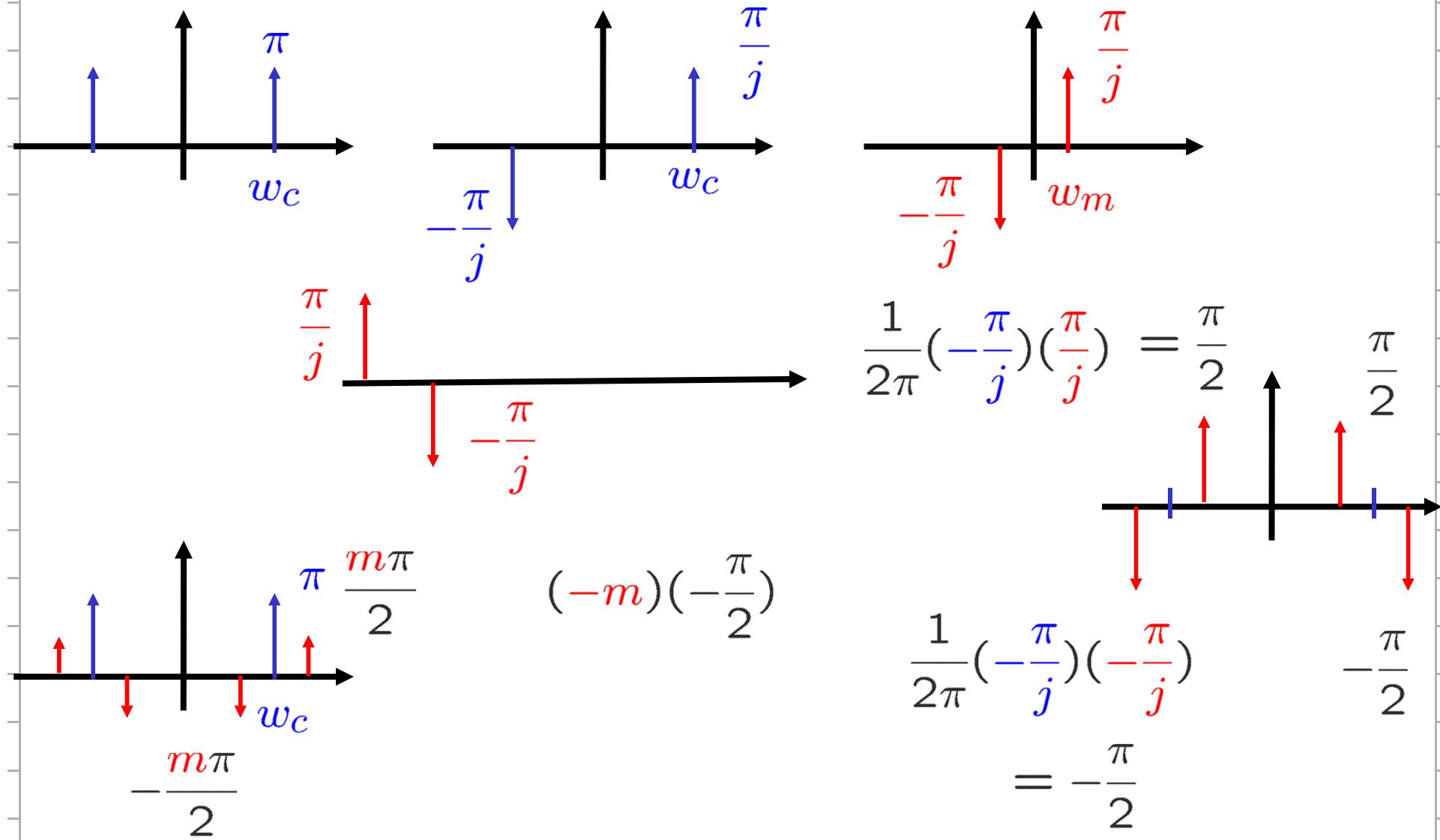
if $0 < \theta \ll 1$

$$\begin{aligned} \Rightarrow \cos(m \sin(w_m t)) &\approx 1 \\ \sin(m \sin(w_m t)) &\approx m \sin(w_m t) \end{aligned} \quad \Rightarrow \begin{aligned} \cos(\theta) &\approx 1 \\ \sin(\theta) &\approx \theta \end{aligned}$$

