

Spring 2015

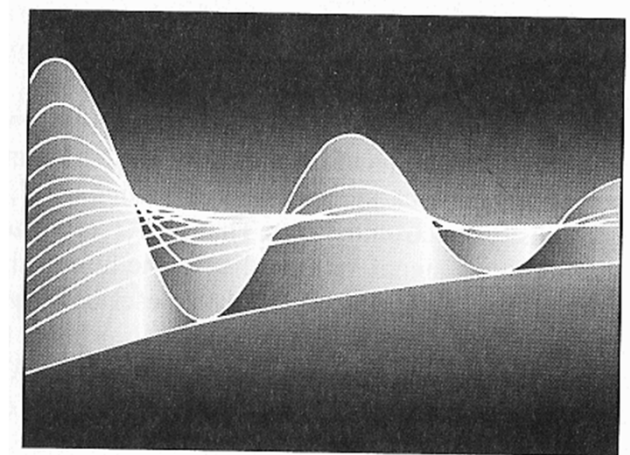
信號與系統 Signals and Systems

Chapter SS-6 Time & Frequency Characterization of Signals and Systems

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NTU-EE

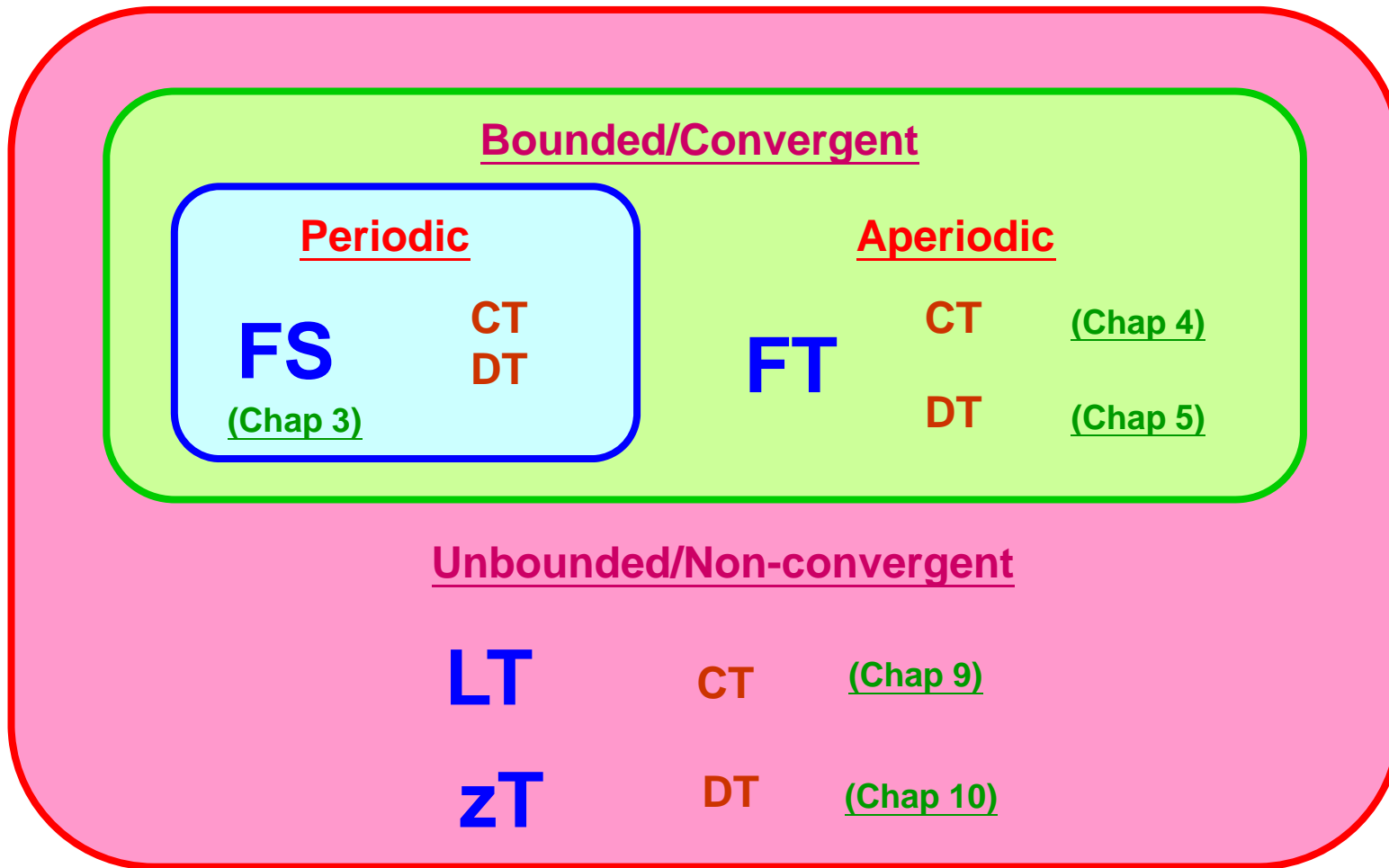
Feb15 – Jun15



Figures and images used in these lecture notes are adopted from
“Signals & Systems” by Alan V. Oppenheim and Alan S. Willsky, 1997

Introduction (Chap 1)

LTI & Convolution (Chap 2)



Time-Frequency (Chap 6)
CT-DT (Chap 7)

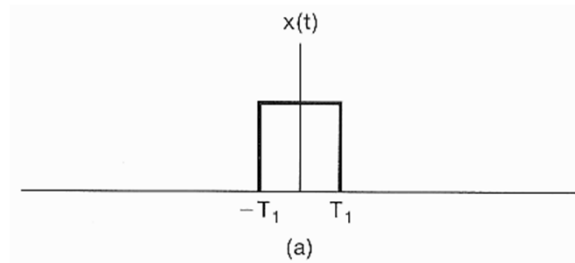
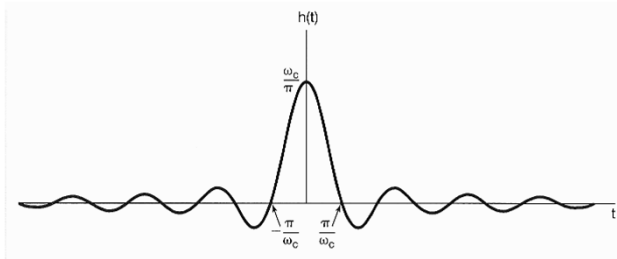
Communication (Chap 8)
Control (Chap 11)

Digital Signal Processing (dsp-8)

Fourier Series, Fourier Transform, Laplace Transform, z-Transform

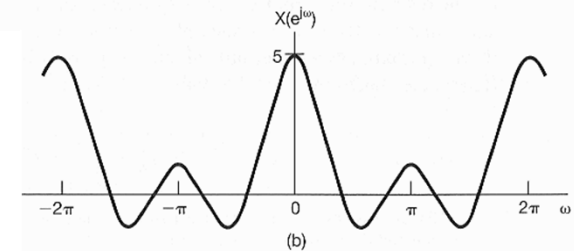
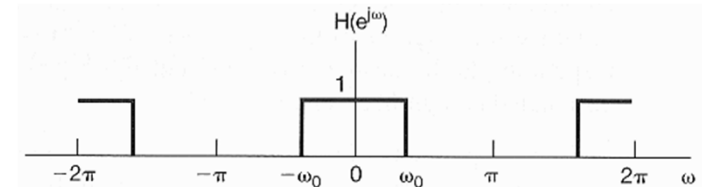
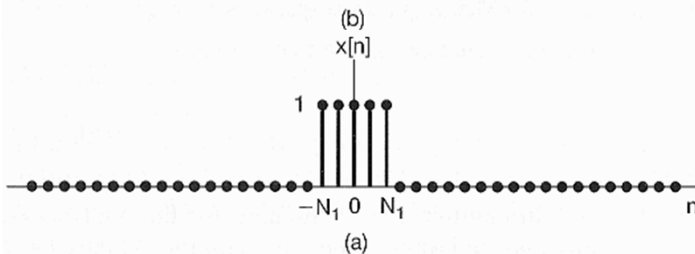
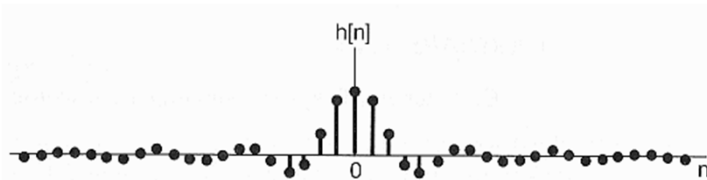
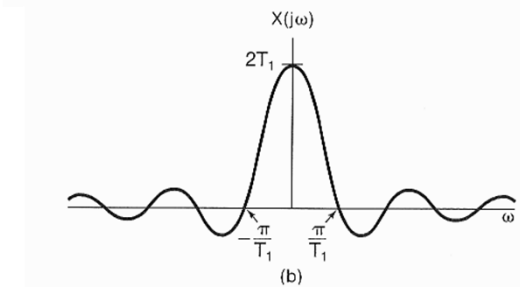
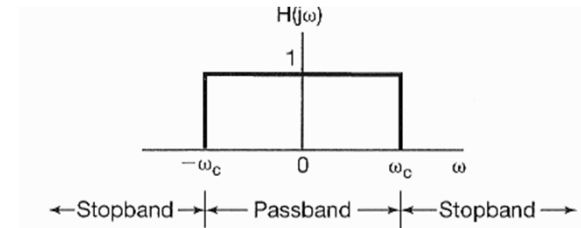
| | CT | | DT | |
|-------|------|-----------|------|-----------|
| | time | frequency | time | frequency |
| FS | | | | |
| FT | | | | |
| LT/zT | | | | |

Time-Domain & Frequency-Domain Characterization:



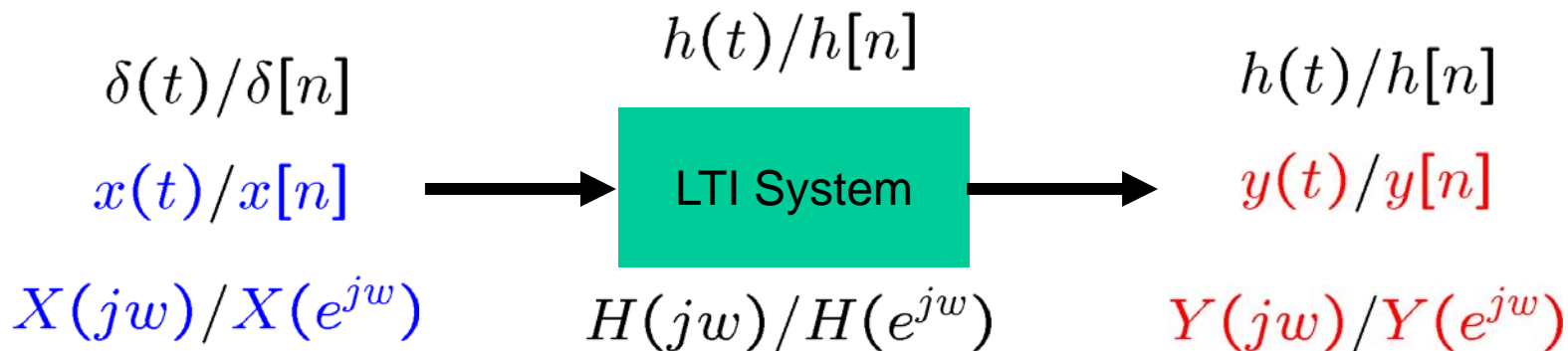
$$h(t) \xleftrightarrow{\mathcal{F}} H(j\omega)$$

$$h[n] \xleftrightarrow{\mathcal{F}} H(e^{j\omega})$$



Time-Domain & Frequency-Domain Characterization:

$$H(j\omega) = \int_{-\infty}^{\infty} h(t)e^{-j\omega t} dt \quad H(e^{j\omega}) = \sum_{n=-\infty}^{+\infty} h[n]e^{-j\omega n}$$



$$x(t) \xleftrightarrow{\mathcal{F}} X(j\omega) \quad h(t) \xleftrightarrow{\mathcal{F}} H(j\omega) \quad y(t) \xleftrightarrow{\mathcal{F}} Y(j\omega)$$

$$x[n] \xleftrightarrow{\mathcal{F}} X(e^{j\omega}) \quad h[n] \xleftrightarrow{\mathcal{F}} H(e^{j\omega}) \quad y[n] \xleftrightarrow{\mathcal{F}} Y(e^{j\omega})$$

$$y(t) = x(t) * h(t) \xleftrightarrow{\mathcal{F}} Y(j\omega) = X(j\omega)H(j\omega)$$

$$y[n] = x[n] * h[n] \xleftrightarrow{\mathcal{F}} Y(e^{j\omega}) = X(e^{j\omega})H(e^{j\omega})$$

Time-Domain

Frequency-Domain

Convolution
↔
Transformation

Differential Eqns
or
Difference Eqns

System Model
& Operations

Algebraic
Equations

Convolution
Multiplication

Techniques

Multiplication
Convolution

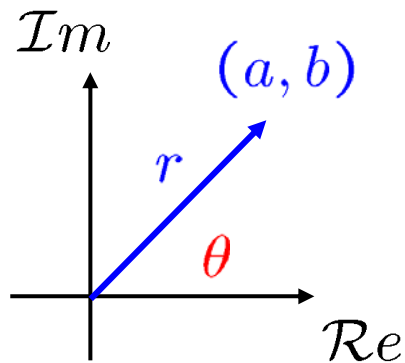
Time-Domain
Considerations

System
Design

Frequency-Domain
Considerations

- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems (p. 427)
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

▪ Magnitude & Phase Representation:



$$a + jb \Rightarrow \begin{cases} r = \sqrt{a^2 + b^2} \\ \tan(\theta) = \frac{b}{a} \end{cases}$$

$$\Rightarrow a + jb = r e^{j\theta}$$

$$|a + jb| = \sqrt{a^2 + b^2} \quad \left| \frac{1}{a + jb} \right| = \frac{1}{\sqrt{a^2 + b^2}}$$

$$\angle a + jb = \tan^{-1}\left(\frac{b}{a}\right) \quad \angle \frac{1}{a + jb} = -\tan^{-1}\left(\frac{b}{a}\right)$$

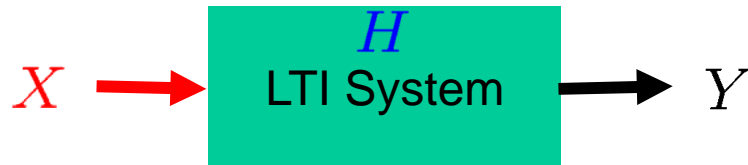
$$X(j\omega) = \text{Re}\{X(j\omega)\} + j \text{Im}\{X(j\omega)\} = |X(j\omega)| e^{j\angle X(j\omega)}$$

$$X(e^{j\omega}) = \text{Re}\{X(e^{j\omega})\} + j \text{Im}\{X(e^{j\omega})\} = |X(e^{j\omega})| e^{j\angle X(e^{j\omega})}$$

$|X(j\omega)|$ or $|X(e^{j\omega})|$: magnitude

$\angle X(j\omega)$ or $\angle X(e^{j\omega})$: phase angle

▪ Magnitude Distortion & Phase Distortion: (p. 428)



$$Y(j\omega) = X(j\omega) H(j\omega)$$

$$Y(e^{j\omega}) = X(e^{j\omega}) H(e^{j\omega})$$

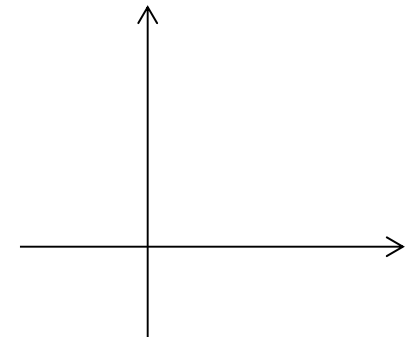
$$\begin{aligned} \Rightarrow |Y(j\omega)| e^{j\angle Y(j\omega)} &= |X(j\omega)| e^{j\angle X(j\omega)} |H(j\omega)| e^{j\angle H(j\omega)} \\ &= |X(j\omega)| |H(j\omega)| e^{j(\angle X(j\omega) + \angle H(j\omega))} \end{aligned}$$

$$\Rightarrow \begin{cases} |Y(j\omega)| = |X(j\omega)| |H(j\omega)| & \text{magnitude distortion} \\ \angle Y(j\omega) = \angle X(j\omega) + \angle H(j\omega) & \text{phase distortion} \end{cases}$$

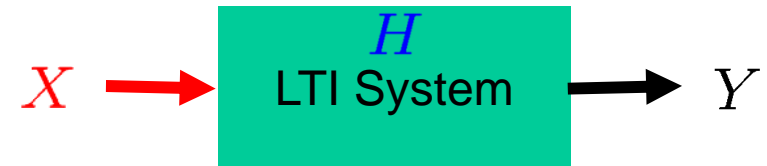
$$\Rightarrow \begin{cases} |Y(e^{j\omega})| = |X(e^{j\omega})| |H(e^{j\omega})| \\ \angle Y(e^{j\omega}) = \angle X(e^{j\omega}) + \angle H(e^{j\omega}) \end{cases}$$

$|H(j\omega)|$ or $|H(e^{j\omega})|$: gain of the system

$\angle H(j\omega)$ or $\angle H(e^{j\omega})$: phase shift of the system

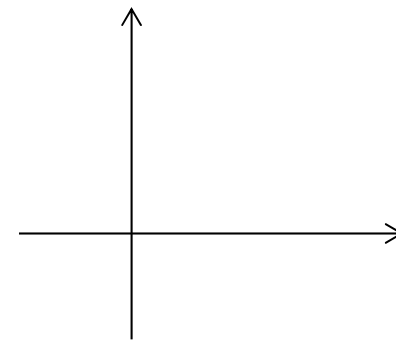


▪ Log-Magnitude & Phase Plots: (p. 436)



$$Y(j\omega) = X(j\omega) H(j\omega)$$

$$\Rightarrow \begin{cases} |Y(j\omega)| &= |X(j\omega)| |H(j\omega)| \\ \angle Y(j\omega) &= \angle X(j\omega) + \angle H(j\omega) \end{cases}$$



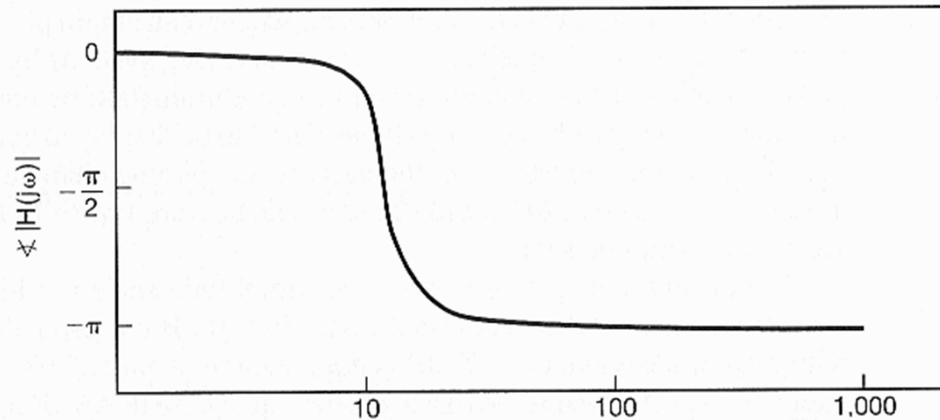
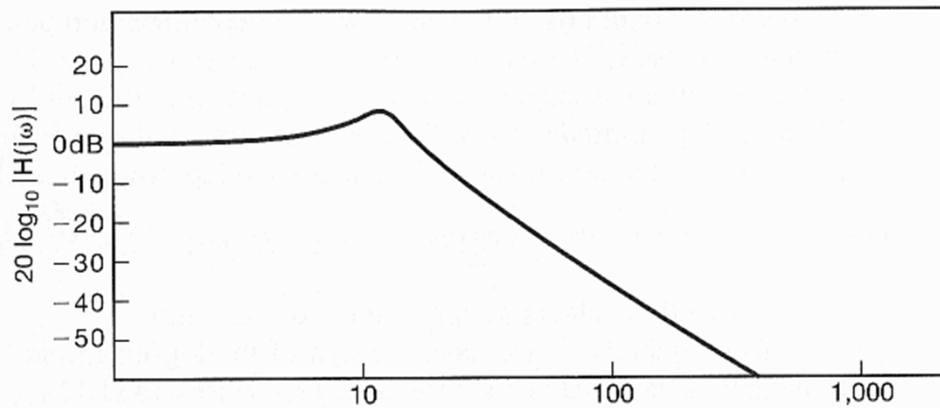
$$\Rightarrow \log |Y(j\omega)| = \log |X(j\omega)| + \log |H(j\omega)|$$

$$\Rightarrow 20 \log_{10} |Y(j\omega)| = 20 \log_{10} |X(j\omega)| + 20 \log_{10} |H(j\omega)|$$

$$\Rightarrow \begin{cases} 20 \log_{10} (1) &= 0 \text{ dB} \\ 20 \log_{10} (10) &= 20 \text{ dB} \\ 20 \log_{10} (0.1) &= -20 \text{ dB} \end{cases}$$

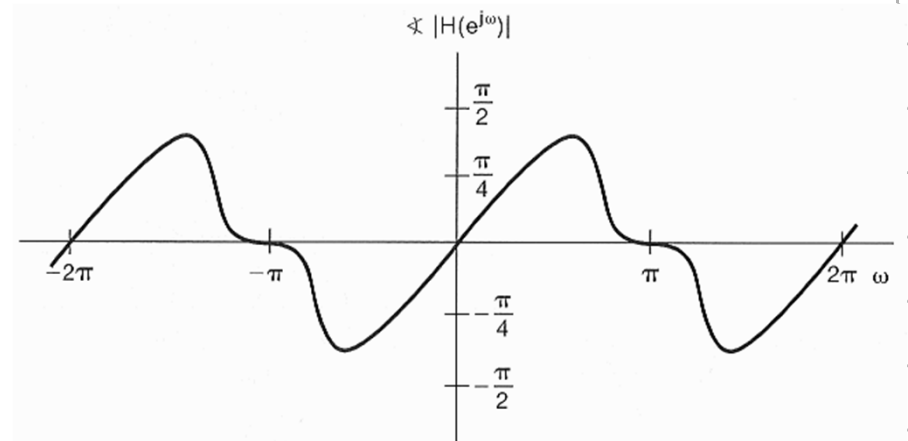
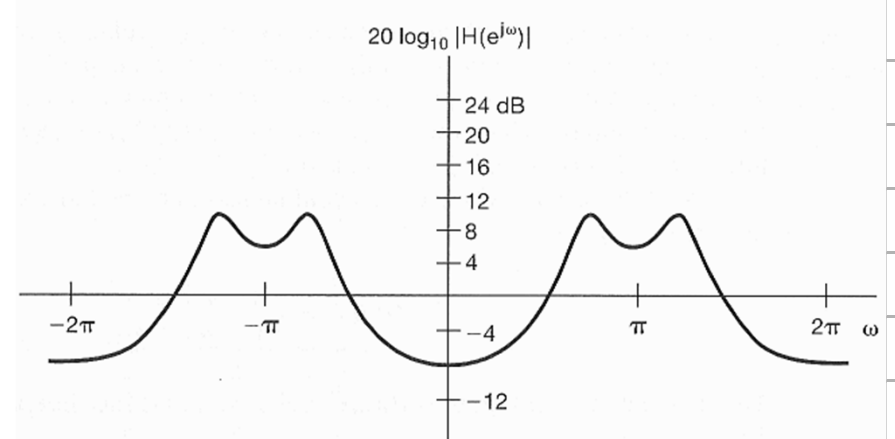
■ Log-Magnitude & Bode Plots: (p. 436)

Continuous-Time Bode plot



$\log(\omega)$, $\omega : 0 \leftrightarrow \infty$

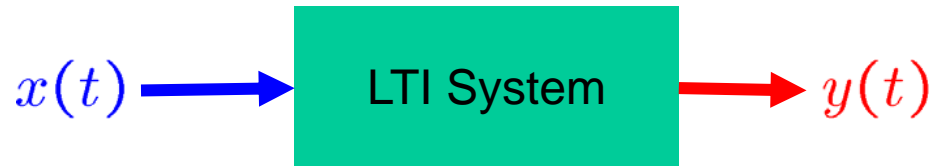
Discrete-Time Bode plot



(ω) , $\omega : -\pi \leftrightarrow \pi$

- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters [\(p. 448\)](#)
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