$$\Rightarrow y(t) \approx \cos(w_c t) - m \sin(w_m t) \sin(w_c t)$$

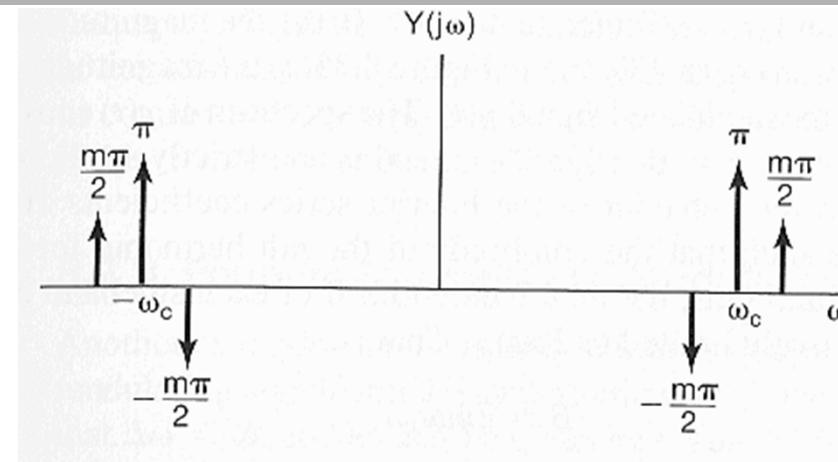
■ Narrowband FM:

$$\Rightarrow y(t) \approx \cos(w_c t) - m \sin(w_m t) \sin(w_c t)$$



■ Narrowband FM:

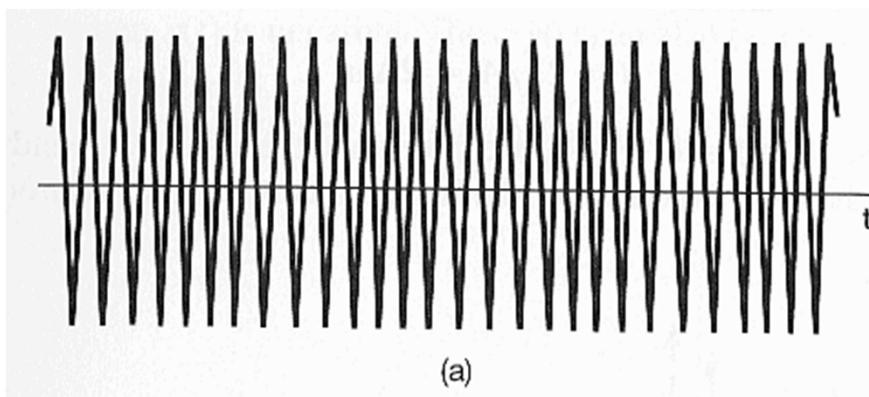
$$x(t) = A \cos(w_m t)$$



Approximate spectrum for narrowband FM

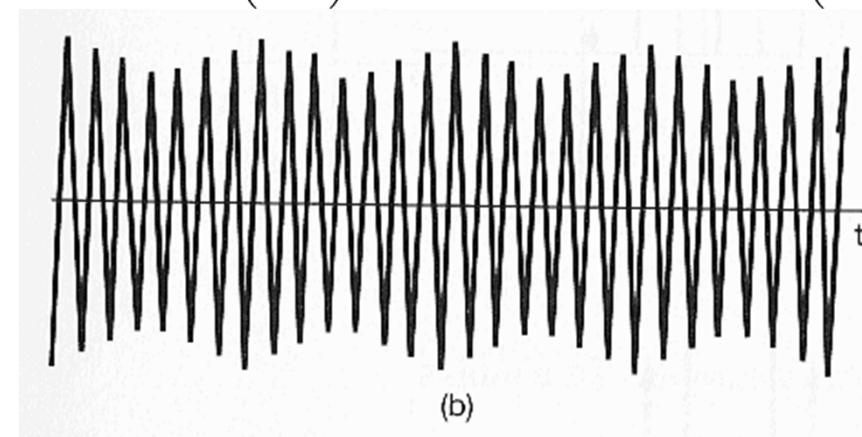
$$y(t) \approx \cos(w_c t) - m \sin(w_m t) \sin(w_c t)$$

$$y_2(t) = \cos(w_c t) + m \cos(w_m t) \cos(w_c t)$$



(a)