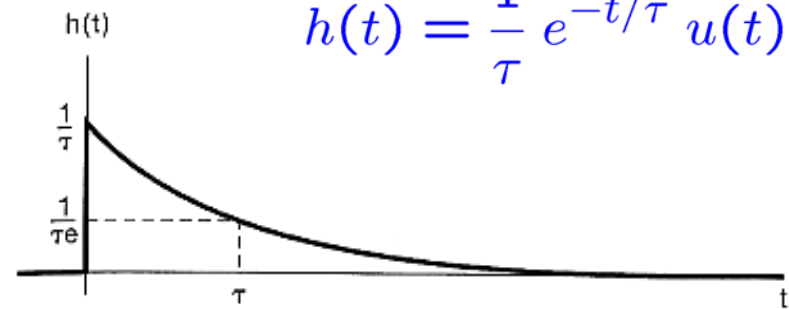
▪ First-Order CT Systems: (p. 448)



$$Y(j\omega) = X(j\omega)H(j\omega)$$

$$\tau \frac{d}{dt}y(t) + y(t) = x(t)$$

$$h(t) = \frac{1}{\tau} e^{-t/\tau} u(t)$$

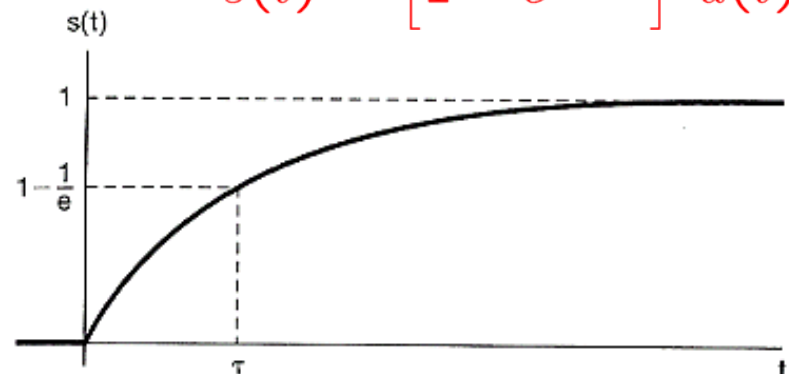


(a)

$$\Rightarrow H(j\omega) = \frac{1}{j\omega\tau + 1}$$

$$\Rightarrow h(t) = \frac{1}{\tau} e^{-t/\tau} u(t)$$

$$s(t) = [1 - e^{-t/\tau}] u(t)$$



(b) Time Constant

$$\begin{aligned} \Rightarrow s(t) &= h(t) * u(t) \\ &= [1 - e^{-t/\tau}] u(t) \end{aligned}$$

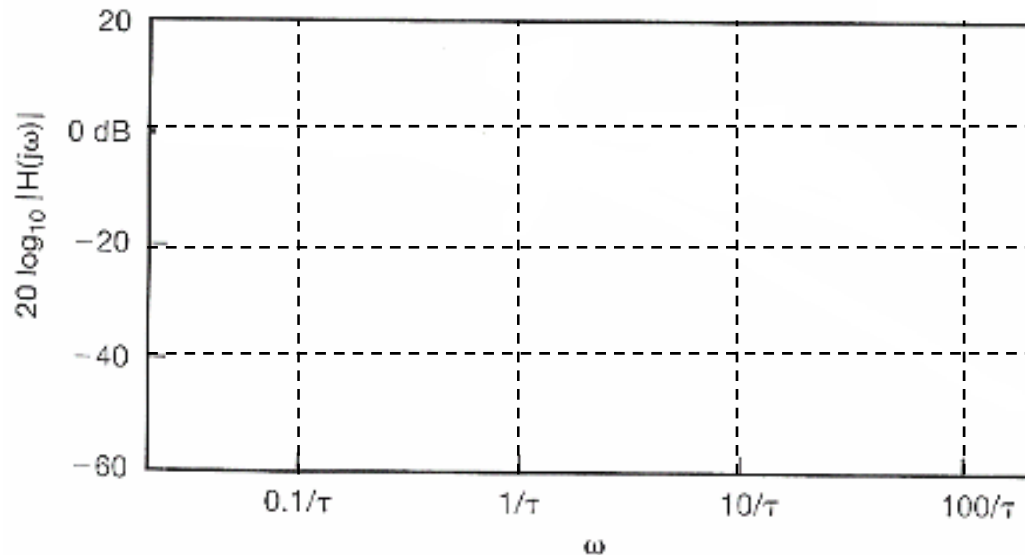
■ First-Order CT Systems:

$$H(j\omega) = \frac{1}{j\omega\tau + 1}$$

$$|H(j\omega)| = \frac{1}{\sqrt{(\omega\tau)^2 + 1}}$$

$$20 \log_{10} |H(j\omega)| = -10 \log_{10} [(\omega\tau)^2 + 1]$$

$$\approx \begin{cases} -10 \log_{10} [(\omega\tau)^2 + 1] = 0 & \omega \ll \frac{1}{\tau} \\ -10 \log_{10} [(\omega\tau)^2 + 1] = -10 \log_{10}(2) \approx -3dB & \omega = \frac{1}{\tau} \\ -10 \log_{10} [(\omega\tau)^2 + 1] = -20 \log_{10}(\omega\tau) & \omega \gg \frac{1}{\tau} \\ = -20 \log_{10}(\omega) - 20 \log_{10}(\tau) & \end{cases}$$

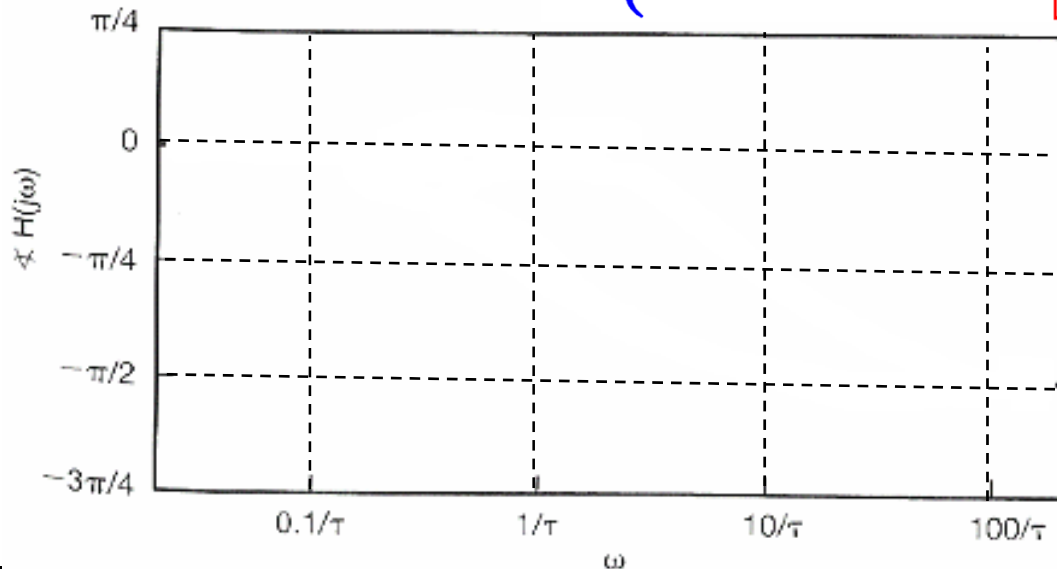


■ First-Order CT Systems:

$\angle H(j\omega) = -\tan^{-1}(\omega\tau)$

$H(j\omega) = \frac{1}{j\omega\tau + 1}$

$$\approx \begin{cases} 0 & \omega \leq \frac{0.1}{\tau} \\ -\frac{\pi}{4} & \omega = \frac{1}{\tau} \\ -\frac{\pi}{2} & \omega \geq \frac{10}{\tau} \\ -\left(\frac{\pi}{4}\right)[\log_{10}(\omega\tau) + 1] & \frac{0.1}{\tau} \leq \omega \leq \frac{10}{\tau} \\ = -\left(\frac{\pi}{4}\right) \left[\log_{10}(\omega) + \log_{10}(\tau) + 1 \right] & \end{cases}$$



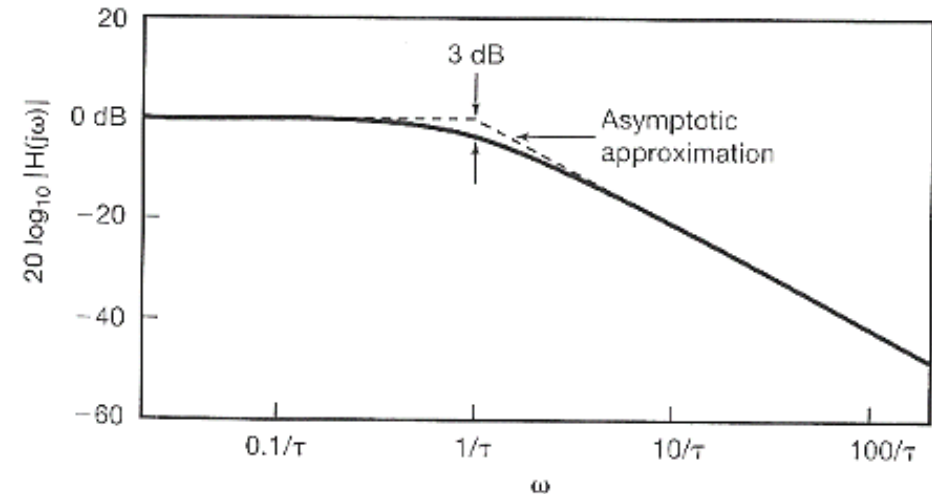
$\tan^{-1}(x) = x - \frac{x^3}{3} + \frac{x^5}{5} - \dots$

▪ First-Order CT Systems:

$$H(j\omega) = \frac{1}{j\omega\tau + 1}$$

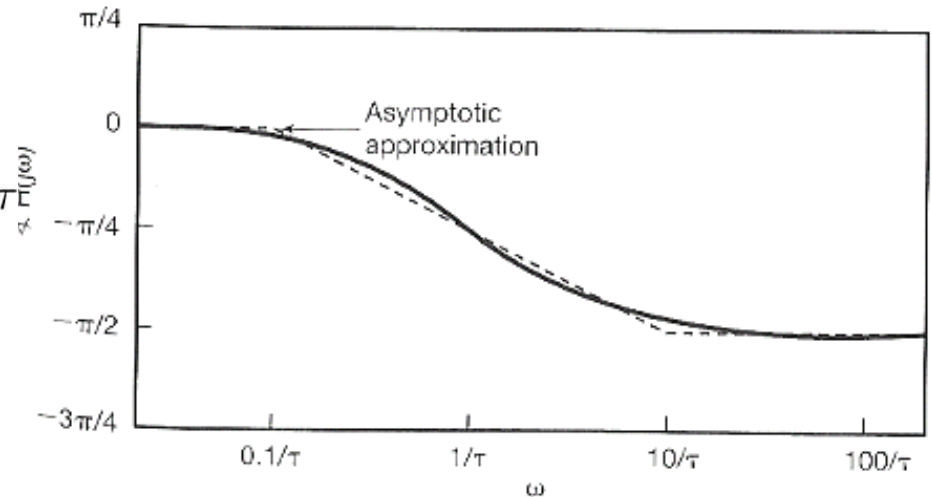
$$20 \log_{10} |H(j\omega)| =$$

$$\begin{cases} 0 & \omega \ll 1/\tau \\ -10 \log_{10}(2) \approx -3dB & \omega = 1/\tau \\ -20 \log_{10}(\omega\tau) & \omega \gg 1/\tau \\ = -20 \log_{10}(\omega) - 20 \log_{10}(\tau) \end{cases}$$



$$\angle H(j\omega) =$$

$$\begin{cases} 0 & \omega \leq 0.1/\tau \\ -(\pi/4)[\log_{10}(\omega\tau) + 1] & 0.1/\tau \leq \omega \leq 10/\tau \\ = -(\pi/4) [\log_{10}(\omega) + \log_{10}(\tau) + 1] \\ -\pi/4 & \omega = 1/\tau \\ -\pi/2 & \omega \geq 10/\tau \end{cases}$$



■ Second-Order CT Systems: (p. 451)

$$\frac{d^2}{dt^2}y(t) + 2\zeta\omega_n \frac{d}{dt}y(t) + \omega_n^2 y(t) = \omega_n^2 x(t)$$

$$\begin{aligned}\Rightarrow H(j\omega) &= \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2} \\ &= \frac{1}{(j\frac{\omega}{\omega_n})^2 + 2\zeta(j\frac{\omega}{\omega_n}) + 1}\end{aligned}$$

$$\Rightarrow H(j\omega) = \frac{\omega_n^2}{(j\omega - c_1)(j\omega - c_2)}$$

$$\begin{cases} c_1 = -\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1} \\ c_2 = -\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1} \end{cases}$$

■ Second-Order CT Systems:

$$\Rightarrow H(j\omega) = \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2}$$

$$H(j\omega) = \frac{1}{(j\frac{\omega}{\omega_n})^2 + 2\zeta(j\frac{\omega}{\omega_n}) + 1}$$

ζ : damping ratio

ω_n : undamped natural frequency

$\left\{ \begin{array}{l} 0 < \zeta < 1 : \text{ underdamped} \\ \zeta = 1 : \text{ critically damped} \\ \zeta > 1 : \text{ overdamped} \end{array} \right.$

- Second-Order CT Systems: $H(jw) = \frac{w_n^2}{(jw - c_1)(jw - c_2)}$
- For $\zeta = 1 \Rightarrow c_1 = c_2 = -w_n$:

$$\Rightarrow H(jw) = \frac{w_n^2}{(jw + w_n)^2}$$

$$\Rightarrow h(t) = w_n^2 t e^{-w_n t} u(t)$$

- For $\zeta \neq 1 \Rightarrow c_1 \neq c_2$:

$$\Rightarrow H(jw) = \frac{M}{jw - c_1} - \frac{M}{jw - c_2}$$

$$M = \frac{w_n}{2\sqrt{\zeta^2 - 1}}$$

$$\Rightarrow h(t) = M [e^{c_1 t} - e^{c_2 t}] u(t)$$

■ Second-Order CT Systems:

$$M = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}}$$

- For $0 < \zeta < 1$, c_1, c_2 : complex:

$$H(j\omega) = \frac{1}{(j\frac{\omega}{\omega_n})^2 + 2\zeta(j\frac{\omega}{\omega_n}) + 1} = \frac{\omega_n^2}{(j\omega - c_1)(j\omega - c_2)}$$

$$\Rightarrow h(t) = M \left[e^{c_1 t} - e^{c_2 t} \right] u(t) \quad \begin{cases} c_1 = -\zeta\omega_n + j\omega_n\sqrt{1-\zeta^2} \\ c_2 = -\zeta\omega_n - j\omega_n\sqrt{1-\zeta^2} \end{cases}$$

$$= \frac{\omega_n e^{-\zeta\omega_n t}}{2j\sqrt{1-\zeta^2}} \left\{ e^{j(\omega_n\sqrt{1-\zeta^2})t} - e^{-j(\omega_n\sqrt{1-\zeta^2})t} \right\} u(t)$$

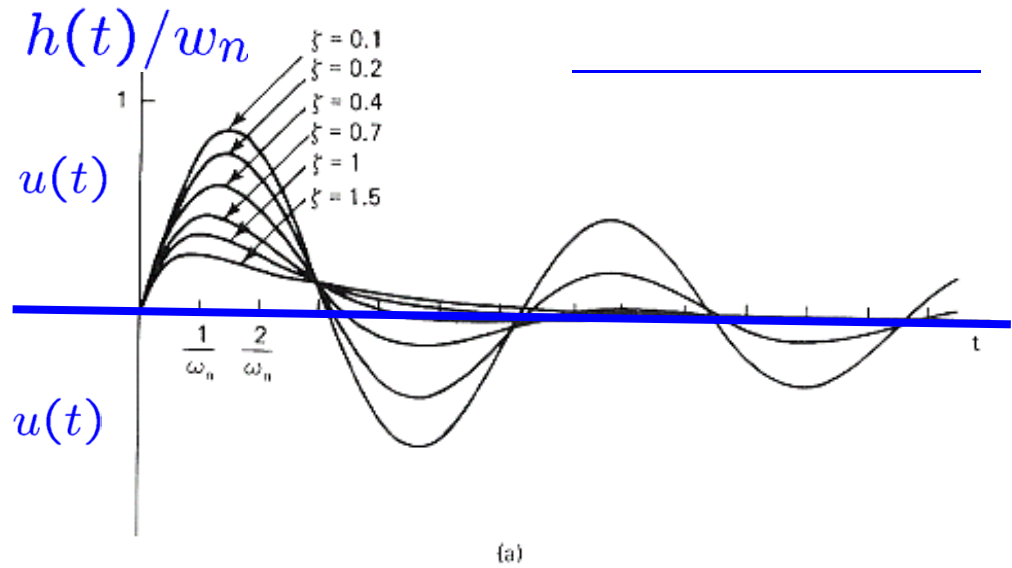
$$= \frac{\omega_n e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} \left[\sin \left((\omega_n\sqrt{1-\zeta^2})t \right) \right] u(t)$$

$$\Rightarrow s(t) = h(t) * u(t) = \left\{ 1 + M \left[\frac{e^{c_1 t}}{c_1} - \frac{e^{c_2 t}}{c_2} \right] \right\} u(t) \quad \zeta \neq 1$$

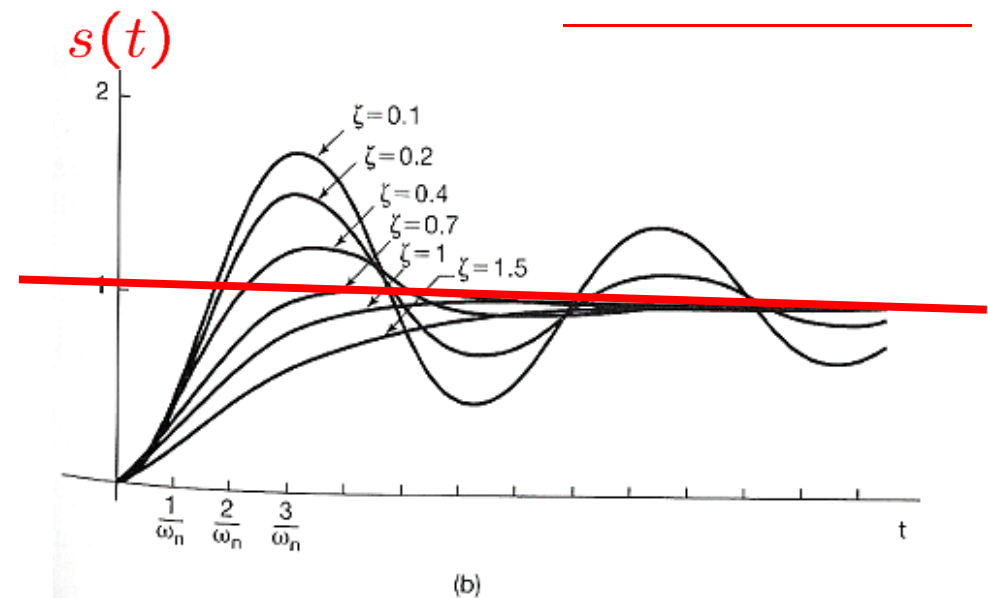
■ Second-Order CT Systems:

$$h(t) = \frac{w_n e^{-\zeta w_n t}}{\sqrt{1 - \zeta^2}} \left[\sin \left((w_n \sqrt{1 - \zeta^2}) t \right) \right] u(t)$$

$$\frac{h(t)}{w_n} = \frac{e^{-\zeta w_n t}}{\sqrt{1 - \zeta^2}} \left[\sin \left((w_n \sqrt{1 - \zeta^2}) t \right) \right] u(t)$$



$$s(t) = \left\{ 1 + M \left[\frac{e^{c_1 t}}{c_1} - \frac{e^{c_2 t}}{c_2} \right] \right\} u(t)$$



▪ **Second-Order CT Systems:** $H(j\omega) = \frac{1}{(j\frac{\omega}{\omega_n})^2 + 2\zeta(j\frac{\omega}{\omega_n}) + 1}$

$$|H(j\omega)| = \frac{1}{\sqrt{\left[1 - \left(\frac{\omega}{\omega_n}\right)^2\right]^2 + 4\zeta^2 \left(\frac{\omega}{\omega_n}\right)^2}}$$

$$20 \log_{10} |H(j\omega)| = -10 \log_{10} \left\{ \left[1 - \left(\frac{\omega}{\omega_n}\right)^2\right]^2 + 4\zeta^2 \left(\frac{\omega}{\omega_n}\right)^2 \right\}$$

$$\left\{ \left[1 - \left(\frac{\omega}{\omega_n}\right)^2\right]^2 + 4\zeta^2 \left(\frac{\omega}{\omega_n}\right)^2 \right\} \quad \left\{ \left[1 - \left(\frac{\omega}{\omega_n}\right)^2\right]^2 + 4\zeta^2 \left(\frac{\omega}{\omega_n}\right)^2 \right\}$$

$$Q = \frac{1}{2\zeta} \approx \begin{cases} 0 & \omega \ll \omega_n \\ -20 \log_{10}(2\zeta) & \omega = \omega_n \\ -40 \log_{10}(\omega) + 40 \log_{10}(\omega_n) & \omega \gg \omega_n \end{cases}$$

$$|H(jw)| = \frac{1}{\sqrt{\left[1 - \left(\frac{w}{w_n}\right)^2\right]^2 + 4\zeta^2 \left(\frac{w}{w_n}\right)^2}}$$

$$\Rightarrow \left(\frac{w}{w_n}\right)^4 - 2\left(\frac{w}{w_n}\right)^2 + 1 + 4\zeta^2 \left(\frac{w}{w_n}\right)^2 = \left(\frac{w}{w_n}\right)^4 + (4\zeta^2 - 2) \left(\frac{w}{w_n}\right)^2 + 1$$

$$\Rightarrow \frac{d}{dw} \left\{ \left(\frac{w}{w_n}\right)^4 + (4\zeta^2 - 2) \left(\frac{w}{w_n}\right)^2 + 1 \right\} = 0$$

$$\Rightarrow \left(\frac{4w^3}{w_n^4}\right) + (4\zeta^2 - 2) \left(\frac{2w}{w_n^2}\right) = 0$$

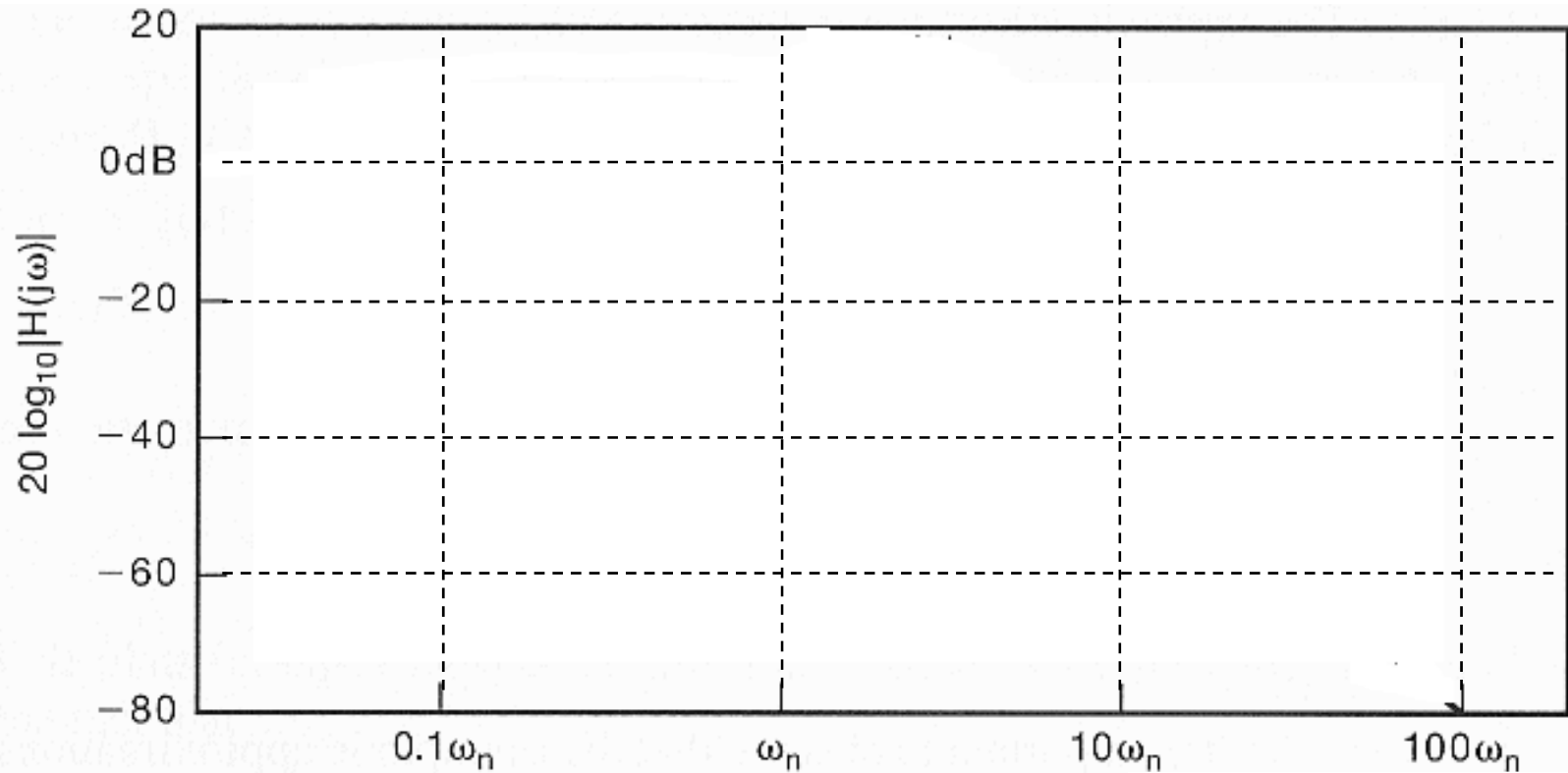
$$\Rightarrow w \left(w^2 + (2\zeta^2 - 1)w_n^2 \right) = 0$$

$$\Rightarrow w = 0, \pm \sqrt{1 - 2\zeta^2} w_n$$

- For $\zeta < \frac{\sqrt{2}}{2}$

$$\Rightarrow \max \{ |H(jw)| \} \text{ at } w_{\max} = w_n \sqrt{1 - 2\zeta^2} \quad |H(jw_{\max})| = \frac{1}{2\zeta \sqrt{1 - \zeta^2}}$$

- Second-Order CT Systems:** $H(j\omega) = \frac{1}{(j\frac{\omega}{\omega_n})^2 + 2\zeta(j\frac{\omega}{\omega_n}) + 1}$
- $$Q = \frac{1}{2\zeta}$$
- $$\begin{cases} 0 & \omega \ll \omega_n \\ -20 \log_{10}(2\zeta) & \omega = \omega_n \\ -40 \log_{10}(\omega) + 40 \log_{10}(\omega_n) & \omega \gg \omega_n \end{cases}$$



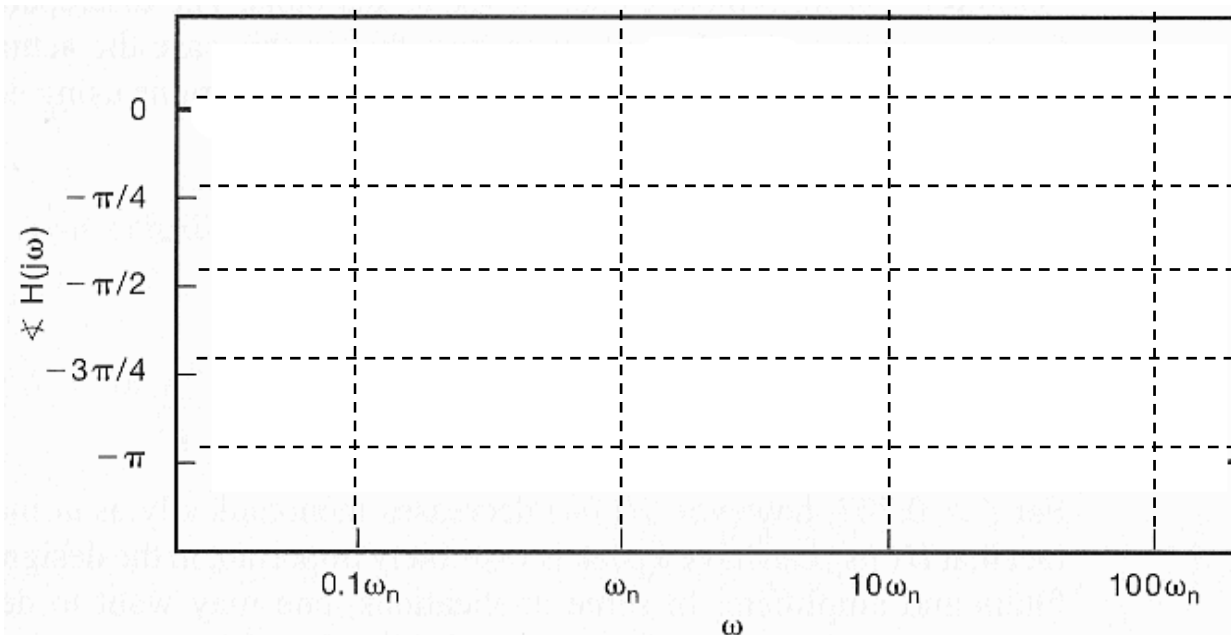
$$\omega_{\max} = \omega_n \sqrt{1 - 2\zeta^2}$$

$$|H(j\omega_{\max})| = \frac{1}{2\zeta \sqrt{1 - \zeta^2}}$$

■ Second-Order CT Systems: $H(j\omega) = \frac{1}{(j\frac{\omega}{\omega_n})^2 + 2\zeta(j\frac{\omega}{\omega_n}) + 1}$

$$\angle H(j\omega) = -\tan^{-1} \left(\frac{2\zeta(\frac{\omega}{\omega_n})}{1 - (\frac{\omega}{\omega_n})^2} \right)$$

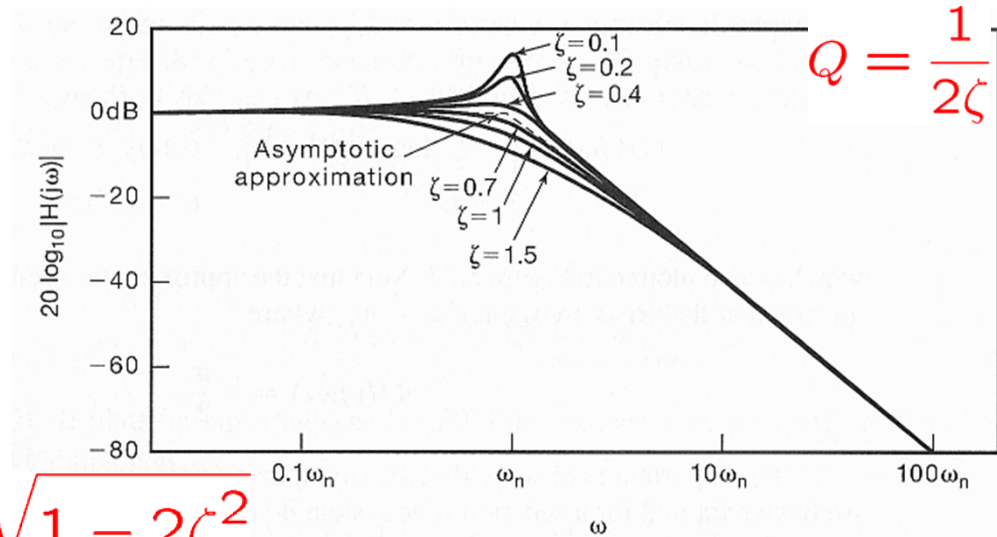
$$\approx \begin{cases} 0 & \omega \leq 0.1\omega_n \\ -\pi/2 & \omega = \omega_n \\ -(\pi/2)[\log_{10}(\frac{\omega}{\omega_n}) + 1] & 0.1\omega_n \leq \omega \leq 10\omega_n \\ -\pi & \omega \geq 10\omega_n \end{cases}$$



■ Second-Order CT Systems: $H(j\omega) = \frac{1}{(j\frac{\omega}{\omega_n})^2 + 2\zeta(j\frac{\omega}{\omega_n}) + 1}$

$20 \log_{10} |H(j\omega)| =$

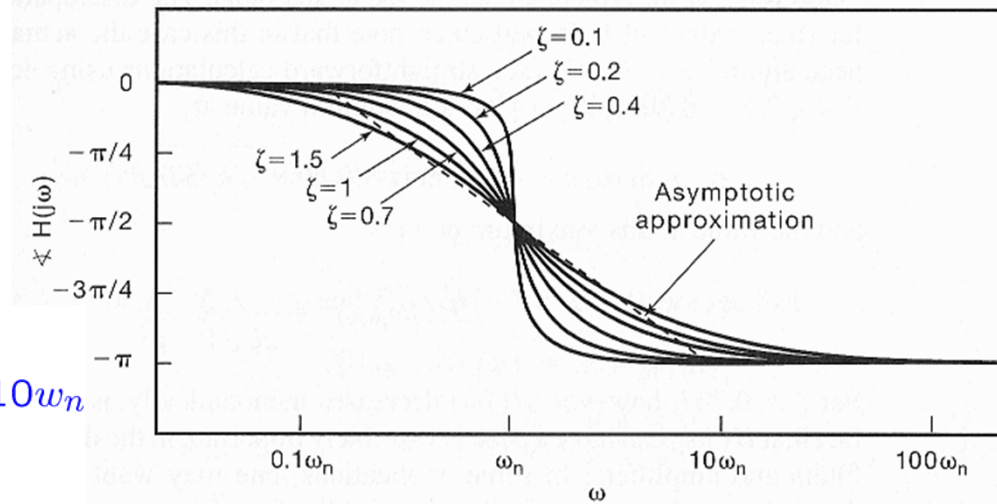
$$\begin{cases} 0 & \omega \ll \omega_n \\ -20 \log_{10}(2\zeta) & \omega = \omega_n \\ -40 \log_{10}(\omega) + 40 \log_{10}(\omega_n) & \omega \gg \omega_n \end{cases}$$



• For $\zeta < \frac{\sqrt{2}}{2}$ $\omega_{max} = \omega_n \sqrt{1 - 2\zeta^2}$

$\angle H(j\omega) =$

$$\begin{cases} 0 & \omega \leq 0.1\omega_n \\ -(\pi/2)[\log_{10}(\omega/\omega_n) + 1] & 0.1\omega_n \leq \omega \leq 10\omega_n \\ -\pi/2 & \omega = \omega_n \\ -\pi & \omega \geq 10\omega_n \end{cases}$$



▪ Example 6.4: (p.457)

$$H(j\omega) = \frac{2 \times 10^4}{(j\omega)^2 + 100(j\omega) + 10^4}$$

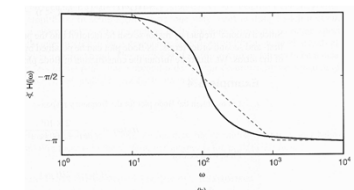
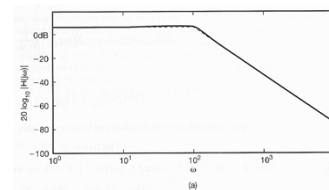
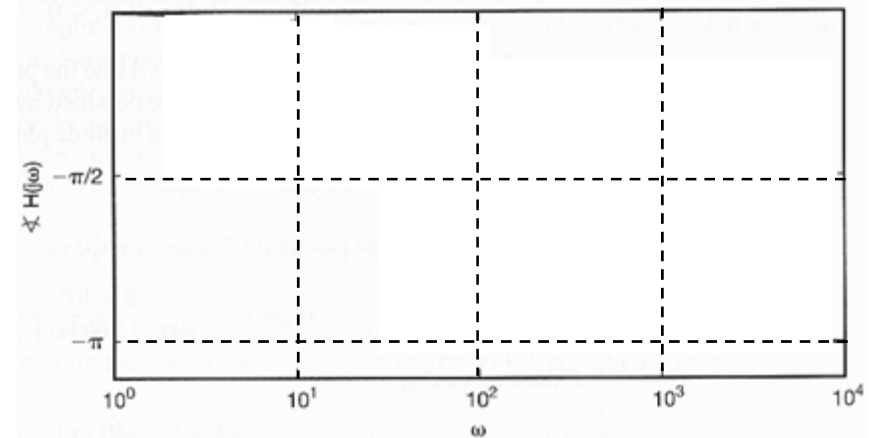
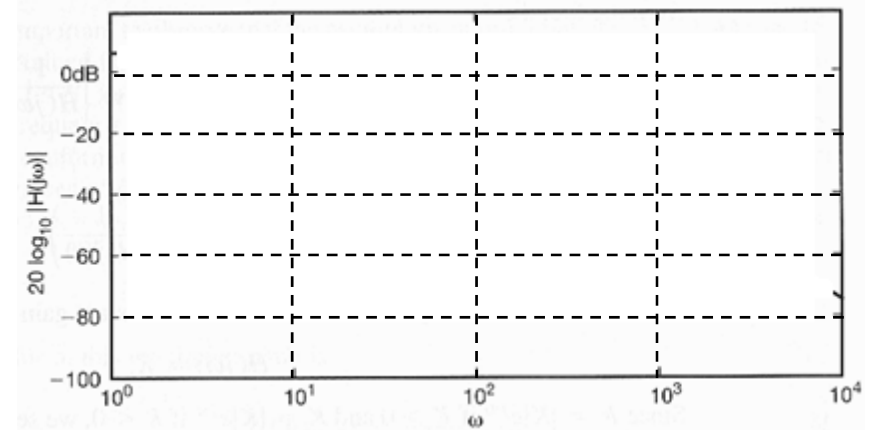
$$H(j\omega) = 2 \times \hat{H}(j\omega)$$

$$\angle H(j\omega) = \angle \hat{H}(j\omega)$$

$$\Rightarrow \begin{cases} \omega_n = 100 \\ \zeta = 1/2 \end{cases}$$

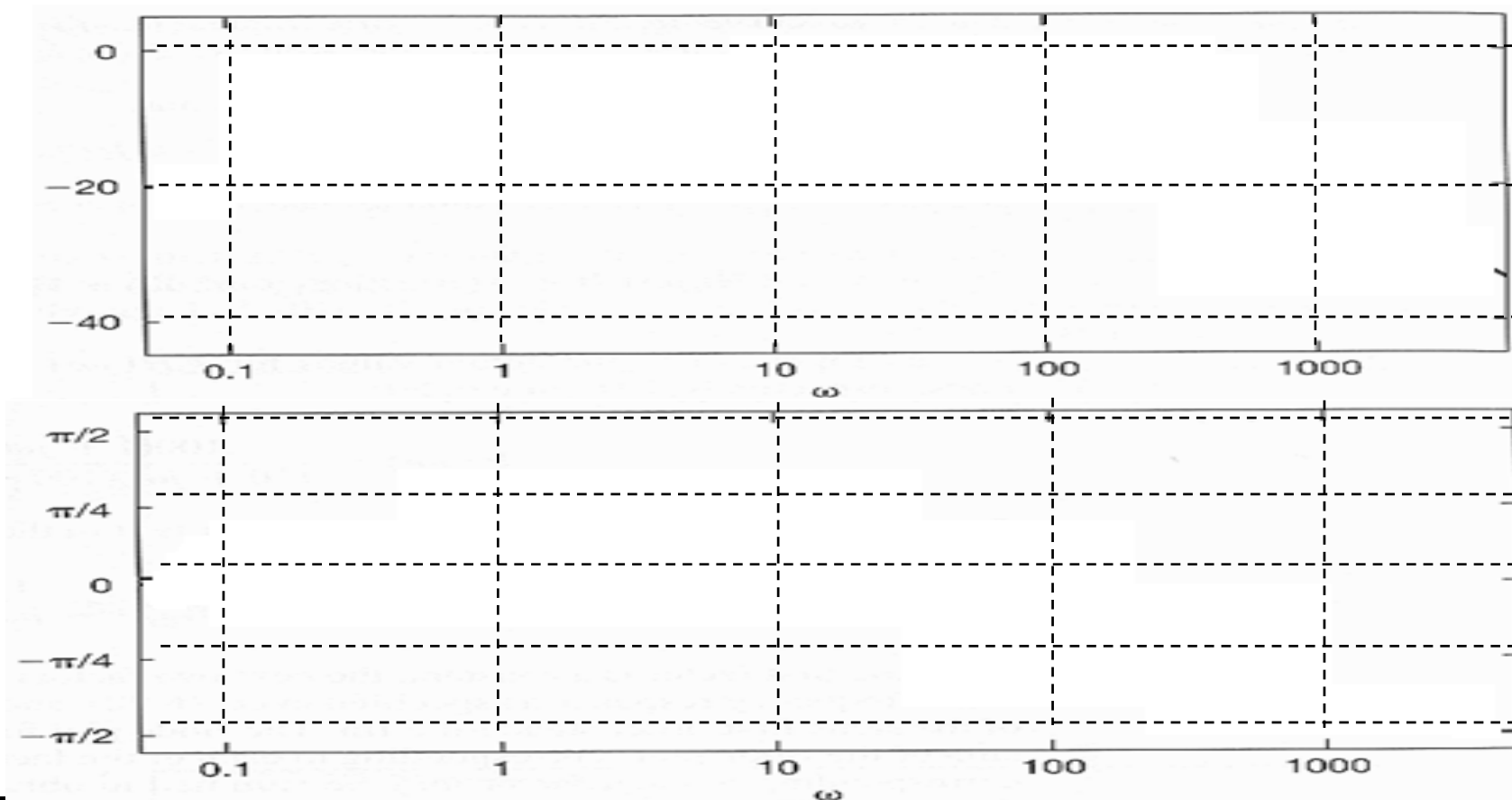
$$\Rightarrow 20 \log_{10} |H(j\omega)| = 20 \log_{10}(2) + 20 \log_{10} |\hat{H}(j\omega)|$$

$$\hat{H}(j\omega) = \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2}$$

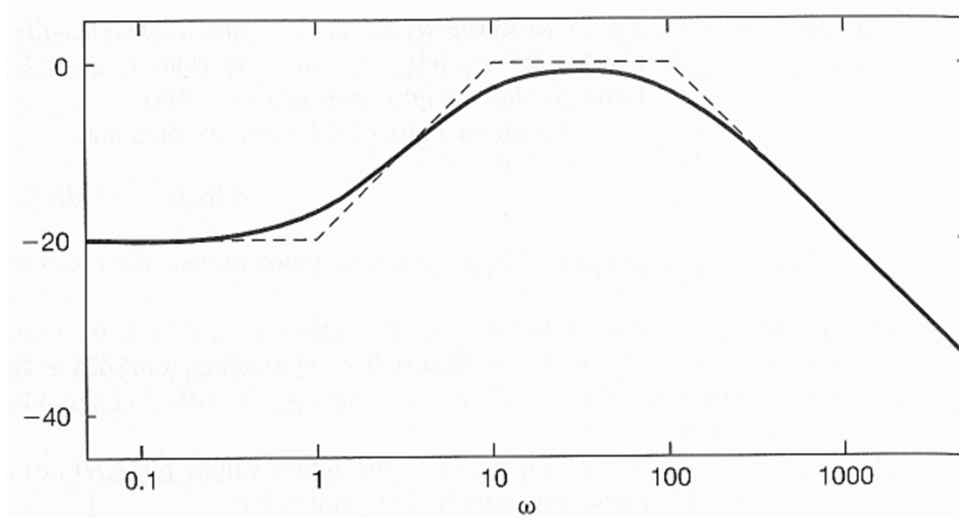


■ Example 6.5:
$$H(j\omega) = \frac{100(1 + j\omega)}{(10 + j\omega)(100 + j\omega)}$$

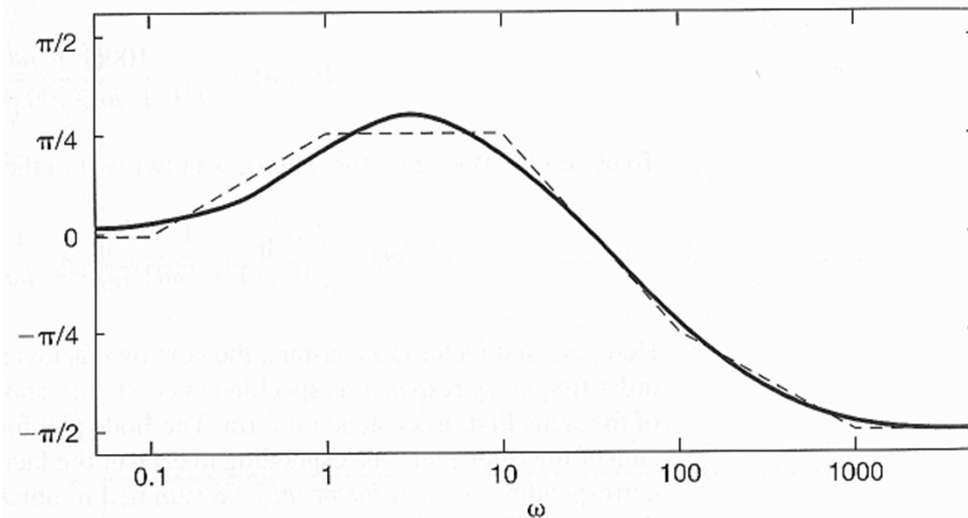
$$= \left(\frac{1}{10}\right) (1 + j\omega) \left(\frac{1}{1 + j\frac{\omega}{10}}\right) \left(\frac{1}{1 + j\frac{\omega}{100}}\right)$$



■ Example 6.5:

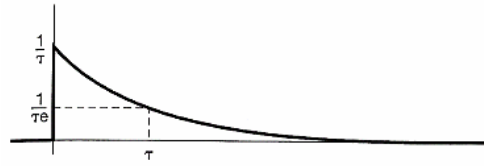


(a)

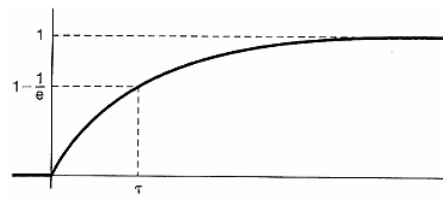


(b)

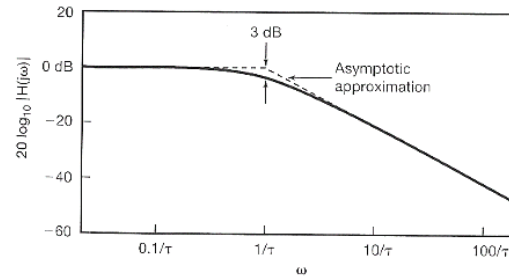
$h(t)$



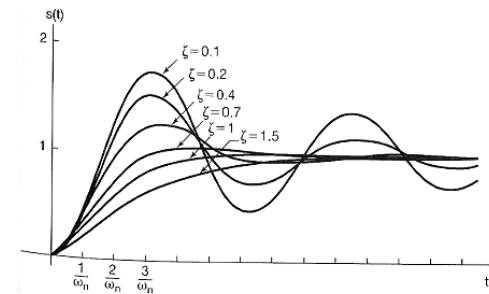
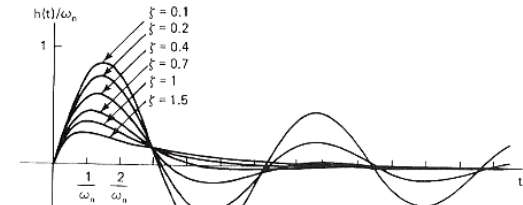
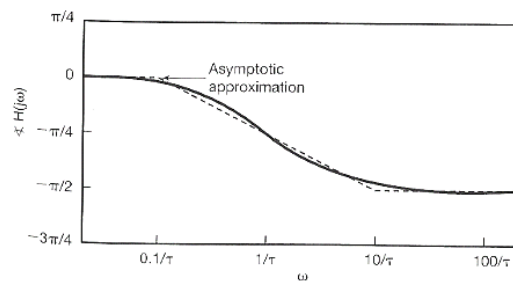
$s(t)$



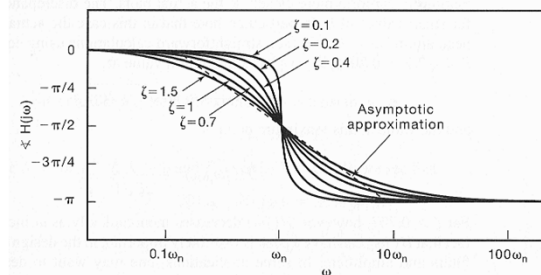
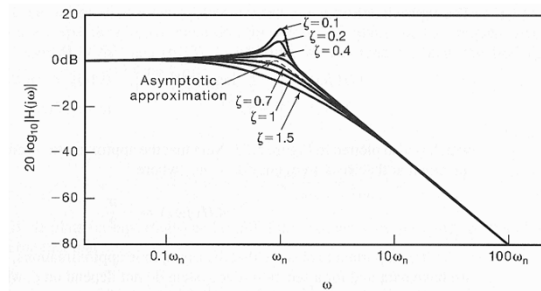
$20 \log_{10} |H(j\omega)|$



$\angle H(j\omega)$



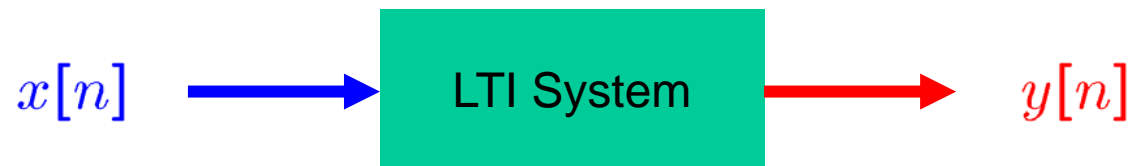
(b)



- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- p.461 ■ 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