Narrowband FM



(b)

AM-Double Sideband/with carrier

$$m \triangleq \frac{\Delta\omega}{w_m}$$

■ Wideband FM:

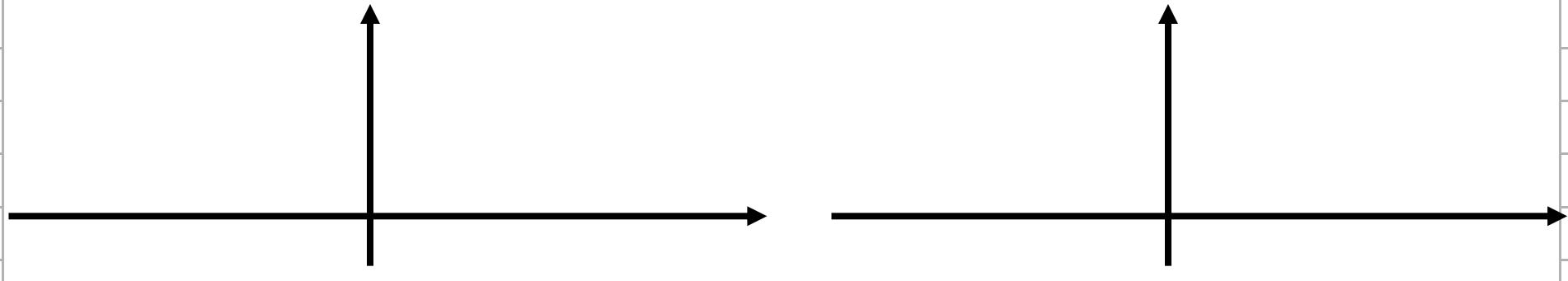
- When m is large

$$y(t) = \cos(w_c t) \cos(m \sin(w_m t)) - \sin(w_c t) \sin(m \sin(w_m t))$$

Periodic signals with fundamental frequency ω_m

$$\cos(m \sin(w_m t)) = J_0(m) + \sum_{n \text{ even}}^{\infty} 2J_n(m) \cos(n w_m t)$$

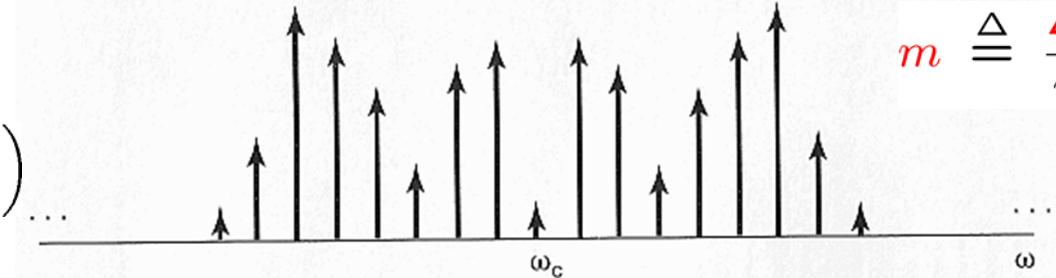
$$\sin(m \sin(w_m t)) = \sum_{n \text{ odd}}^{\infty} 2J_n(m) \sin(n w_m t)$$



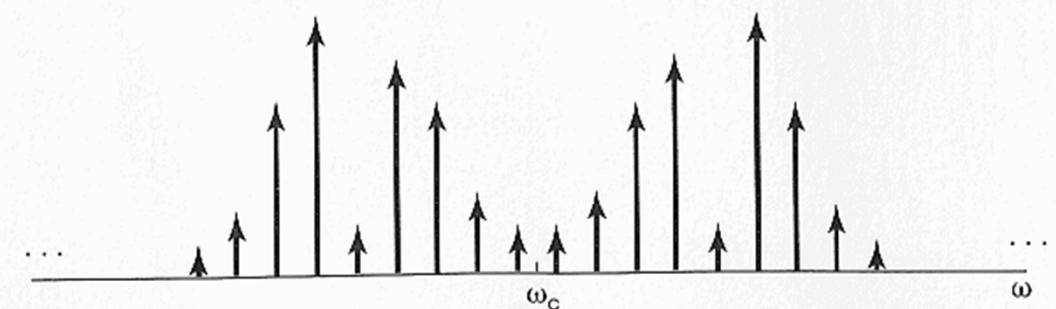
■ Magnitude of Spectrum of Wideband FM:

$$\Delta w \triangleq k_f A$$

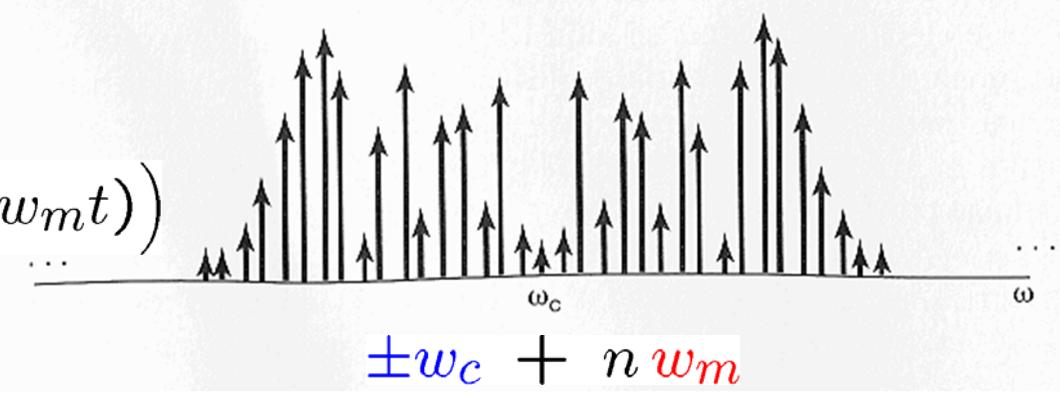
$$\cos(w_c t) \cos(m \sin(w_m t)) \dots$$