First-Order DT Systems: (p.461)

$$Y(e^{j\omega}) = X(e^{j\omega}) H(e^{j\omega})$$



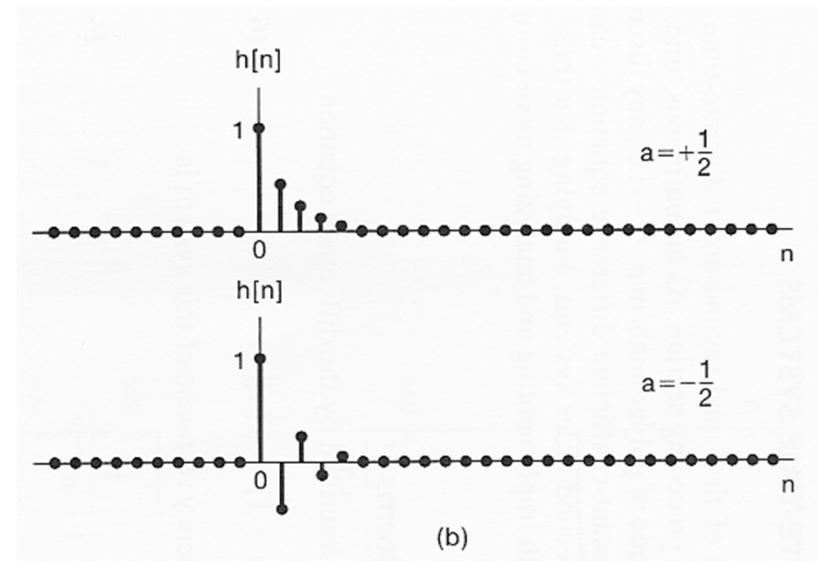
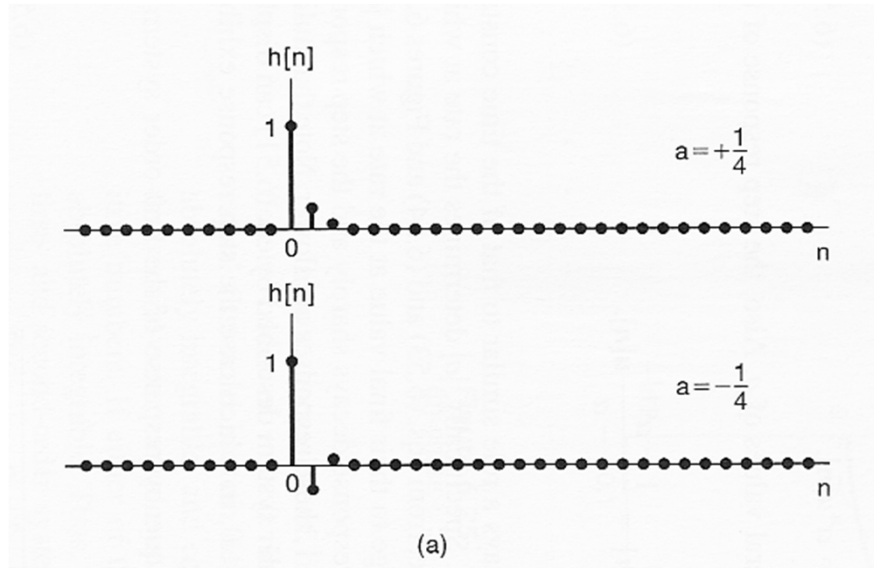
$$y[n] - a y[n-1] = x[n] \quad |a| < 1$$

$$\Rightarrow H(e^{j\omega}) = \frac{1}{1 - a e^{-j\omega}}$$

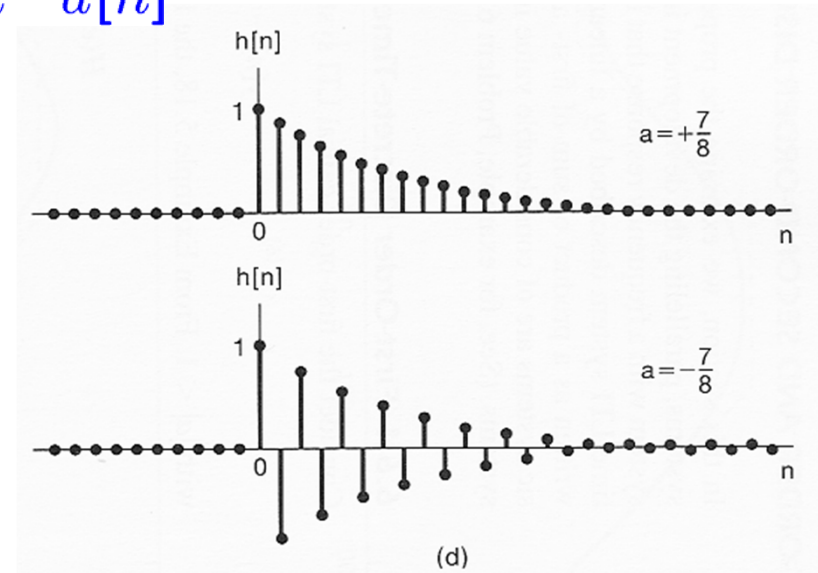
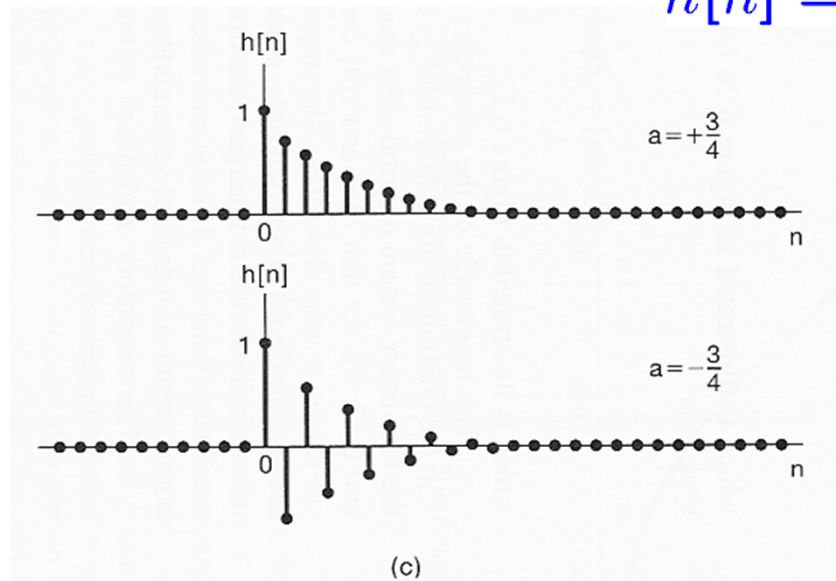
$$\Rightarrow h[n] = a^n u[n]$$

$$\Rightarrow s[n] = h[n] * u[n] = \frac{1 - a^{n+1}}{1 - a} u[n]$$

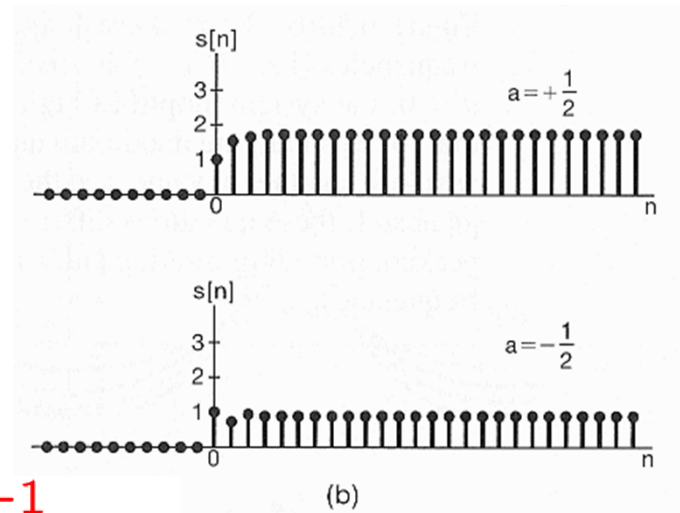
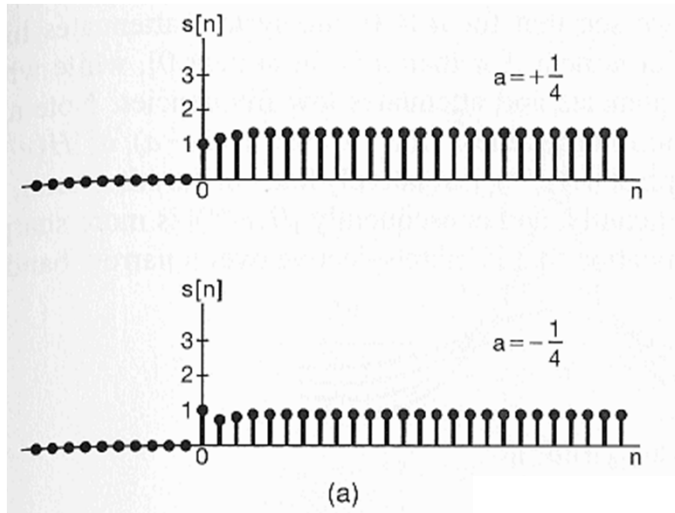
■ Impulse Response of First-Order DT Systems:



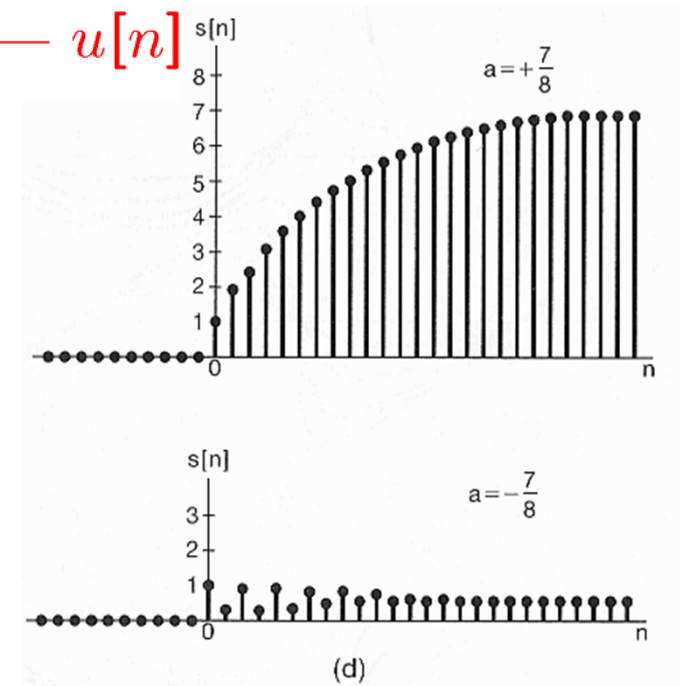
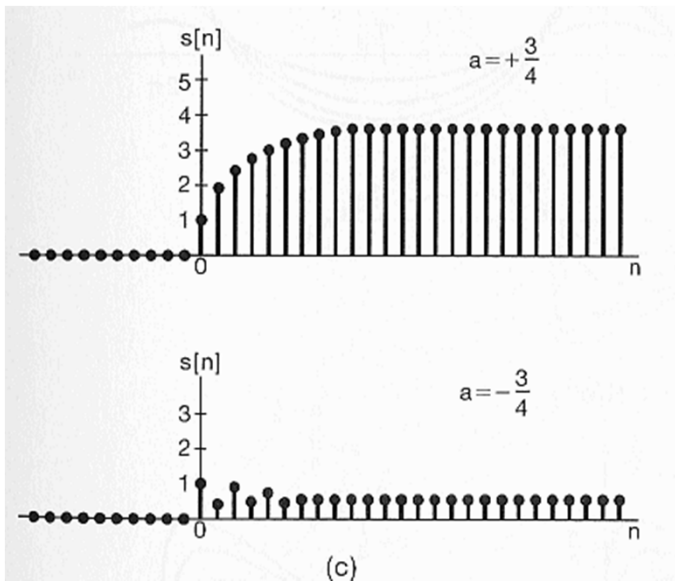
$$h[n] = a^n u[n]$$



Step Response of First-Order DT Systems:



$$s[n] = \frac{1 - a^{n+1}}{1 - a} u[n]$$



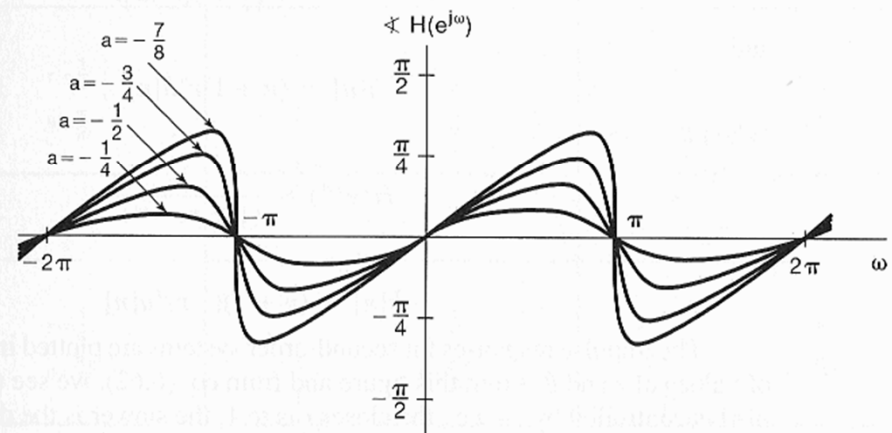
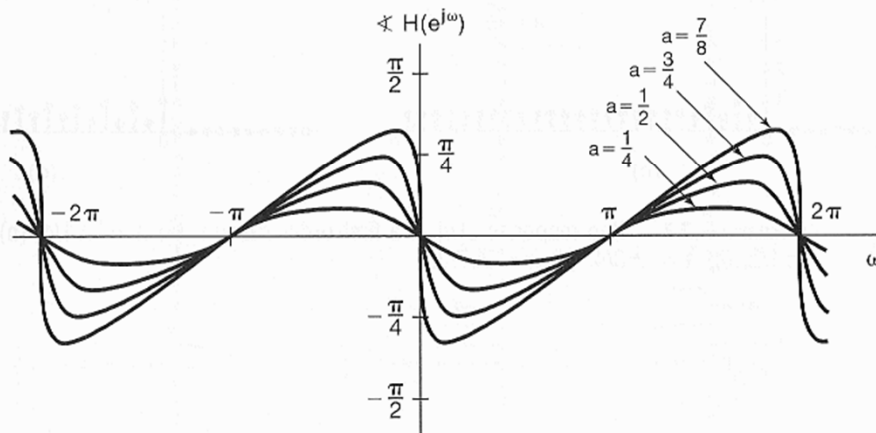
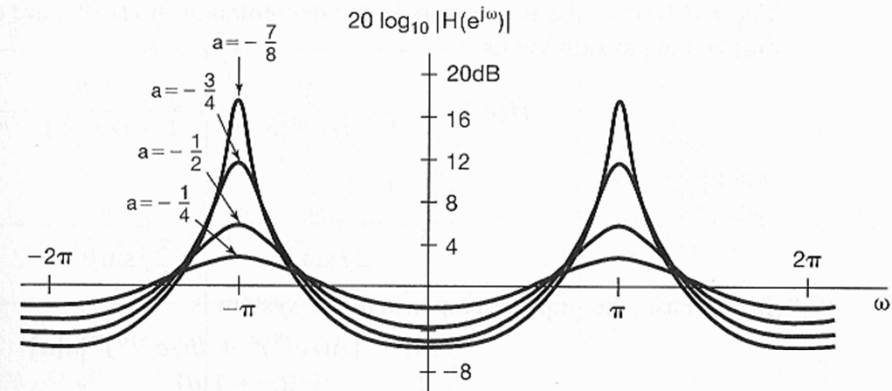
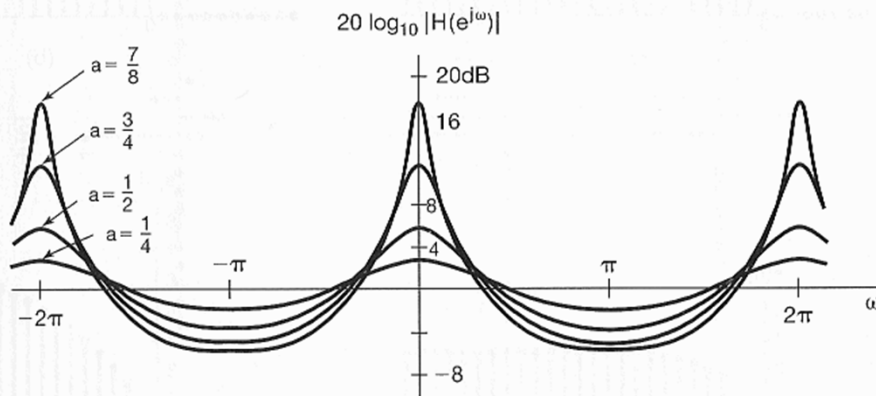
- Magnitude & Phase of Frequency Response:

$$H(e^{jw}) = \frac{1}{1 - ae^{-jw}} = \frac{1}{1 - a \cos w + ja \sin w}$$

$$|H(e^{jw})| = \frac{1}{\sqrt{1 + a^2 - 2a \cos w}}$$

$$\angle H(e^{jw}) = -\tan^{-1} \left[\frac{a \sin w}{1 - a \cos w} \right]$$

Magnitude & Phase of Frequency Response:



(a)

(b)

- Second-Order DT Systems: (p.465)

$$0 < r < 1 \text{ and } 0 \leq \theta \leq \pi$$

$$y[n] - 2r \cos(\theta) y[n-1] + r^2 y[n-2] = x[n]$$

$$\Rightarrow H(e^{j\omega}) = \frac{1}{1 - 2r \cos(\theta) e^{-j\omega} + r^2 e^{-j2\omega}}$$

$$\cos(\theta) = \frac{1}{2} (e^{j\theta} + e^{-j\theta})$$

$$= \frac{1}{[1 - (r e^{j\theta}) e^{-j\omega}] [1 - (r e^{-j\theta}) e^{-j\omega}]}$$

Impulse Response of 2nd-Order DT Systems:

- For $\theta = 0$:

$$\Rightarrow H(e^{j\omega}) = \frac{1}{(1 - r e^{-j\omega})^2} \Rightarrow h[n] = (n+1) (r)^n u[n]$$

- For $\theta = \pi$:

$$\Rightarrow H(e^{j\omega}) = \frac{1}{(1 + r e^{-j\omega})^2} \Rightarrow h[n] = (n+1) (-r)^n u[n]$$

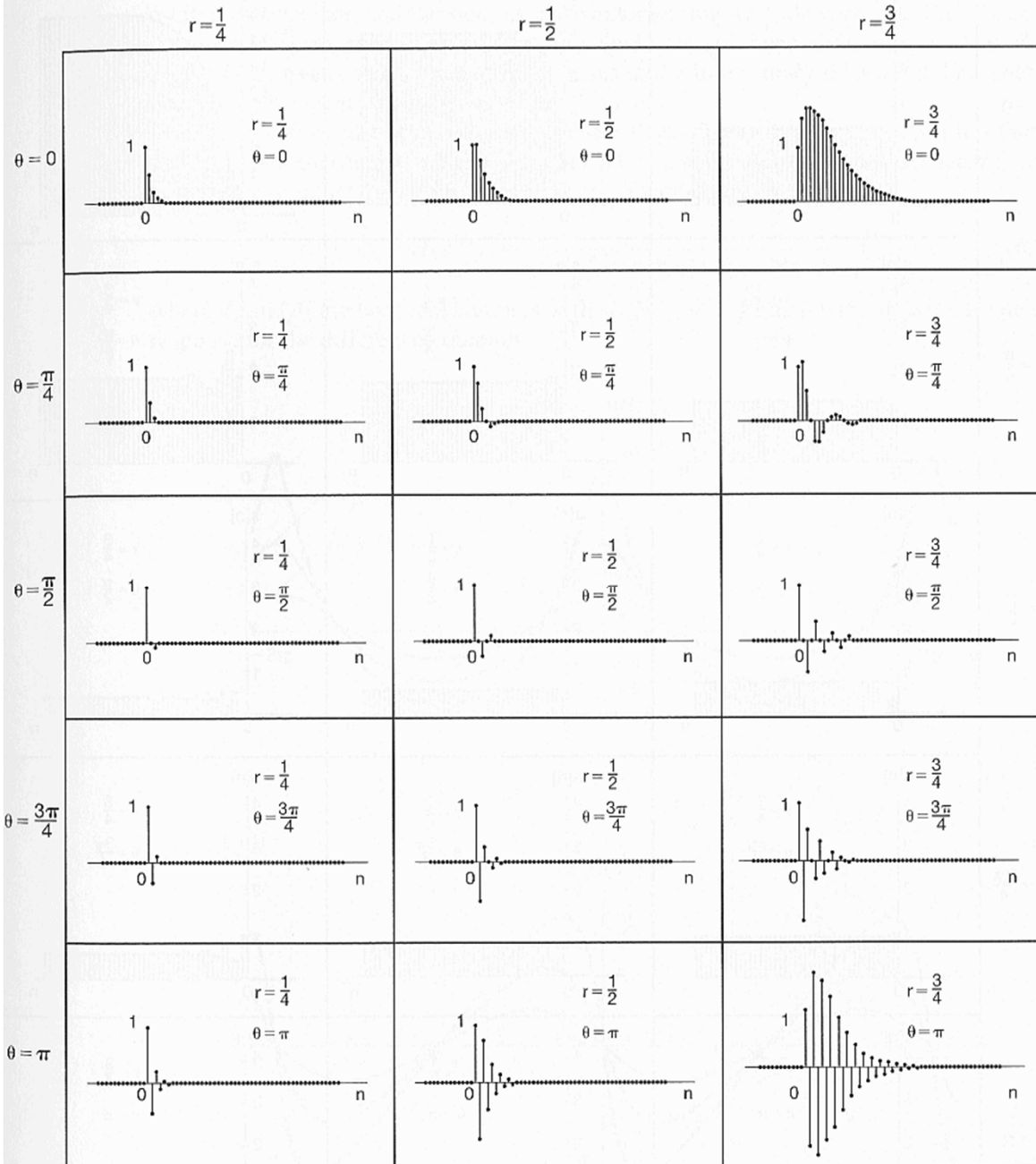
- For $\theta \neq 0$ or π :

$$\Rightarrow H(e^{j\omega}) = \frac{A}{1 - (r e^{j\theta}) e^{-j\omega}} + \frac{B}{1 - (r e^{-j\theta}) e^{-j\omega}}$$

$$A = \frac{e^{j\theta}}{2j \sin(\theta)}$$

$$B = -\frac{e^{-j\theta}}{2j \sin(\theta)}$$

$$\Rightarrow h[n] = \left[A (r e^{j\theta})^n + B (r e^{-j\theta})^n \right] u[n] = r^n \frac{\sin[(n+1)\theta]}{\sin(\theta)} u[n]$$



$$h[n] = (n+1) (r)^n u[n]$$

$$r^n \frac{\sin[(n+1)\theta]}{\sin(\theta)} u[n]$$

$$h[n] = (n+1) (-r)^n u[n]$$

Step Response of 2nd-Order DT Systems:

- For $\theta = 0$:

$$s[n] = \left[\frac{1}{(r-1)^2} - \frac{r}{(r-1)^2} r^n + \frac{r}{r-1} (n+1) r^n \right] u[n]$$

- For $\theta = \pi$:

$$s[n] = \left[\frac{1}{(r+1)^2} + \frac{r}{(r+1)^2} (-r)^n + \frac{r}{r+1} (n+1) (-r)^n \right] u[n]$$

- For $\theta \neq 0$ or π :

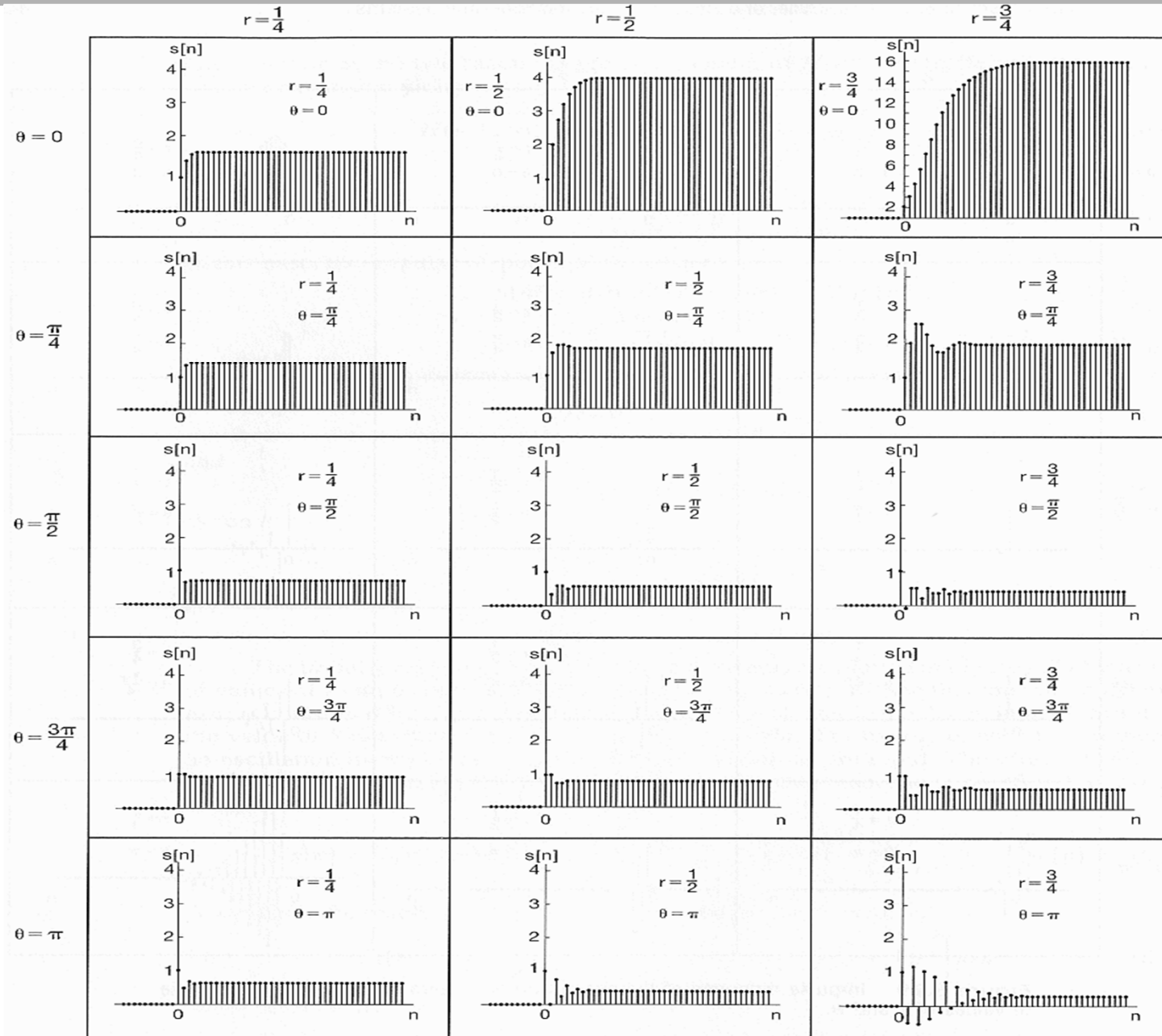
$$s[n] = h[n] * u[n]$$

$$A = \frac{e^{j\theta}}{2j \sin(\theta)}$$

$$B = -\frac{e^{-j\theta}}{2j \sin(\theta)}$$

$$= \left[A \left(\frac{1 - (re^{j\theta})^{n+1}}{1 - re^{j\theta}} \right) + B \left(\frac{1 - (re^{-j\theta})^{n+1}}{1 - re^{-j\theta}} \right) \right] u[n]$$

First-Order & Second-Order DT Systems

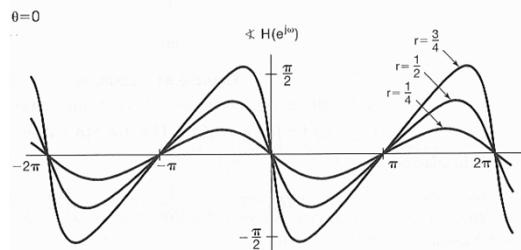
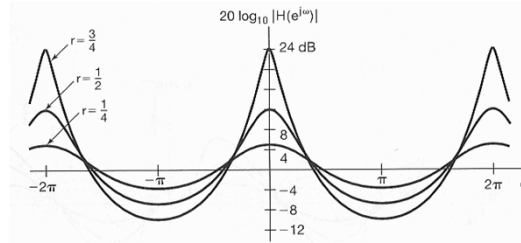


* Note: The plot for $r = \frac{3}{4}$, $\theta = 0$ has a different scale from the others.