$$\sin(w_c t) \sin(m \sin(w_m t)) \dots$$



$$y(t) = \cos(w_c t + m \sin(w_m t)) \dots$$



$$\Rightarrow B \approx 2 m w_m = 2 k_f A = 2 \Delta w$$

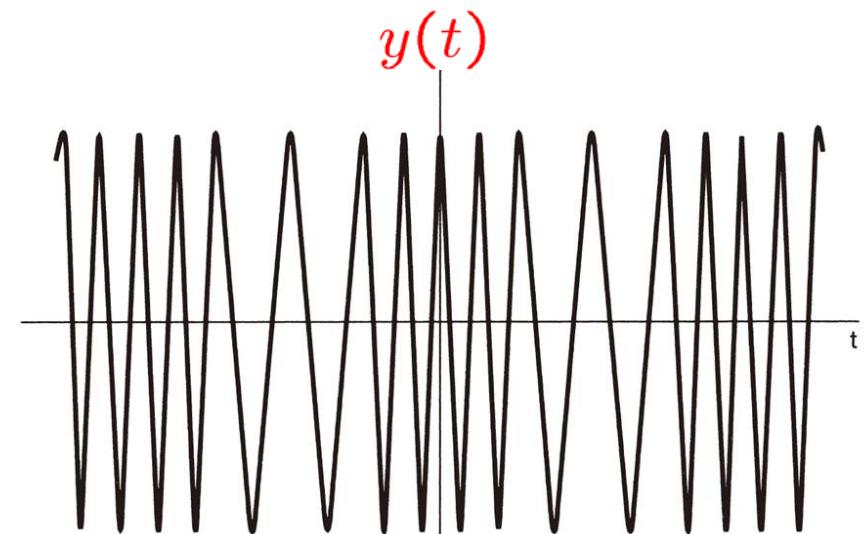
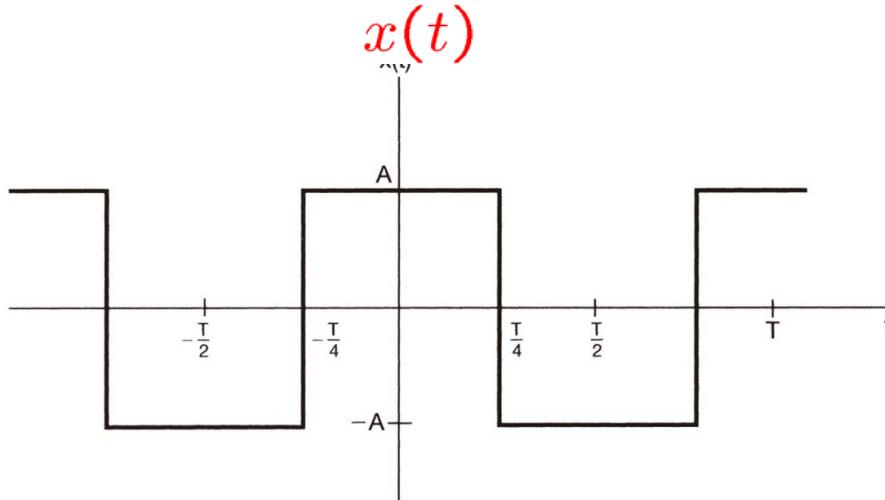
■ Periodic Square-Wave Modulating Signal:

$$\Delta w \triangleq k_f A$$

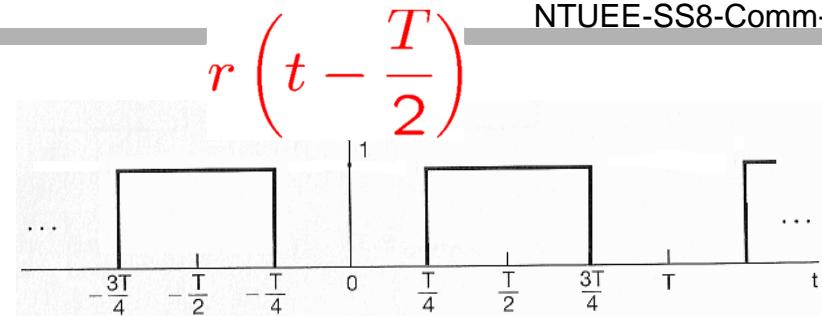
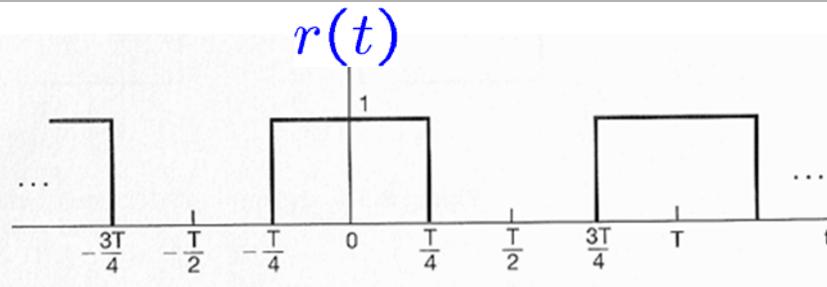
$$m \triangleq \frac{\Delta w}{w_m}$$

$$w_i(t) = w_c + k_f x(t) \quad k_f = 1 \Rightarrow \Delta w = A$$

- When $x(t) > 0$, $w_i(t) = w_c + \Delta w$
- When $x(t) < 0$, $w_i(t) = w_c - \Delta w$



Sinusoidal Frequency Modulation



$$\Rightarrow y(t) = r(t) \cos((\omega_c + \Delta\omega)t) + r\left(t - \frac{T}{2}\right) \cos((\omega_c - \Delta\omega)t)$$