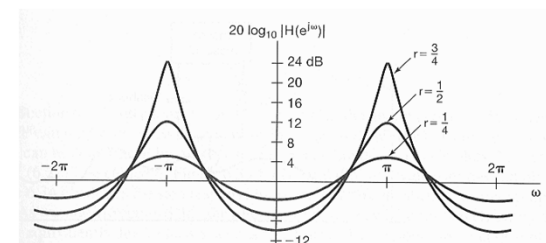
Magnitude & Phase of Frequency Response:

$$H(e^{j\omega}) =$$

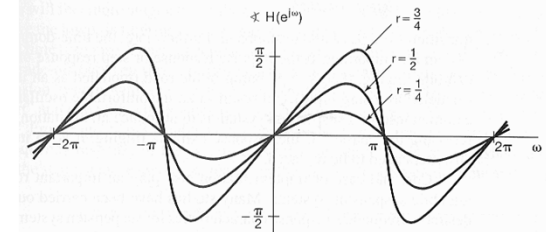
$$\frac{1}{1 - 2r \cos(\theta) e^{-j\omega} + r^2 e^{-j2\omega}}$$



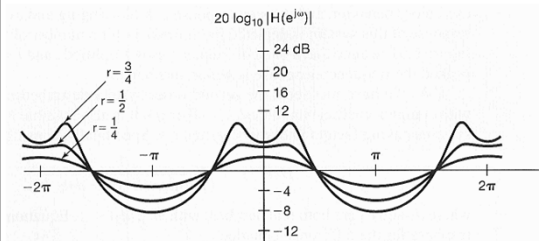
(a)



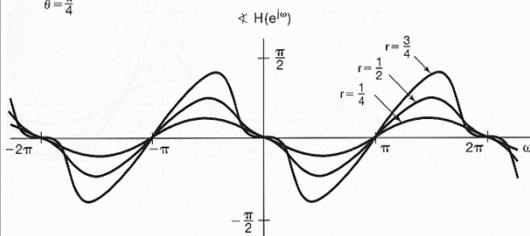
$\theta = \pi$



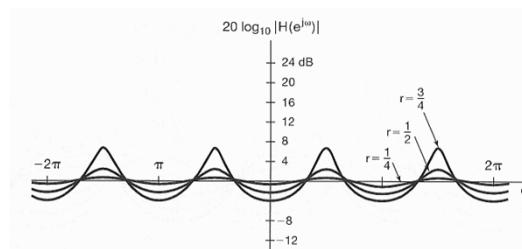
(e)



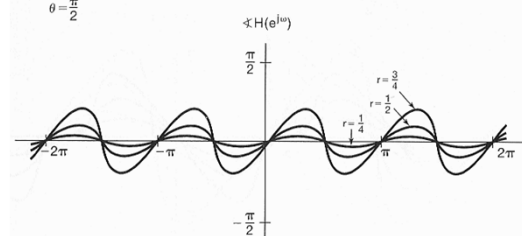
$\theta = \pi/4$



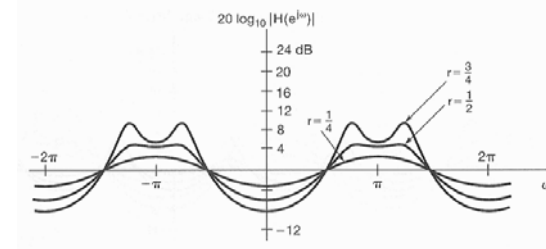
(b)



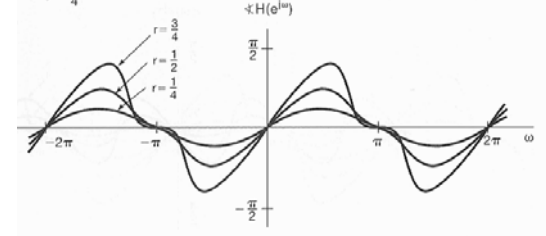
$\theta = \pi/2$



(c)



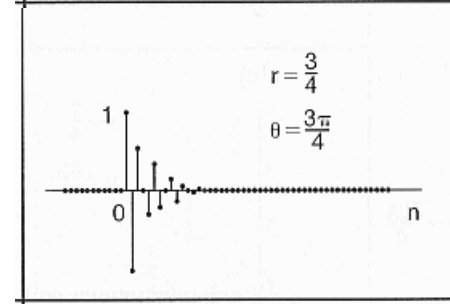
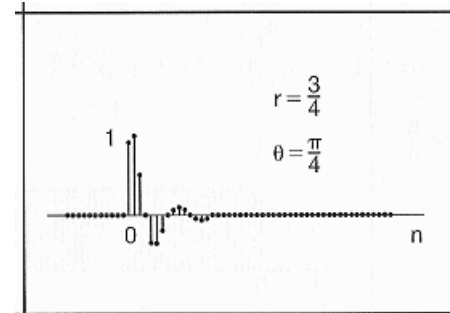
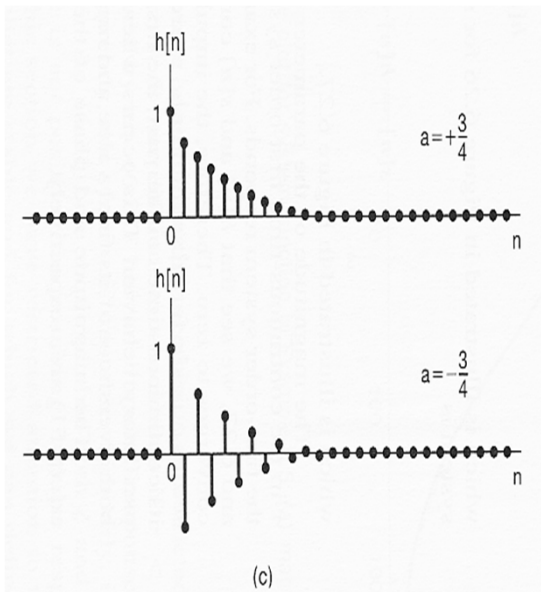
$\theta = 3\pi/4$



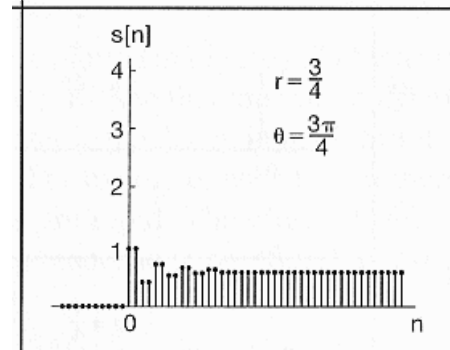
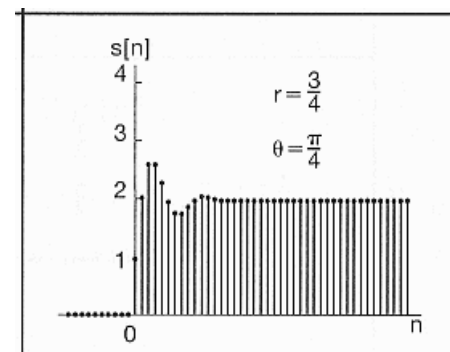
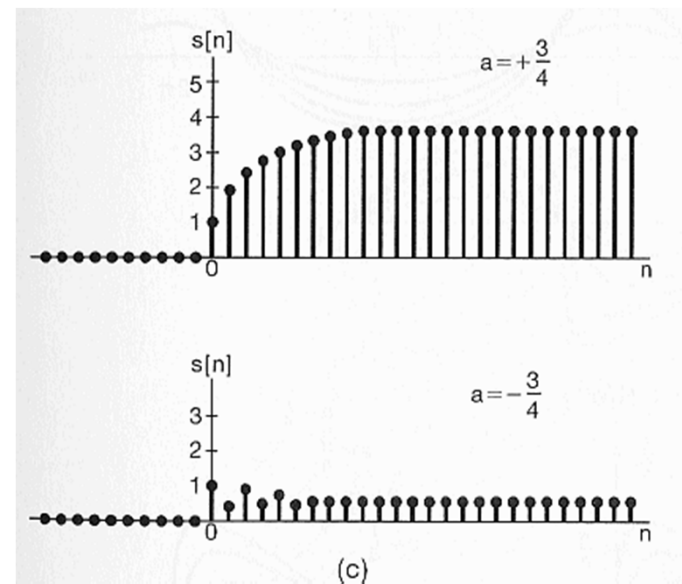
(d)

First-Order & Second-Order DT Systems

$h[n]$



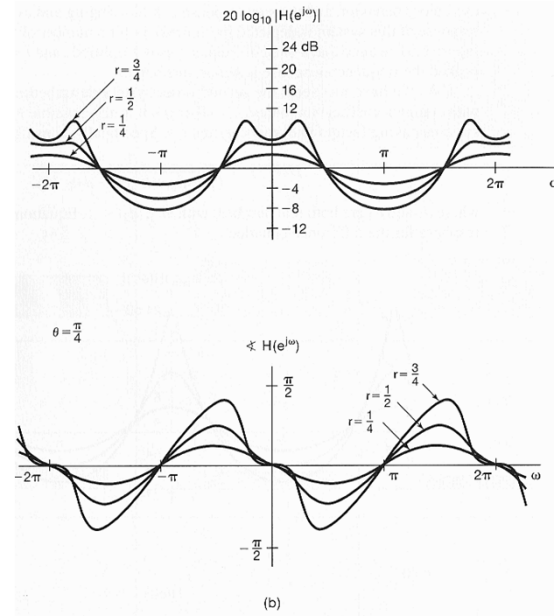
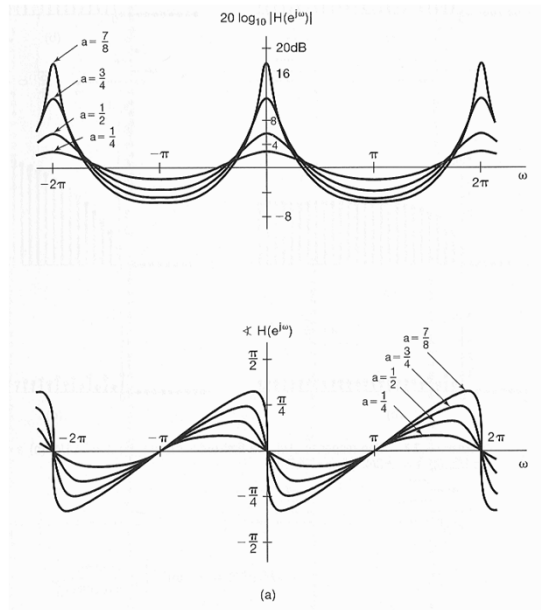
$s[n]$



First-Order & Second-Order DT Systems

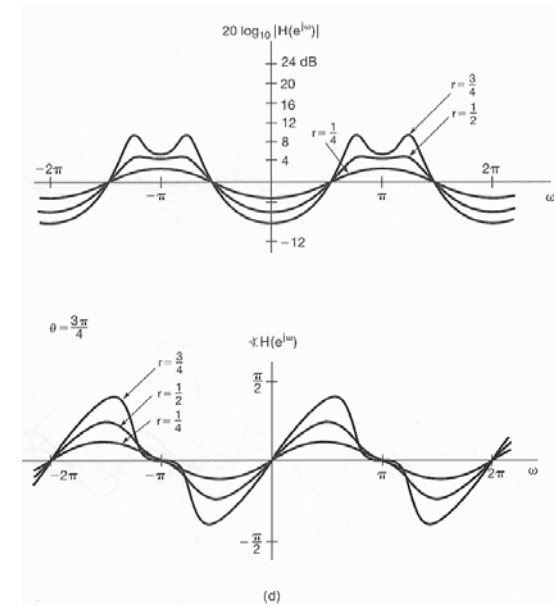
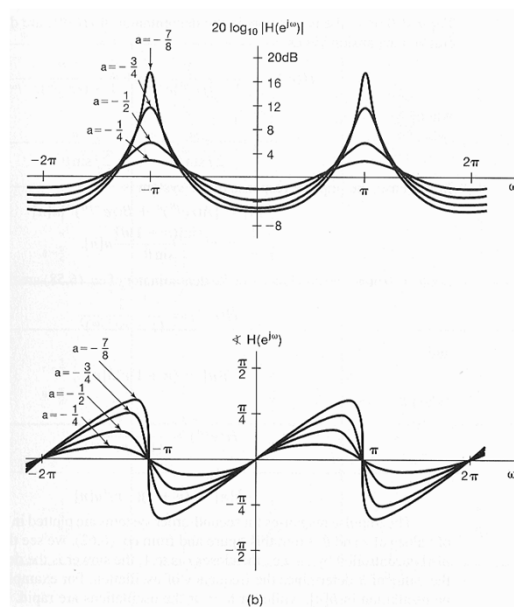
$$20 \log_{10} |H(e^{j\omega})|$$

$$\angle H(e^{j\omega})$$



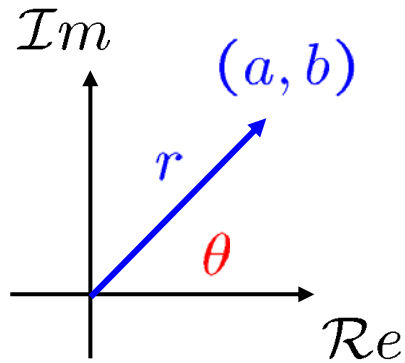
$$20 \log_{10} |H(e^{j\omega})|$$

$$\angle H(e^{j\omega})$$



- The Magnitude-Phase Representation of the Fourier Transform [\(p.423\)](#)
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

■ Magnitude & Phase Representation:



$$a + jb \Rightarrow \begin{cases} r = \sqrt{a^2 + b^2} \\ \tan(\theta) = \frac{b}{a} \end{cases}$$

$$\Rightarrow a + jb = r e^{j\theta}$$

$$|a + jb| = \sqrt{a^2 + b^2} \quad \left| \frac{1}{a + jb} \right| = \frac{1}{\sqrt{a^2 + b^2}}$$

$$\angle a + jb = \tan^{-1}\left(\frac{b}{a}\right) \quad \angle \frac{1}{a + jb} = -\tan^{-1}\left(\frac{b}{a}\right)$$

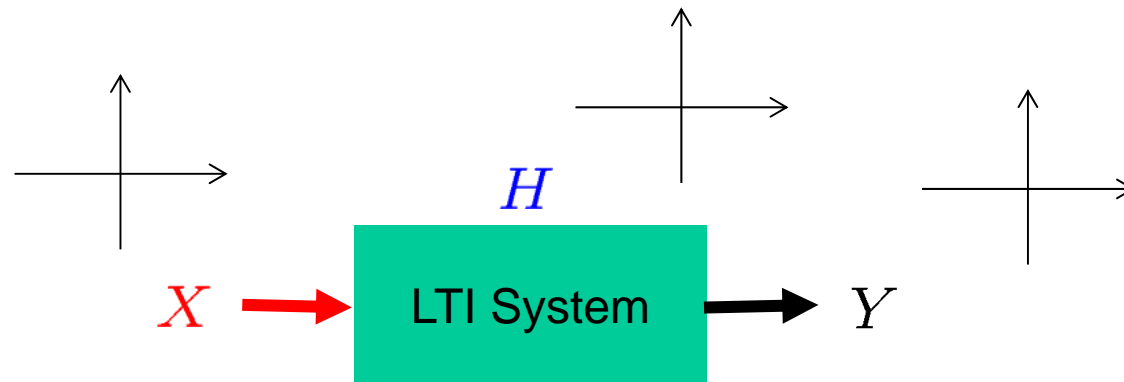
$$X(j\omega) = \text{Re}\{X(j\omega)\} + j \text{Im}\{X(j\omega)\} = |X(j\omega)| e^{j\angle X(j\omega)}$$

$$X(e^{j\omega}) = \text{Re}\{X(e^{j\omega})\} + j \text{Im}\{X(e^{j\omega})\} = |X(e^{j\omega})| e^{j\angle X(e^{j\omega})}$$

$|X(j\omega)|$ or $|X(e^{j\omega})|$: magnitude

$\angle X(j\omega)$ or $\angle X(e^{j\omega})$: phase angle

▪ Magnitude & Phase Distortions:



$$Y(j\omega) = X(j\omega) H(j\omega)$$

$$Y(e^{j\omega}) = X(e^{j\omega}) H(e^{j\omega})$$

$$\Rightarrow |Y(j\omega)| = |X(j\omega)| |H(j\omega)|$$

$$|Y(e^{j\omega})| = |X(e^{j\omega})| |H(e^{j\omega})|$$

magnitude distortion

$$\Rightarrow \angle Y(j\omega) = \angle X(j\omega) + \angle H(j\omega)$$

$$\angle Y(e^{j\omega}) = \angle X(e^{j\omega}) + \angle H(e^{j\omega})$$

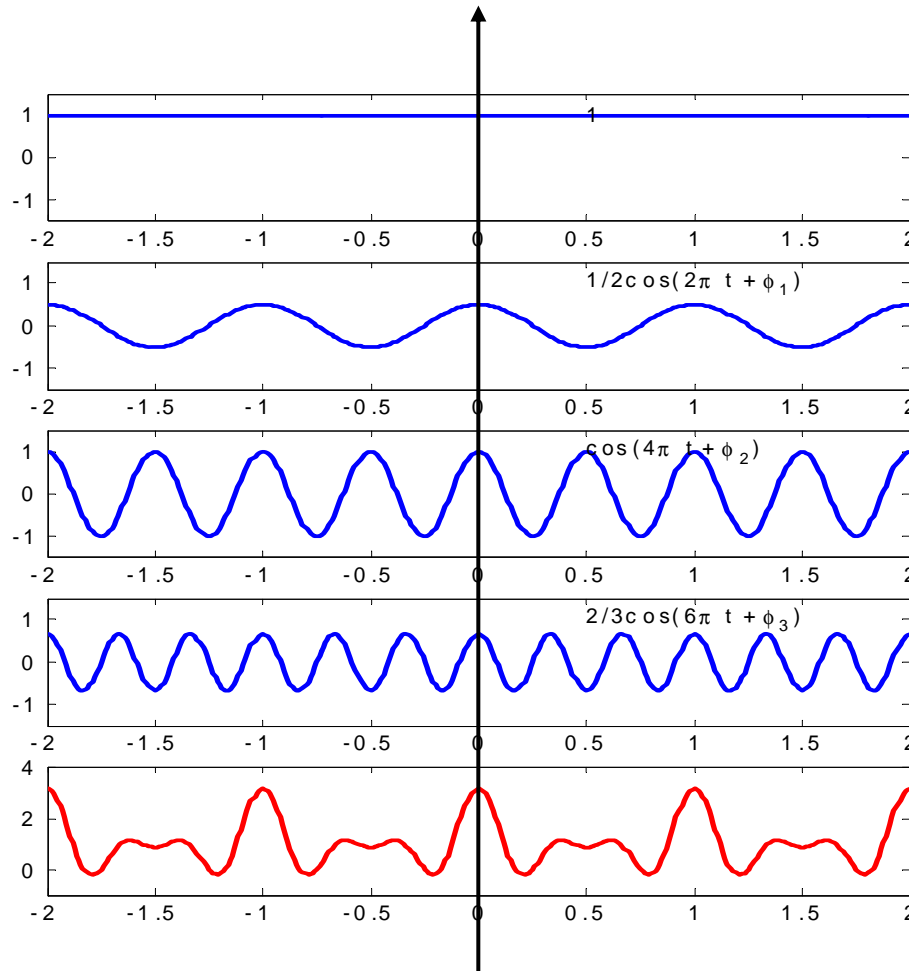
phase distortion

$|H(j\omega)|$ or $|H(e^{j\omega})|$: gain of the system

$\angle H(j\omega)$ or $\angle H(e^{j\omega})$: phase shift of the system

- Magnitude & Phase Angle:** $A \cos(\omega_0 t + \phi) = \frac{A}{2} e^{j\phi} e^{j\omega_0 t} + \frac{A}{2} e^{-j\phi} e^{-j\omega_0 t}$

$$x(t) = 1 \cos(0\pi t + \phi_0) + \frac{1}{2} \cos(2\pi t + \phi_1) + 1 \cos(4\pi t + \phi_2) + \frac{2}{3} \cos(6\pi t + \phi_3)$$



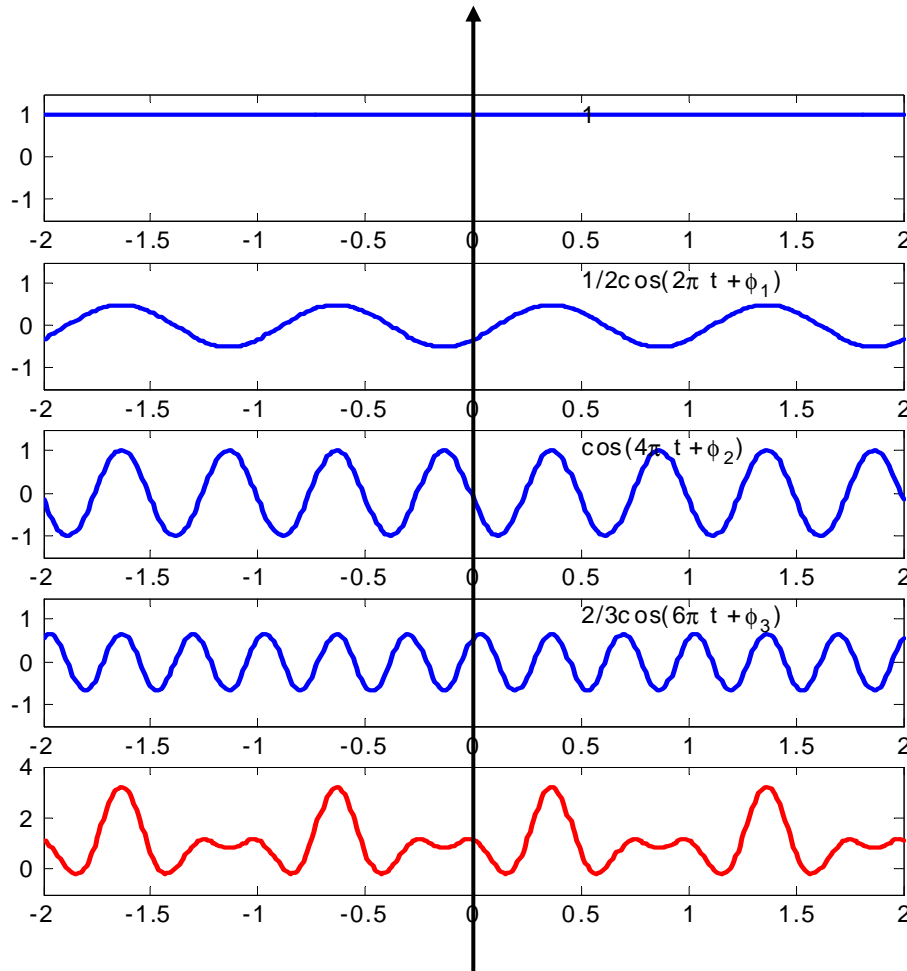
$$\begin{cases} \phi_1 = 0 \text{ (rad)} \\ \phi_2 = 0 \text{ (rad)} \\ \phi_3 = 0 \text{ (rad)} \end{cases}$$

ss3-17

ss3-18

- Magnitude & Phase Angle:** $A \cos(\omega_0 t + \phi) = \frac{A}{2} e^{j\phi} e^{j\omega_0 t} + \frac{A}{2} e^{-j\phi} e^{-j\omega_0 t}$

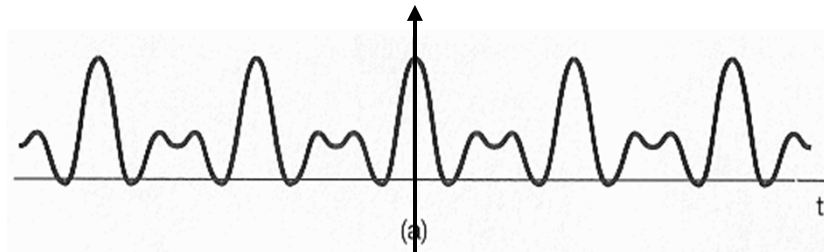
$$x(t) = 1 \cos(0\pi t + \phi_0) + \frac{1}{2} \cos(2\pi t + \phi_1) + 1 \cos(4\pi t + \phi_2) + \frac{2}{3} \cos(6\pi t + \phi_3)$$



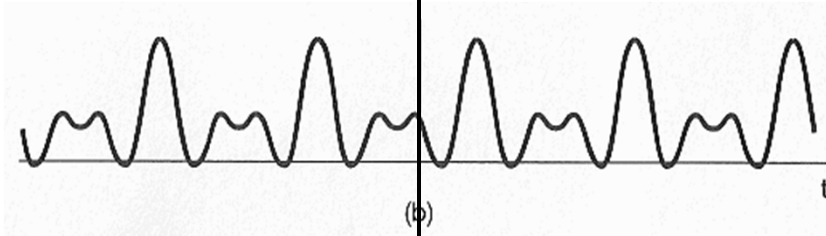
$$\begin{cases} \phi_1 = 4 \text{ (rad)} \\ \phi_2 = 8 \text{ (rad)} \\ \phi_3 = 12 \text{ (rad)} \end{cases}$$

- Magnitude & Phase Angle:** $A \cos(\omega_0 t + \phi) = \frac{A}{2} e^{j\phi} e^{j\omega_0 t} + \frac{A}{2} e^{-j\phi} e^{-j\omega_0 t}$

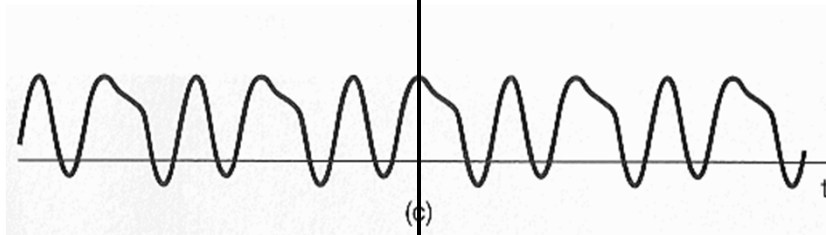
$$x(t) = 1 \cos(0\pi t + \phi_0) + \frac{1}{2} \cos(2\pi t + \phi_1) + 1 \cos(4\pi t + \phi_2) + \frac{2}{3} \cos(6\pi t + \phi_3)$$



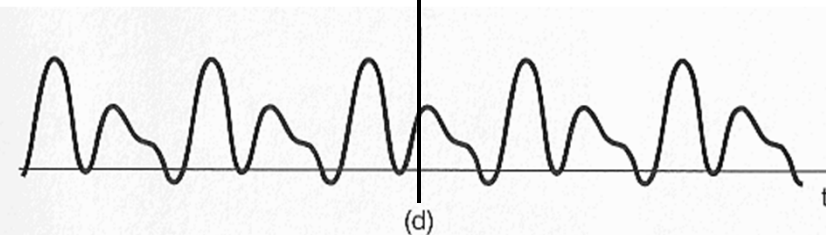
$$\begin{cases} \phi_1 = 0 \text{ (rad)} \\ \phi_2 = 0 \text{ (rad)} \\ \phi_3 = 0 \text{ (rad)} \end{cases}$$



$$\begin{cases} \phi_1 = 4 \text{ (rad)} \\ \phi_2 = 8 \text{ (rad)} \\ \phi_3 = 12 \text{ (rad)} \end{cases}$$



$$\begin{cases} \phi_1 = 6 \text{ (rad)} \\ \phi_2 = -2.7 \text{ (rad)} \\ \phi_3 = 0.93 \text{ (rad)} \end{cases}$$



$$\begin{cases} \phi_1 = 1.2 \text{ (rad)} \\ \phi_2 = 4.1 \text{ (rad)} \\ \phi_3 = -7.02 \text{ (rad)} \end{cases}$$

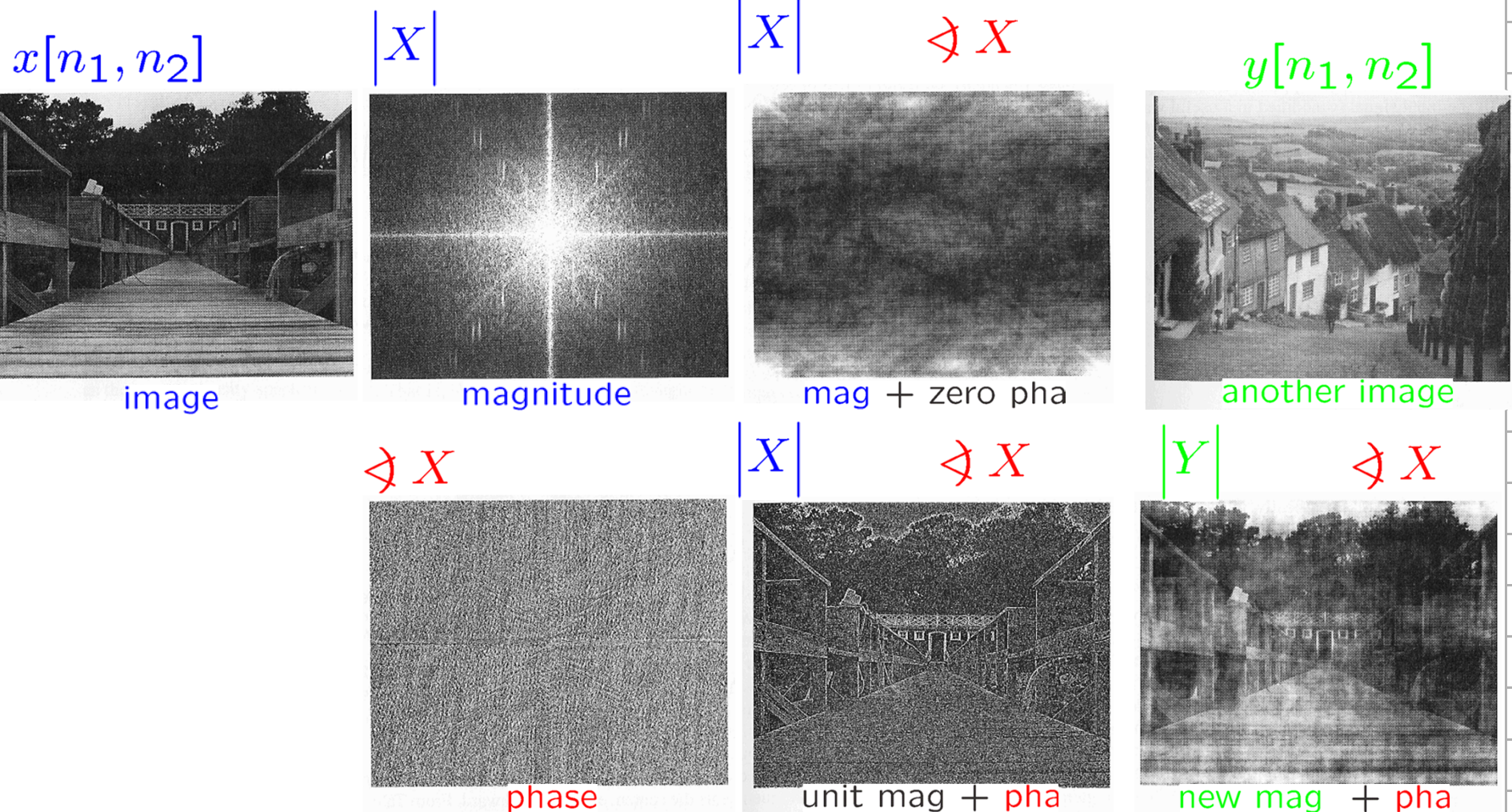
Magnitude & Phase Angle in Images:

$$x(t_1, t_2) \xleftrightarrow{\mathcal{F}} X(j\omega_1, j\omega_2)$$

$$x[n_1, n_2] \xleftrightarrow{\mathcal{F}} X(e^{j\omega_1}, e^{j\omega_2})$$

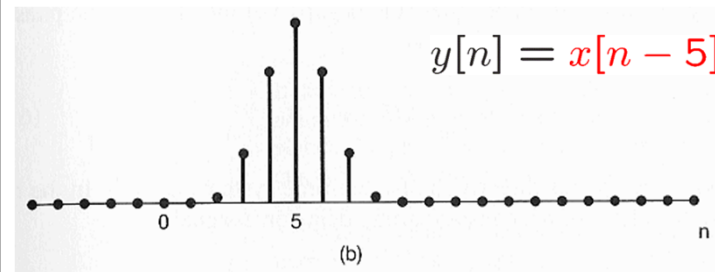
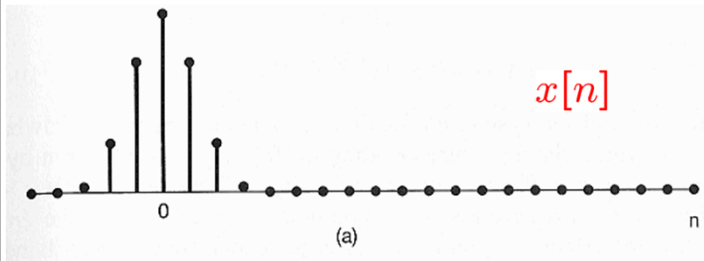
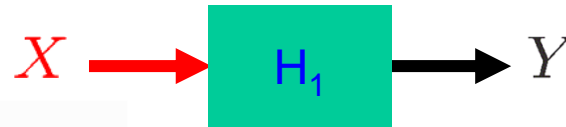
$$|X(j\omega_1, j\omega_2)| e^{j\angle X(j\omega_1, j\omega_2)}$$

$$|X(e^{j\omega_1}, e^{j\omega_2})| e^{j\angle X(e^{j\omega_1}, e^{j\omega_2})}$$



- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems (p.427)
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

Linear Phase:



$$n_0 = 5$$

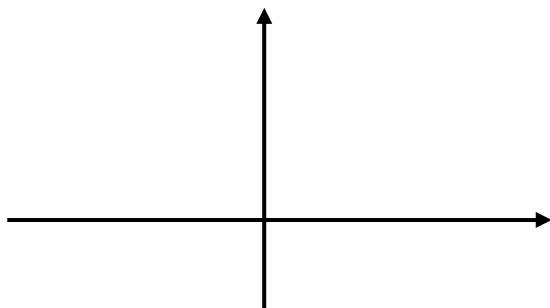
- $H_1(e^{j\omega}) = e^{-j\omega n_0}$

$$\Rightarrow \begin{cases} |H_1(e^{j\omega})| & = 1 \\ \angle |H_1(e^{j\omega})| & = -\omega n_0 \end{cases}$$

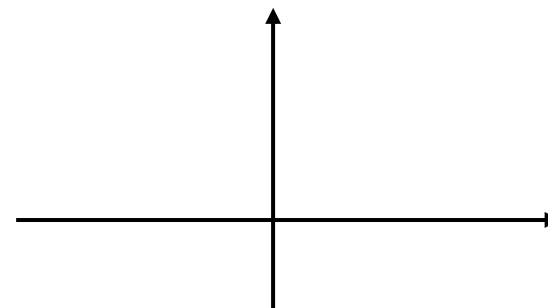
$$\begin{aligned} Y_1(e^{j\omega}) &= H_1(e^{j\omega}) X(e^{j\omega}) \\ &= e^{-j\omega n_0} X(e^{j\omega}) \end{aligned}$$

$$\Rightarrow y[n] = x[n - n_0]$$

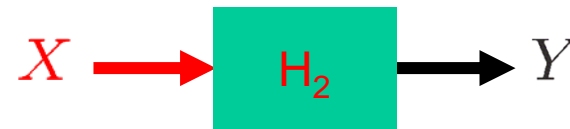
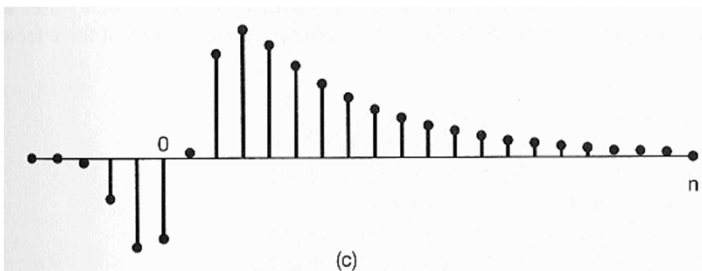
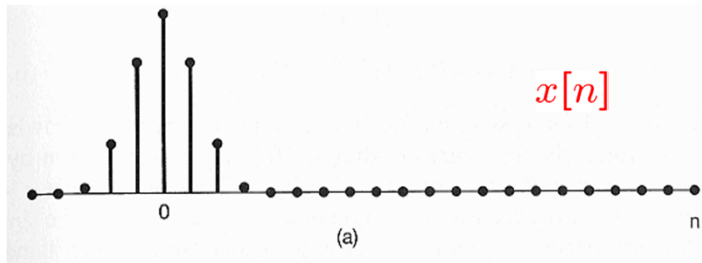
$$\angle H_1(e^{j\omega}) =$$



$$-\frac{d}{d\omega} \{ \angle H_1(e^{j\omega}) \} =$$



Non-Linear Phase:



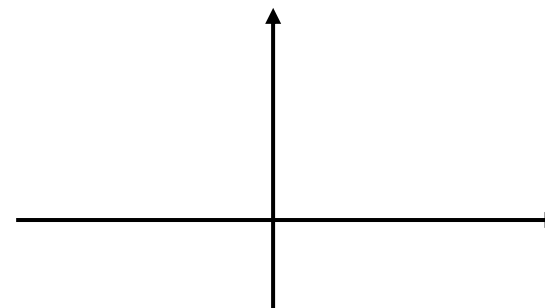
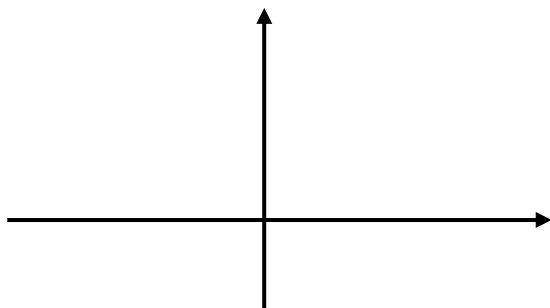
$$H_2(e^{j\omega}) = e^{jf(\omega)}$$

$$\bullet Y_2(e^{j\omega}) = H_2(e^{j\omega}) X(e^{j\omega})$$

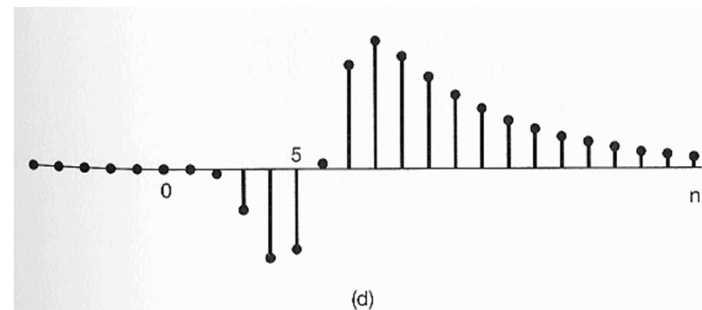
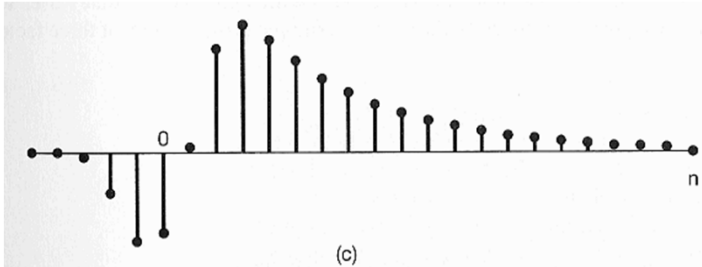
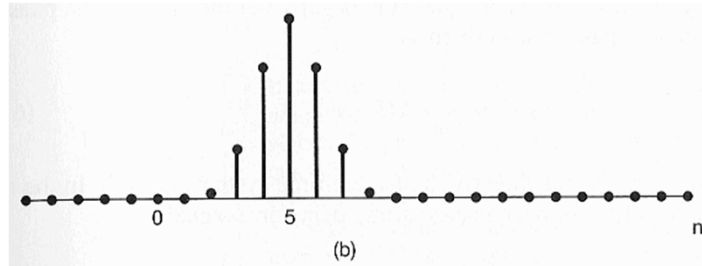
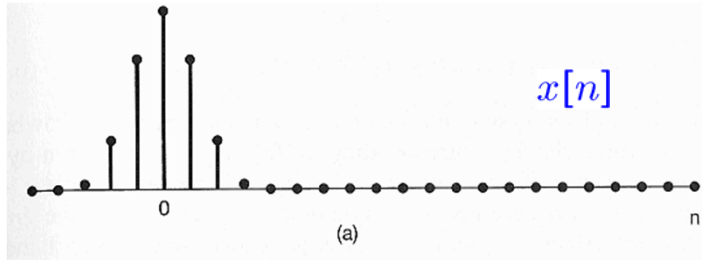
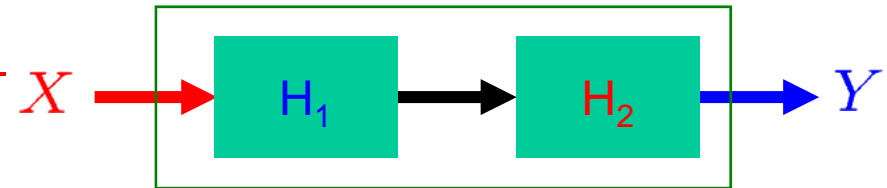
$$= e^{jf(\omega)} X(e^{j\omega})$$

$$\angle H_2(e^{j\omega}) =$$

$$-\frac{d}{d\omega} \left\{ \angle H_2(e^{j\omega}) \right\} =$$



Linear & Non-Linear Phase:



$$\bullet Y_3(e^{j\omega}) = H_2(e^{j\omega}) H_1(e^{j\omega}) X(e^{j\omega})$$

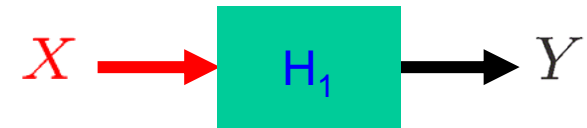
$$H_3(e^{j\omega}) = H_2(e^{j\omega}) H_1(e^{j\omega})$$

$$= H_2(e^{j\omega}) e^{-j\omega n_0}$$

$$= e^{j(f(\omega) - \omega n_0)}$$

$$-\frac{d}{d\omega} \left\{ \angle H_3(e^{j\omega}) \right\} =$$

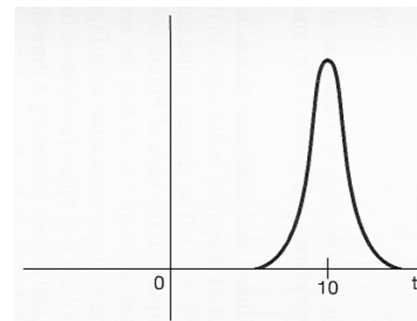
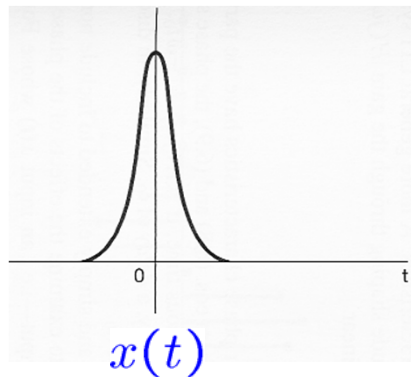
Linear Phase:



$$H_1(j\omega) = e^{-j\omega t_0}$$

$$\Rightarrow \begin{cases} |H_1(j\omega)| &= 1 \\ \angle |H_1(j\omega)| &= -\omega t_0 \end{cases}$$

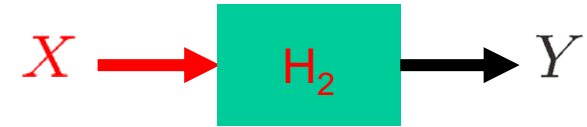
$$\Rightarrow y(t) = x(t - t_0)$$



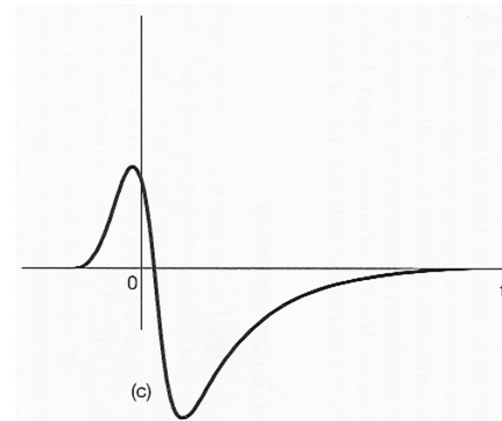
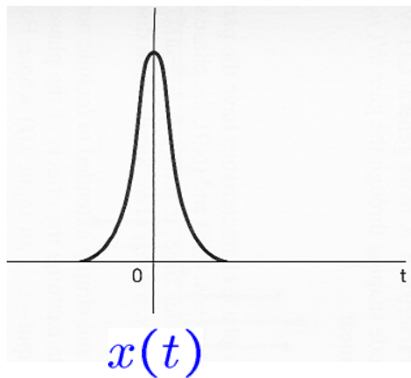
$$y(t) = x(t - 10)$$

$$t_0 = 10$$

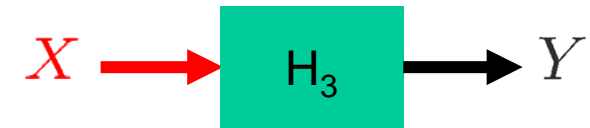
▪ Non-Linear Phase:



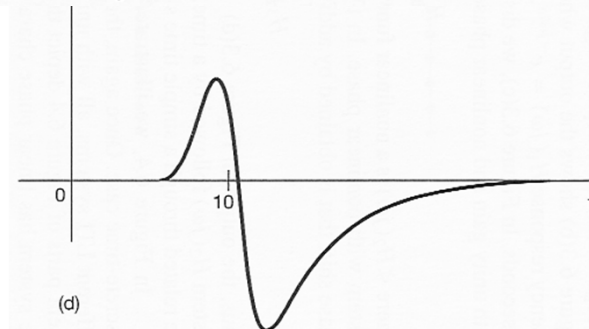
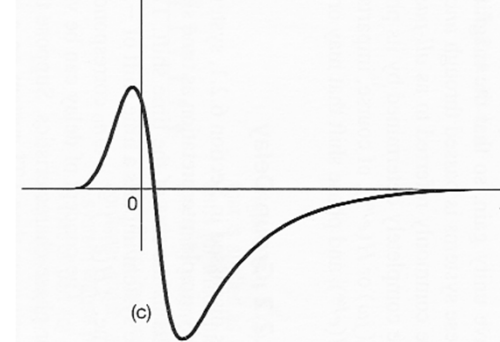
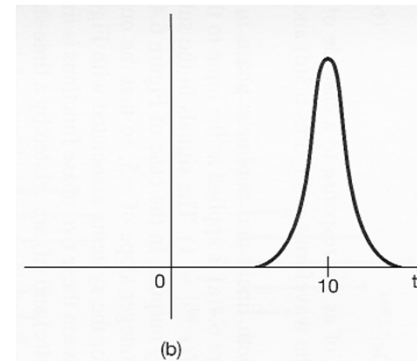
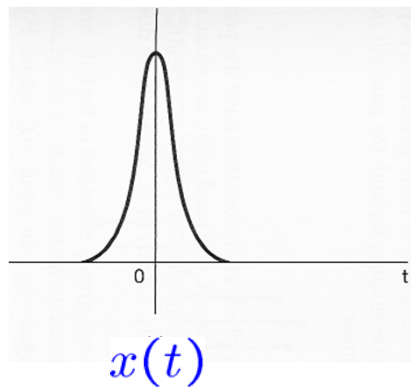
$$H_2(j\omega) = e^{jf(\omega)}$$



Linear & Non-Linear Phase:



$$H_3(j\omega) = H_2(j\omega) H_1(j\omega) = H_2(j\omega) e^{-j\omega t_0} = e^{j(f(\omega) - \omega t_0)}$$



■ Group Delay & Phase:

• Linear Phase & Delay:

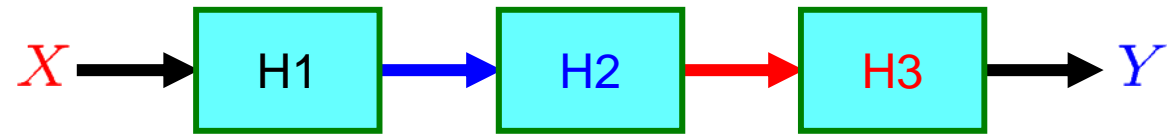
$$H_1(j\omega) = e^{-j\omega t_0} \quad \Rightarrow \quad y(t) = x(t - t_0) \quad \Rightarrow \quad \text{delay} = t_0$$

$$H_1(e^{j\omega}) = e^{-j\omega n_0} \quad \Rightarrow \quad y[n] = x[n - n_0] \quad \Rightarrow \quad \text{delay} = n_0$$

• Nonlinear Phase & Group Delay

$$\begin{aligned} H_2(j\omega) = e^{jf(\omega)} & \quad \Rightarrow \quad \tau(\omega) = -\frac{d}{d\omega} \left\{ \cancel{H_2(j\omega)} \right\} \\ & \quad \quad \quad = -\frac{d}{d\omega} \left\{ f(\omega) \right\} \end{aligned}$$

▪ Example 6.1:



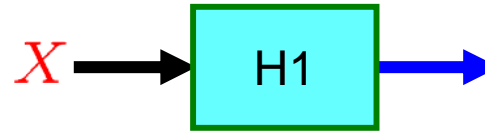
$$H(j\omega) = H_1(j\omega) H_2(j\omega) H_3(j\omega)$$

$$H_i(j\omega) = \frac{(\omega_i)^2 + (j\omega)^2 - 2\zeta_i\omega_i(j\omega)}{(\omega_i)^2 + (j\omega)^2 + 2\zeta_i\omega_i(j\omega)} = \frac{1 + (\frac{j\omega}{\omega_i})^2 - 2j\zeta_i(\frac{\omega}{\omega_i})}{1 + (\frac{j\omega}{\omega_i})^2 + 2j\zeta_i(\frac{\omega}{\omega_i})}$$

$$\Rightarrow \begin{cases} |H_i(j\omega)| = 1 \\ \angle H_i(j\omega) = -2 \arctan \left[\frac{2\zeta_i(\frac{\omega}{\omega_i})}{1 - (\frac{\omega}{\omega_i})^2} \right] \end{cases}$$