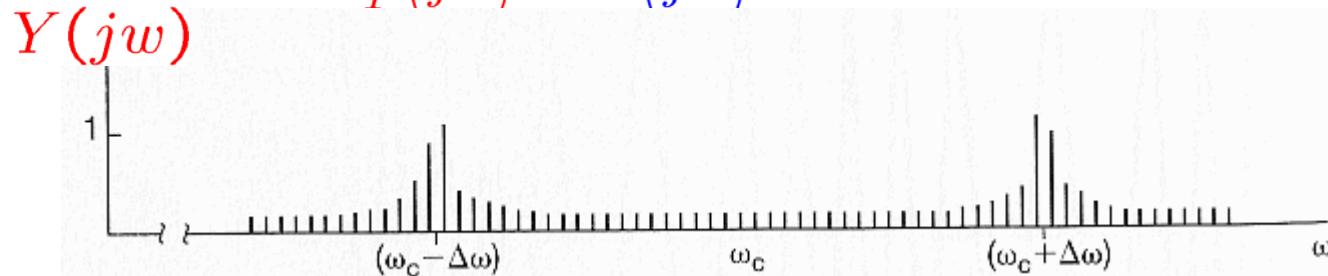
$$\Rightarrow Y(jw) = \frac{1}{2} [R(jw + j\omega_c + j\Delta\omega) + R(jw - j\omega_c - j\Delta\omega)]$$

$$+ \frac{1}{2} [R_T(jw + j\omega_c - j\Delta\omega) + R_T(jw - j\omega_c + j\Delta\omega)]$$