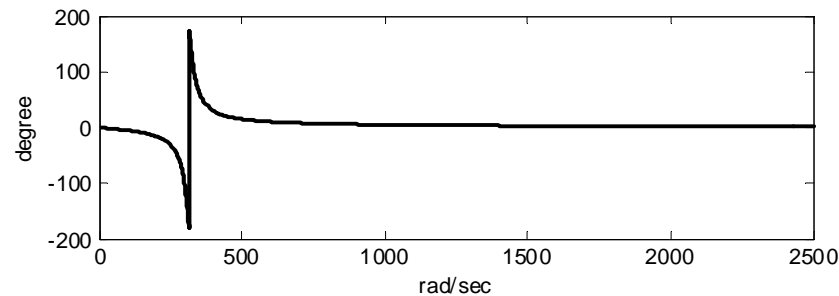
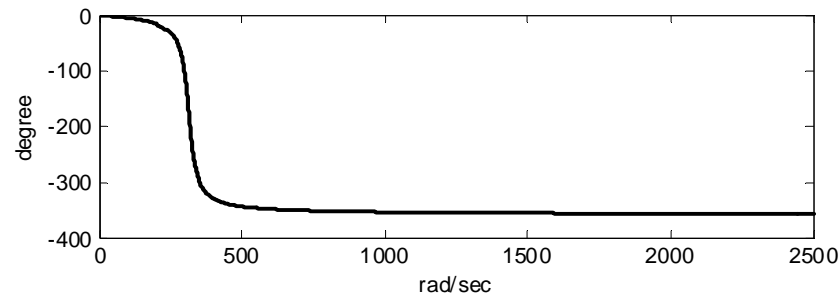
$$\Rightarrow \begin{cases} |H(j\omega)| = 1 \\ \angle H(j\omega) = \angle H_1(j\omega) + \angle H_2(j\omega) + \angle H_3(j\omega) \end{cases}$$

$$\Rightarrow \tau(\omega) = -\frac{d}{d\omega} \left\{ \angle H(j\omega) \right\}$$

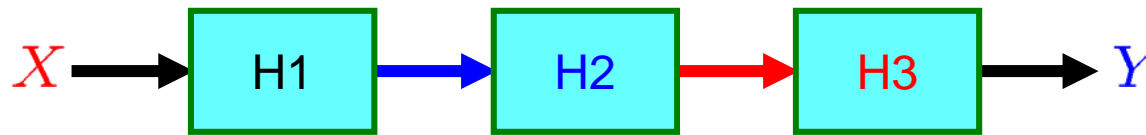


$$H_1(j\omega) = \frac{1 + (j\frac{\omega}{\omega_1})^2 - 2j\zeta_1(\frac{\omega}{\omega_1})}{1 + (j\frac{\omega}{\omega_1})^2 + 2j\zeta_1(\frac{\omega}{\omega_1})} \quad \begin{cases} \omega_1 = 315 & \text{rad/sec} \\ \zeta_1 = 0.066 \\ f_1 \approx 50 & \text{Hz} \end{cases}$$

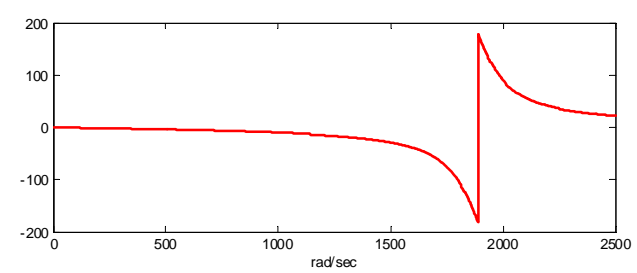
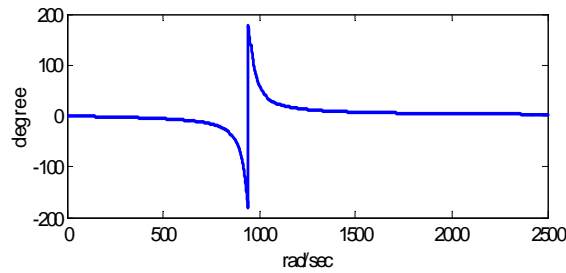
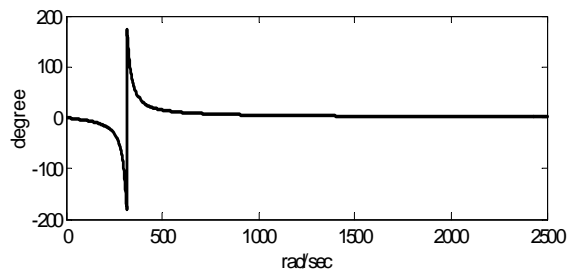
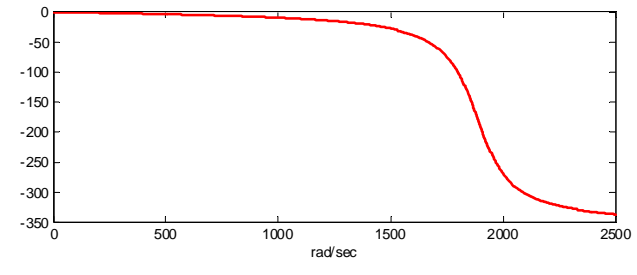
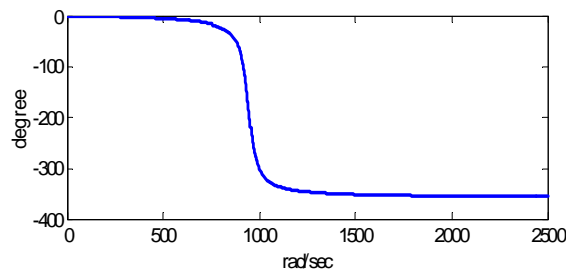
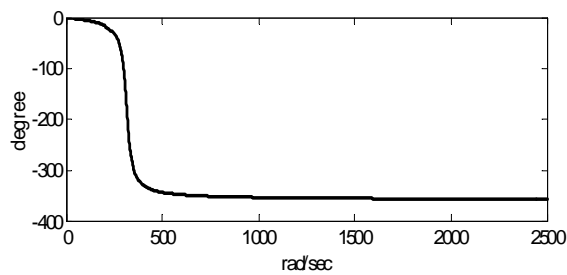
$$\Rightarrow \begin{cases} |H_1(j\omega)| = 1 \\ \angle H_1(j\omega) = -2 \arctan \left[\frac{2\zeta_1(\frac{\omega}{\omega_1})}{1 - (\frac{\omega}{\omega_1})^2} \right] \end{cases}$$



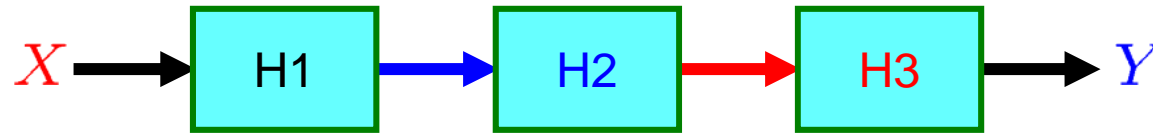
Magnitude-Phase Representation of Freq Resp of LTI Systems



$$\begin{cases} w_1 = 315 \text{ rad/sec} \\ w_2 = 943 \text{ rad/sec} \\ w_3 = 1888 \text{ rad/sec} \end{cases}
 \quad
 \begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$



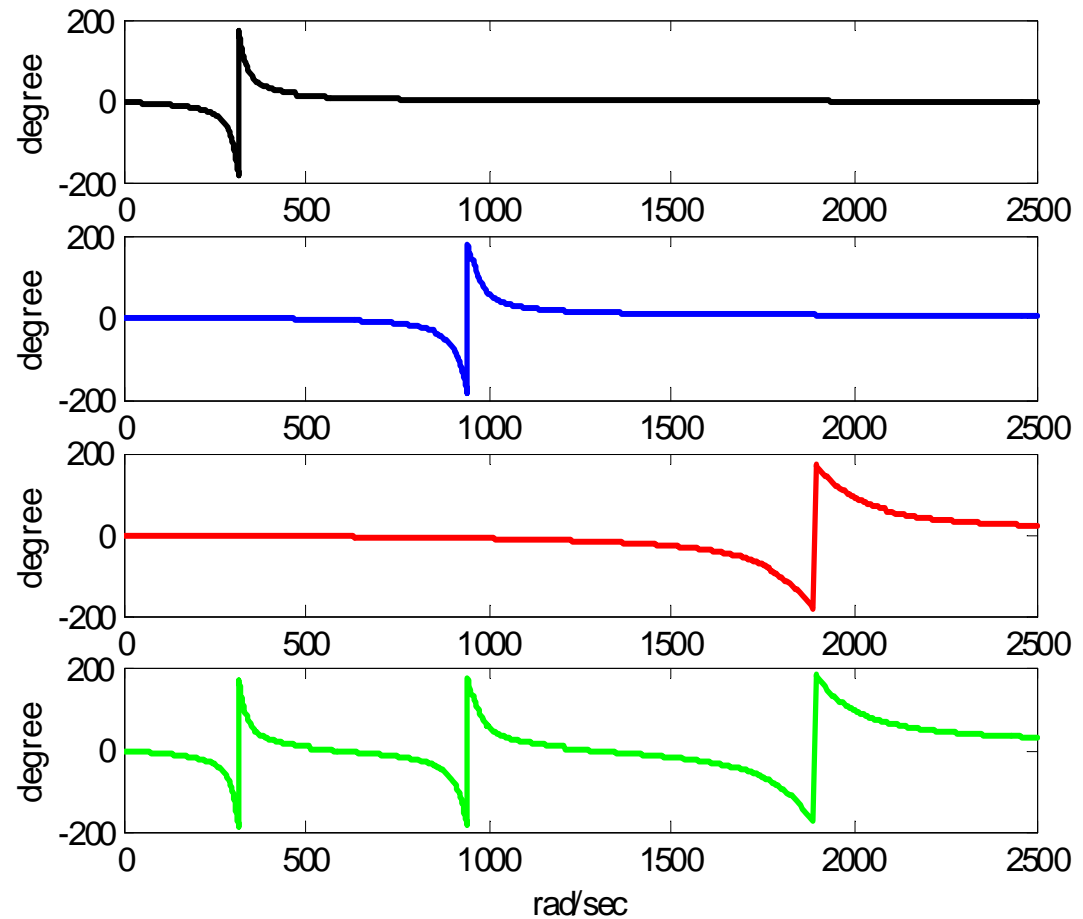
Magnitude-Phase Representation of Freq Resp of LTI Systems



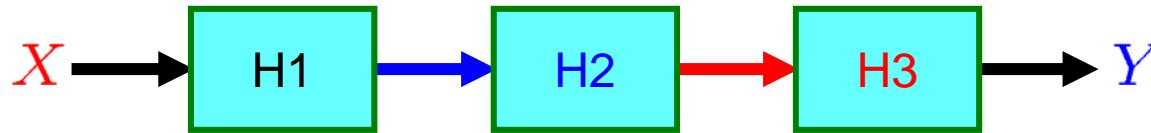
$$\begin{cases} |H(j\omega)| &= 1 \\ \angle H(j\omega) &= \angle H_1(j\omega) + \angle H_2(j\omega) + \angle H_3(j\omega) \end{cases}$$

$$\begin{cases} \omega_1 &= 315 \text{ rad/sec} \\ \omega_2 &= 943 \text{ rad/sec} \\ \omega_3 &= 1888 \text{ rad/sec} \end{cases}$$

$$\begin{cases} \zeta_1 &= 0.066 \\ \zeta_2 &= 0.033 \\ \zeta_3 &= 0.058 \end{cases}$$



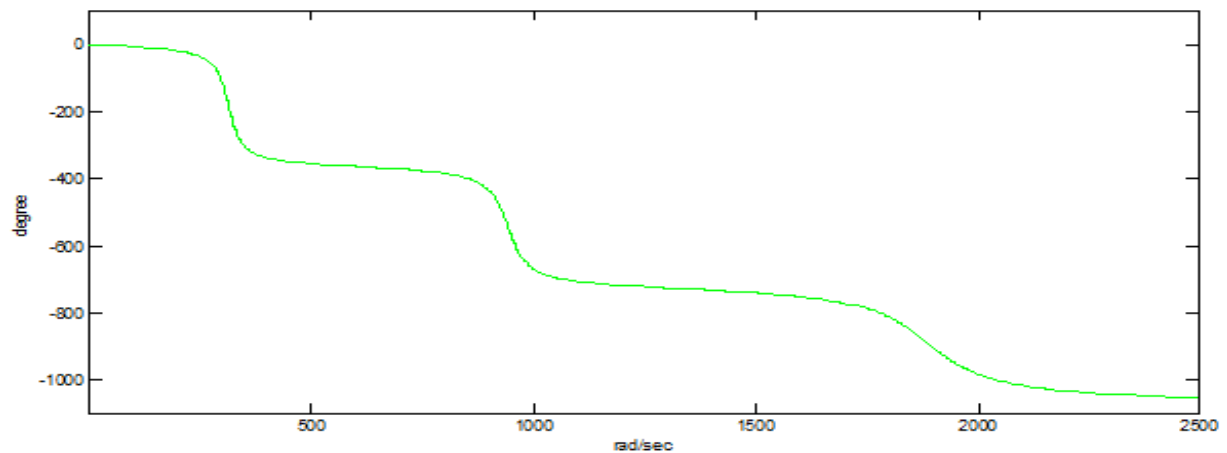
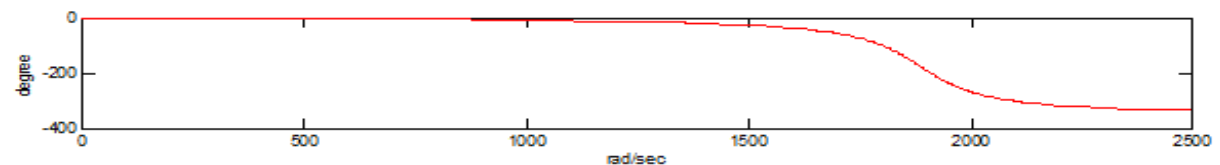
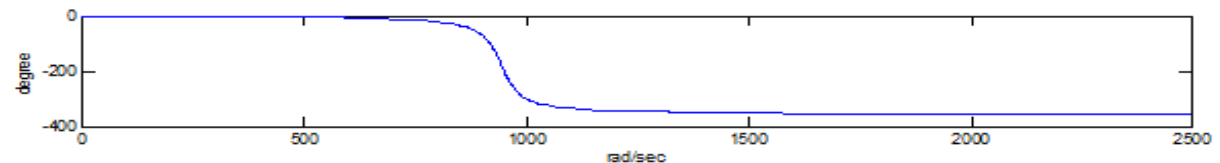
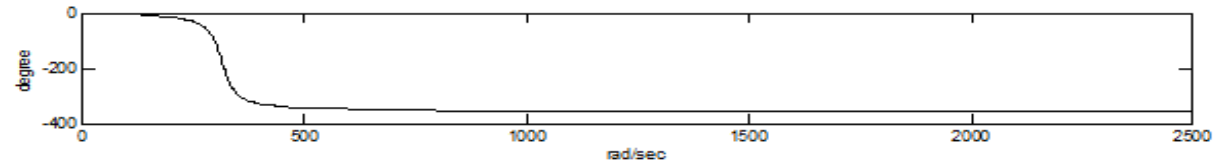
Magnitude-Phase Representation of Freq Resp of LTI Systems



$$\begin{cases} |H(j\omega)| = 1 \\ \angle H(j\omega) = \angle H_1(j\omega) + \angle H_2(j\omega) + \angle H_3(j\omega) \end{cases}$$

$$\begin{cases} w_1 = 315 \text{ rad/sec} \\ w_2 = 943 \text{ rad/sec} \\ w_3 = 1888 \text{ rad/sec} \end{cases}$$

$$\begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$



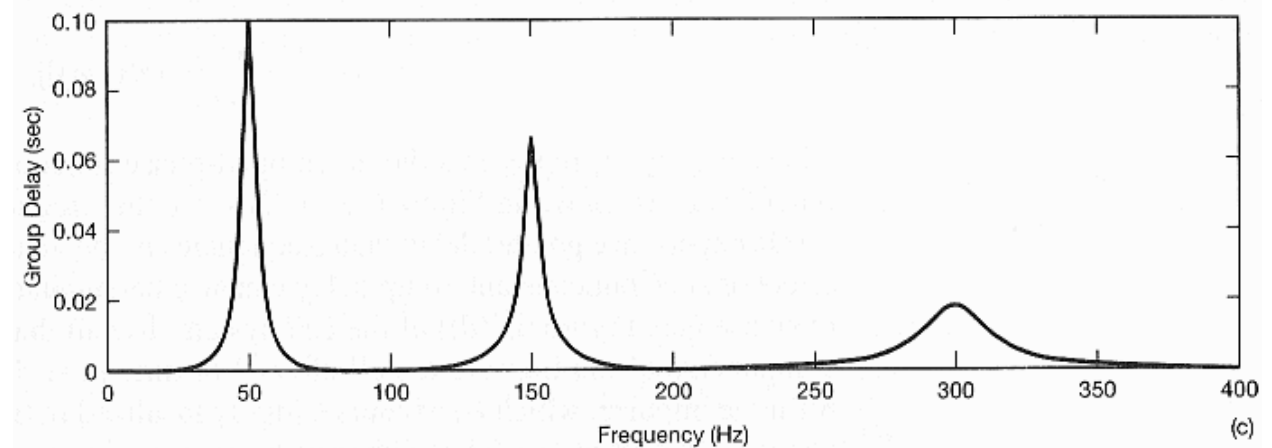
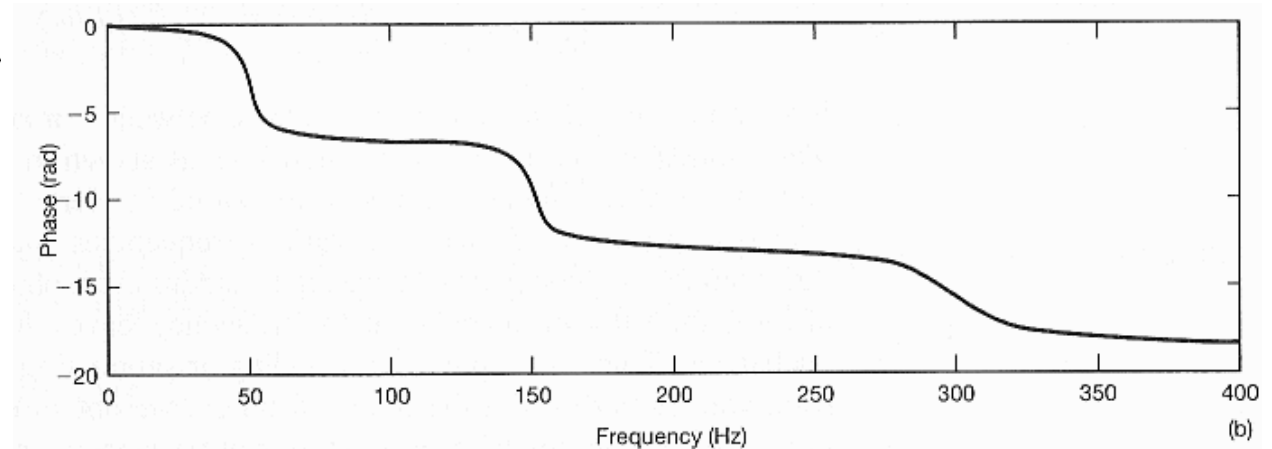
$$\tau(\omega) = -\frac{d}{d\omega} \{ \angle H(j\omega) \}$$

$$\begin{cases} \omega_1 = 315 \text{ rad/sec} \\ \omega_2 = 943 \text{ rad/sec} \\ \omega_3 = 1888 \text{ rad/sec} \end{cases}$$

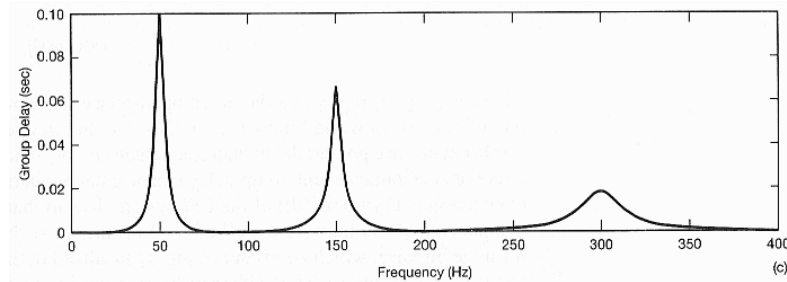
$$\begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$

$$\omega_i = 2\pi f_i$$

$$\begin{cases} f_1 \approx 50 \text{ Hz} \\ f_2 \approx 150 \text{ Hz} \\ f_3 \approx 300 \text{ Hz} \end{cases}$$

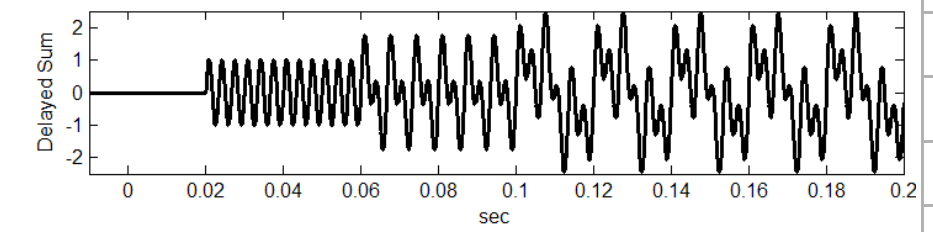
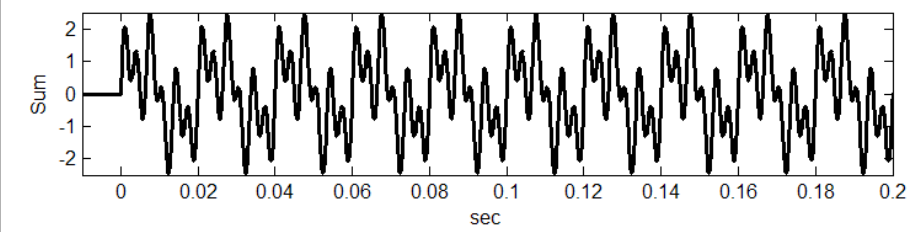
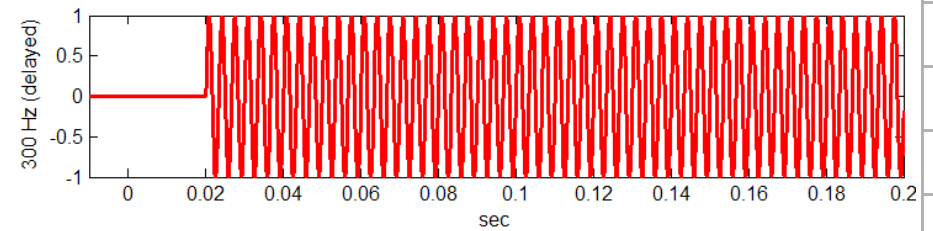
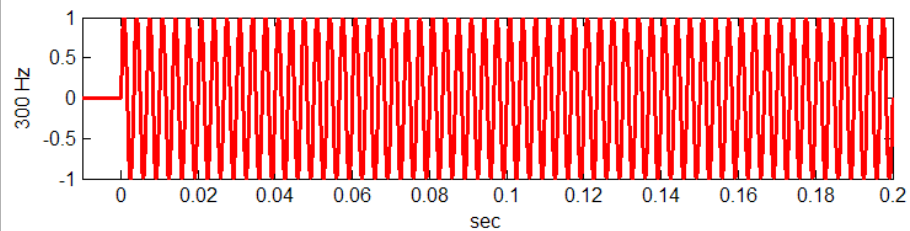
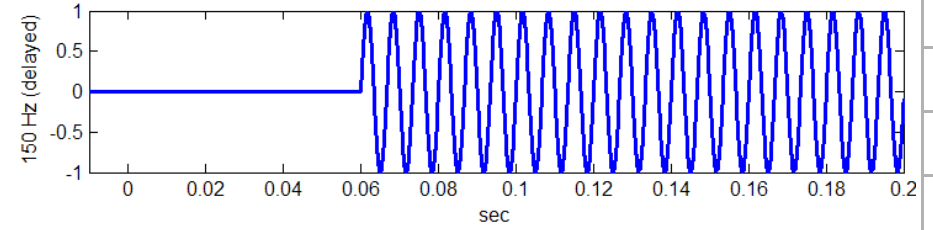
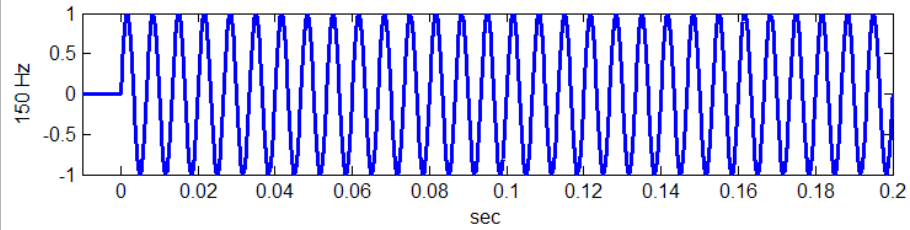
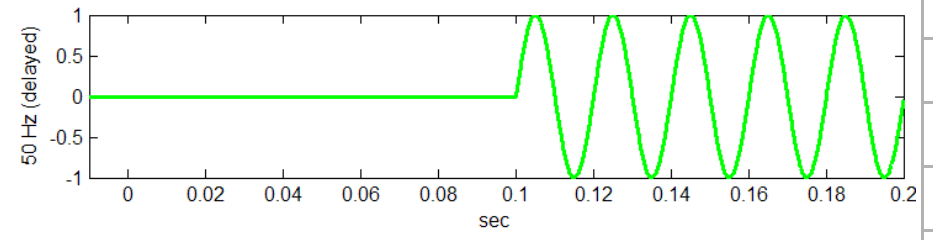
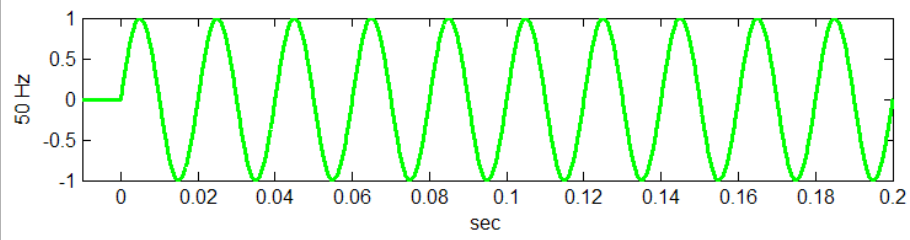