Ex 4.6

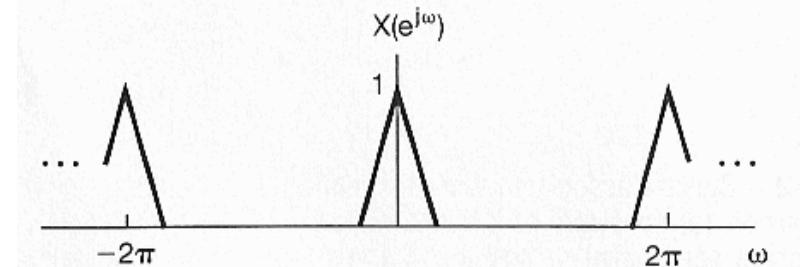
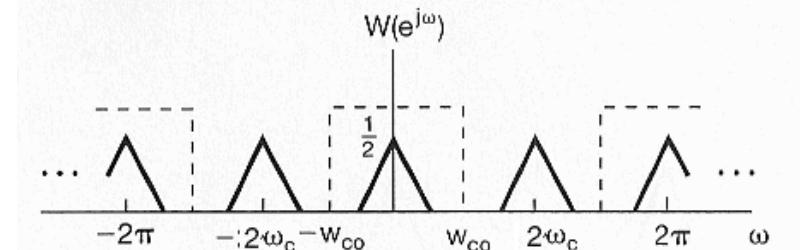
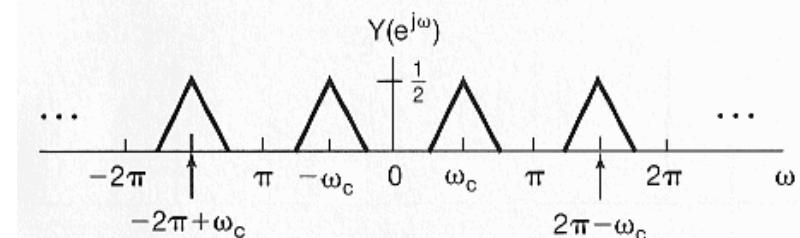
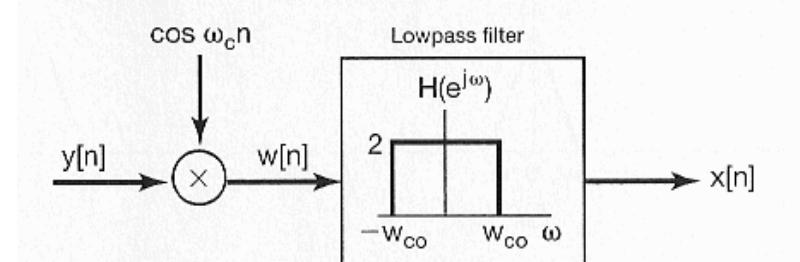
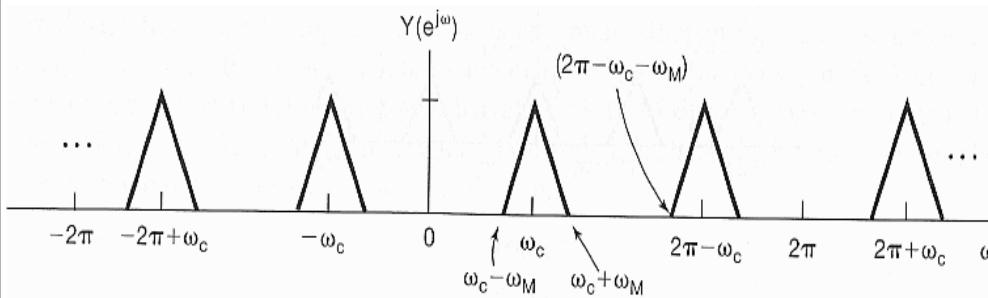
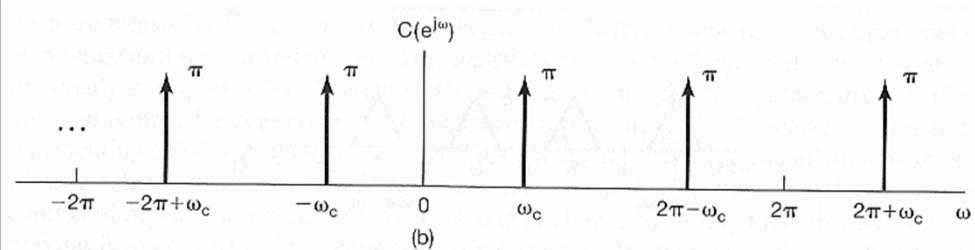
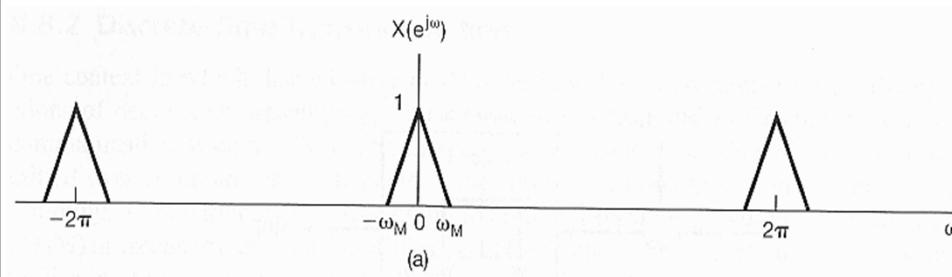
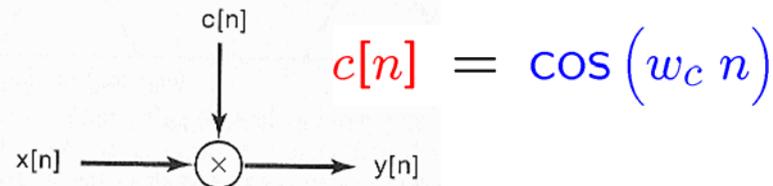
$$R(jw) = \sum_{k=-\infty}^{\infty} \frac{2}{2k+1} (-1)^k \delta\left(w - \frac{2\pi(2k+1)}{T}\right) + \pi\delta(w)$$

$$R_T(jw) = R(jw)e^{-jwT/2}$$



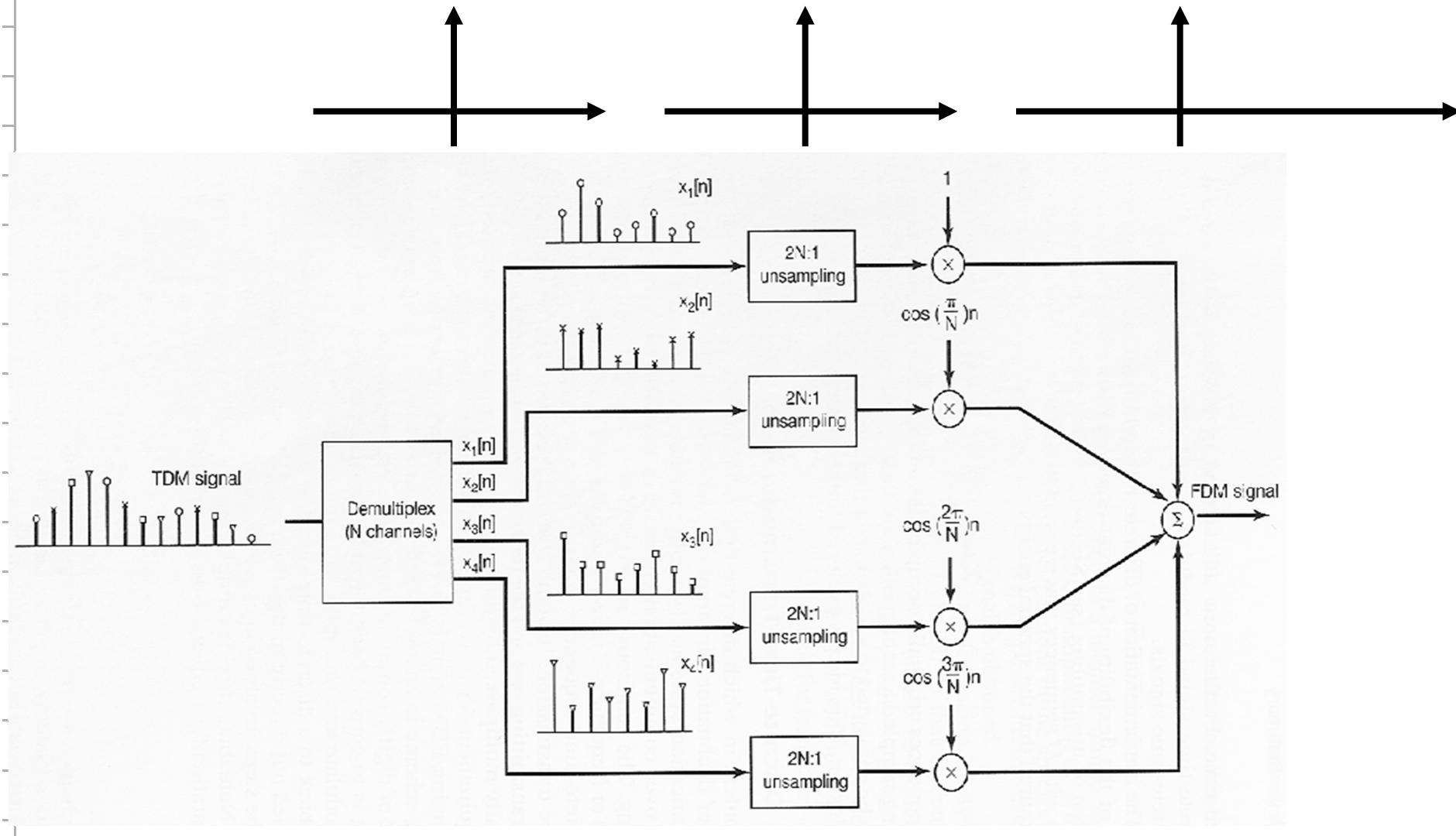
- Complex Exponential & Sinusoidal Amplitude Modulation & Demodulation
- Frequency-Division Multiplexing
- Single-Sideband Sinusoidal Amplitude Modulation
- Amplitude Modulation with a Pulse-Train Carrier
 - » Time-Division Multiplexing
- Pulse-Amplitude Modulation
- Sinusoidal Frequency Modulation
- Discrete-Time Modulation

■ DT Sinusoidal AM:



■ Transmodulation or Transmultiplexing:

- TDM to FDM



■ Higher Equivalent Sampling Rate: Up-sampling