Magnitude-Phase Representation of Freq Resp of LTI Systems



$$x(t) = x_1(t) + x_2(t) + x_3(t)$$

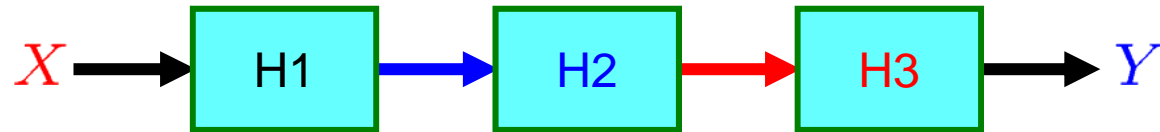
$$y(t) = y_1(t) + y_2(t) + y_3(t)$$



Magnitude-Phase Representation of Freq Resp of LTI Systems

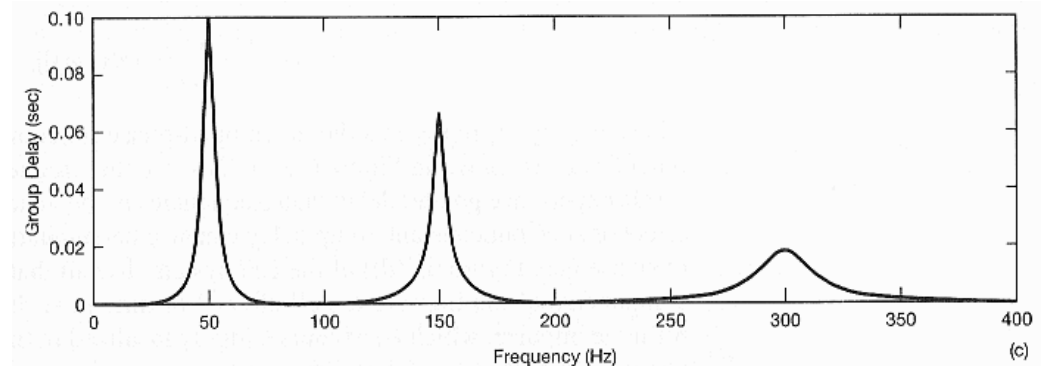
$$x(t) = \delta(t)$$

$$X(j\omega) = 1, \forall \omega$$



$$\begin{cases} |H(j\omega)| = 1 \\ \angle H(j\omega) = \angle H_1(j\omega) + \angle H_2(j\omega) + \angle H_3(j\omega) \end{cases}$$

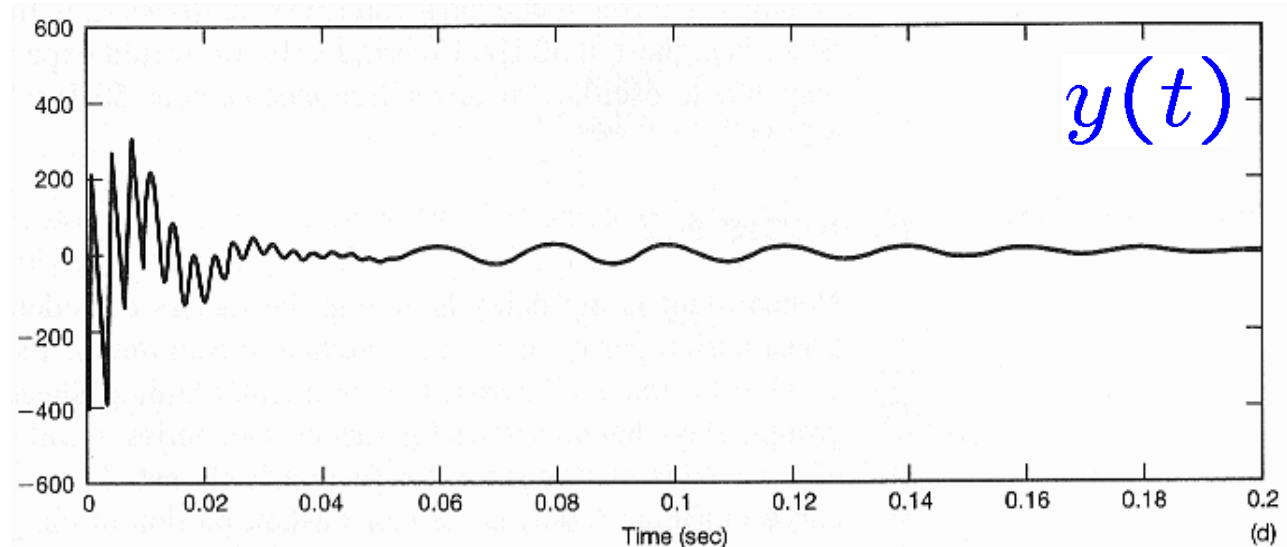
$$\begin{cases} \omega_1 = 315 \text{ rad/sec} \\ \omega_2 = 943 \text{ rad/sec} \\ \omega_3 = 1888 \text{ rad/sec} \end{cases}$$



$$\begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$

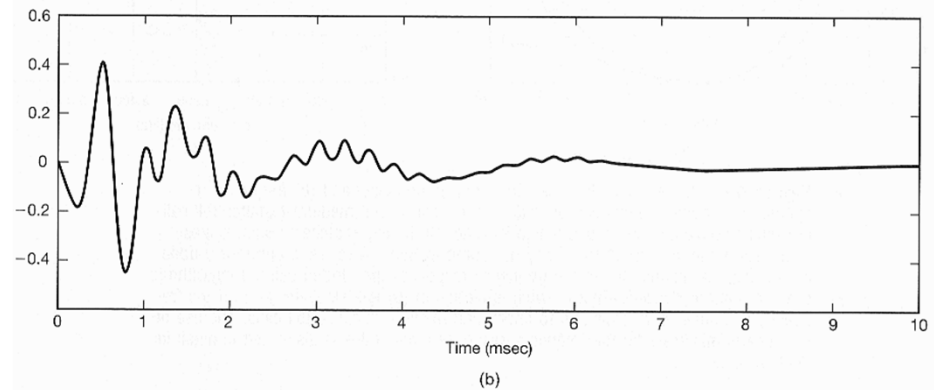
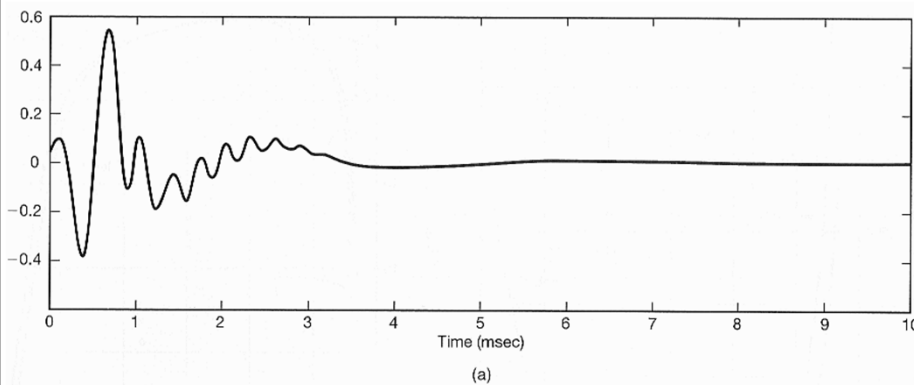
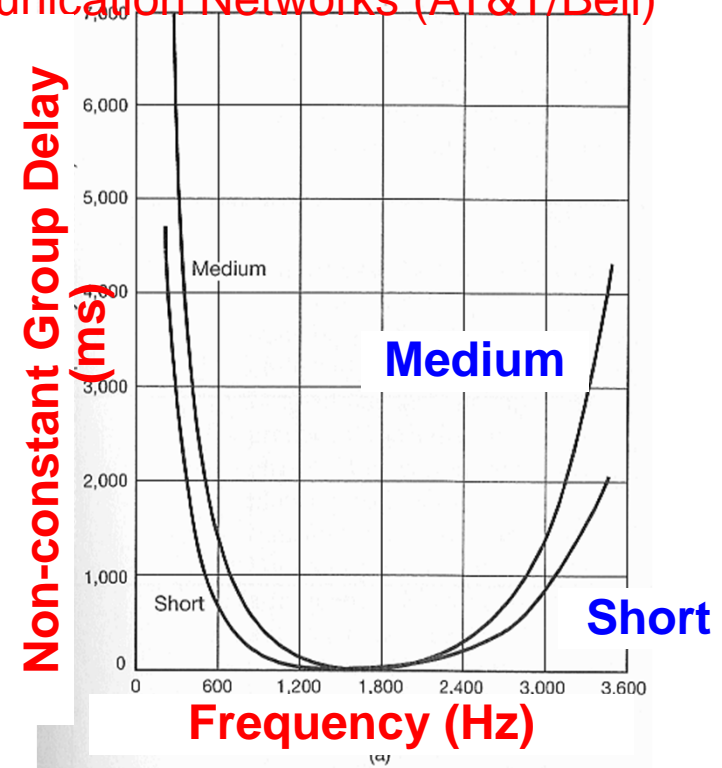
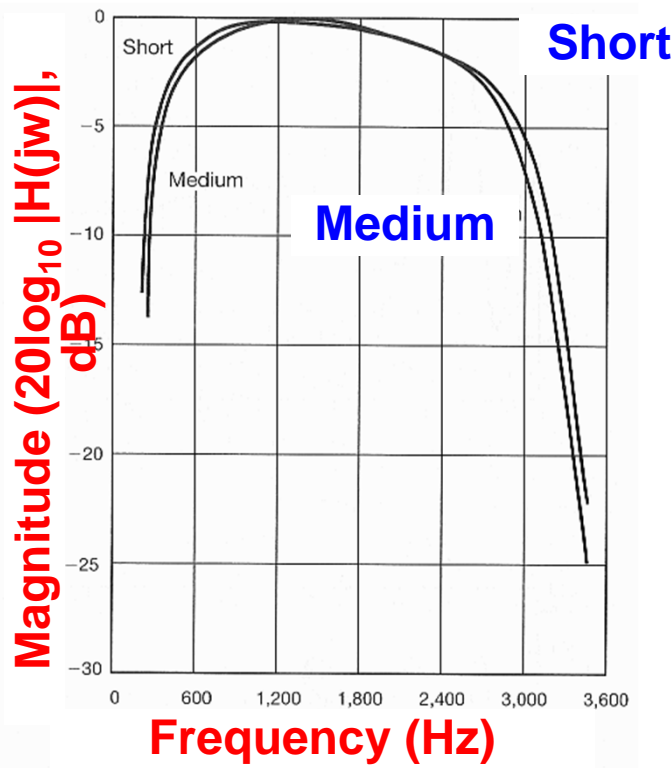
$$\omega_i = 2\pi f_i$$

$$\begin{cases} f_1 \approx 50 \text{ Hz} \\ f_2 \approx 150 \text{ Hz} \\ f_3 \approx 300 \text{ Hz} \end{cases}$$

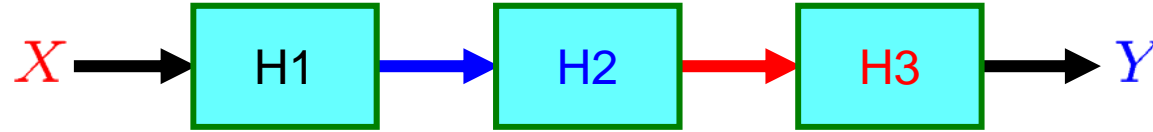


Example 6.2:

Analog Transmission Performance on the Switched Telecommunication Networks (AT&T/Bell)

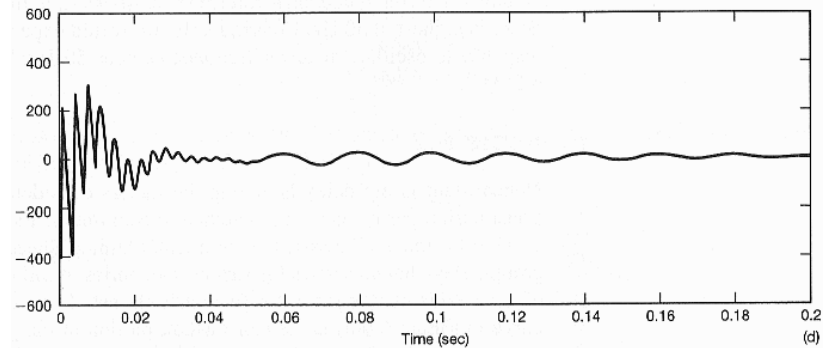
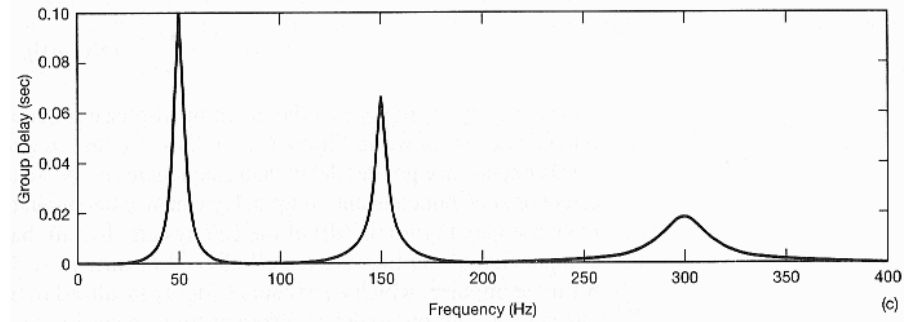
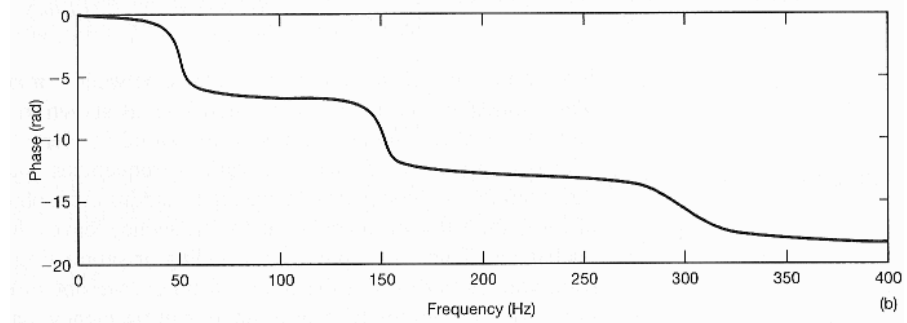


Phase Distortion and Group Delay



$$\tau(\omega) = - \frac{d}{d\omega} \{ \angle H(j\omega) \}$$

$$x(t) = \delta(t)$$



- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters [\(p.439\)](#)
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

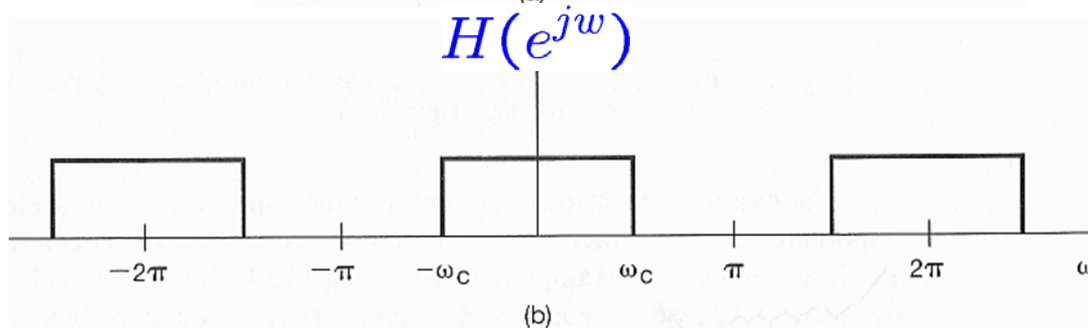
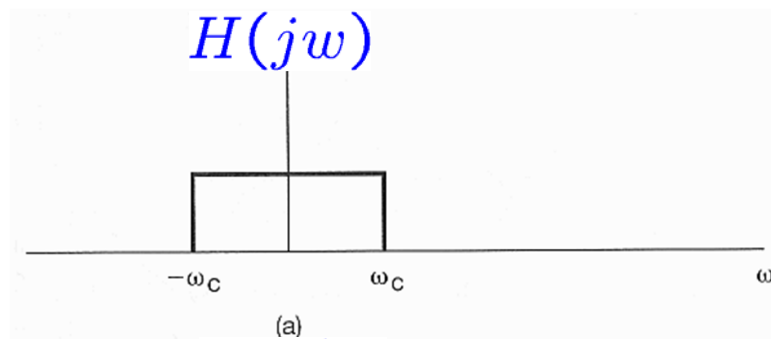
▪ Ideal Lowpass Filters:

$$H(j\omega) = \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & |\omega| > \omega_c \end{cases}$$

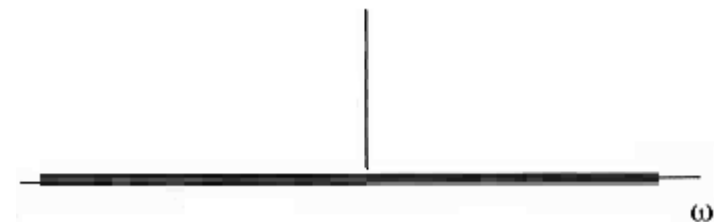
$$H(e^{j\omega}) = \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & \omega_c < |\omega| \leq \pi \end{cases}$$

– unit gain

– zero phase distortion

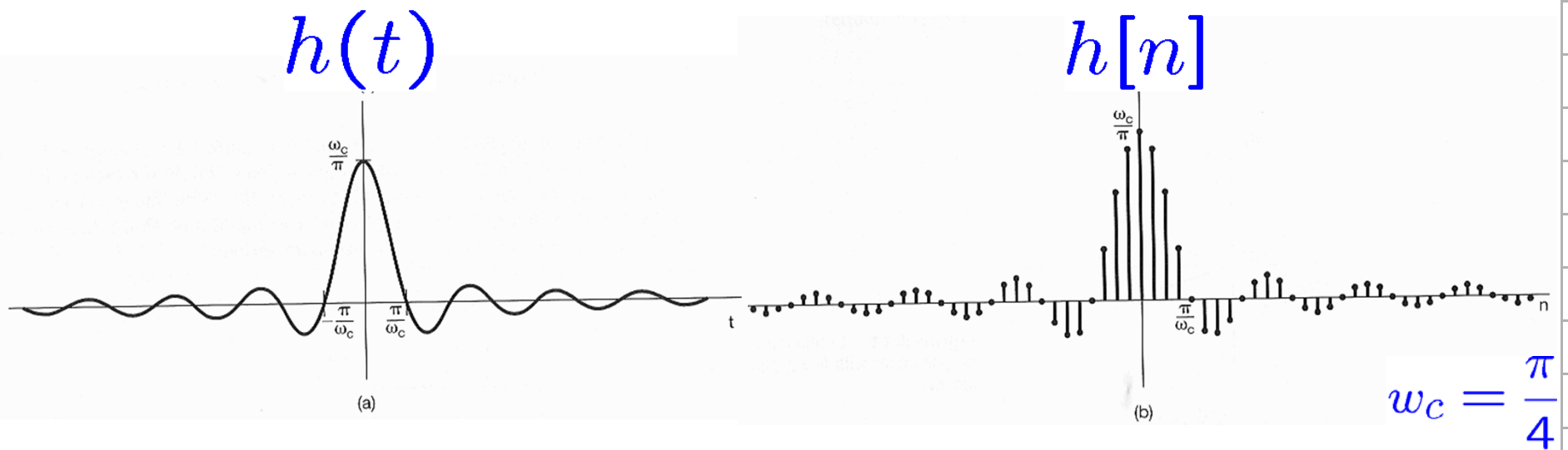


~~$H(j\omega)$~~ ~~$H(e^{j\omega})$~~

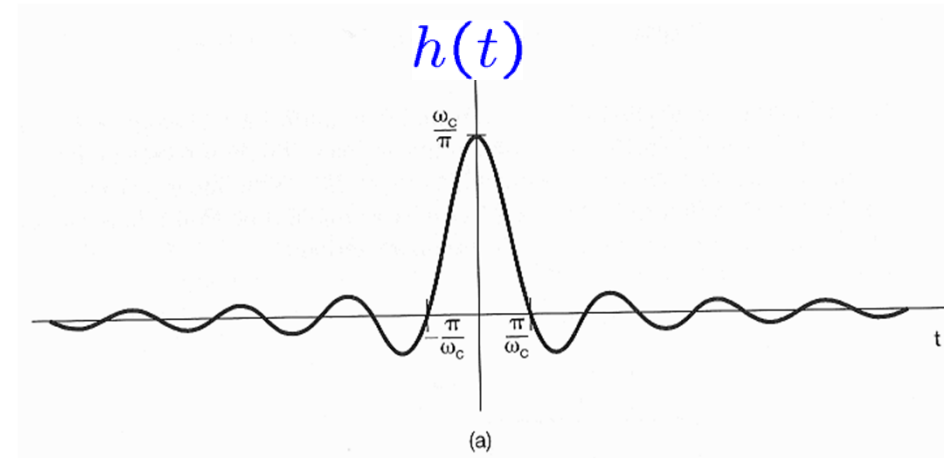
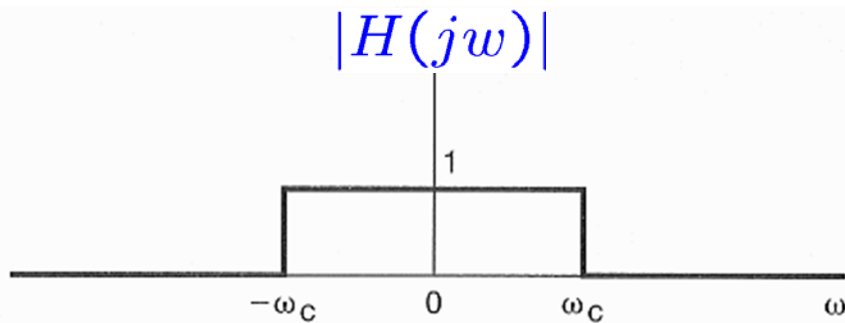


▪ Ideal Lowpass Filters:

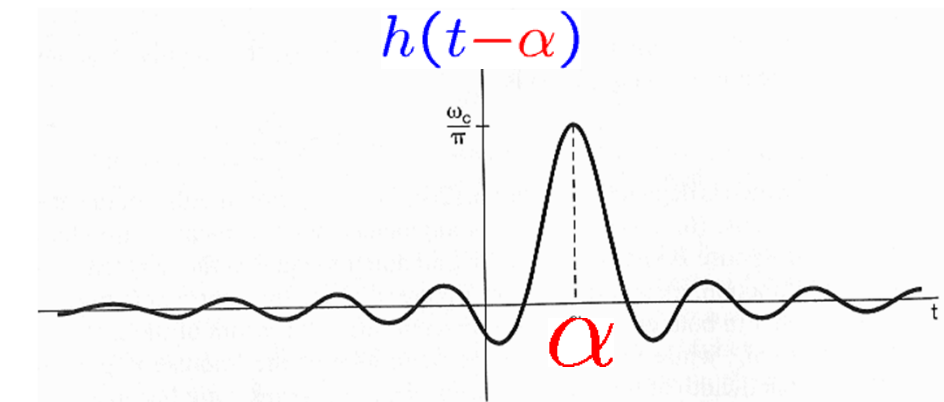
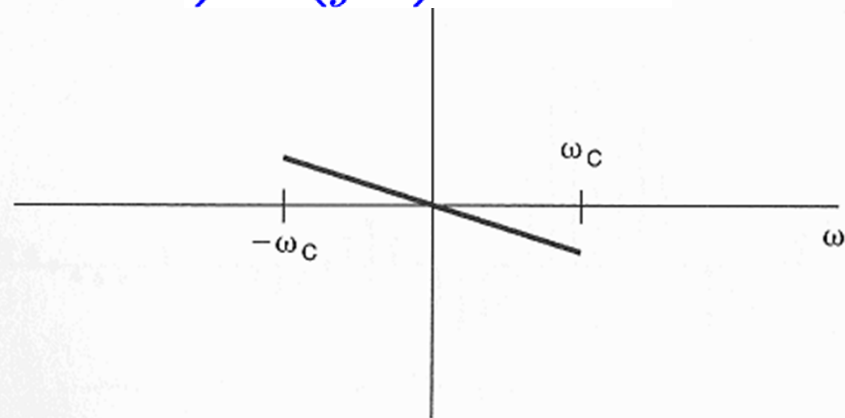
$$\begin{aligned}
 H(j\omega) &= \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & |\omega| > \omega_c \end{cases} \\
 H(e^{j\omega}) &= \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & \omega_c < |\omega| \leq \pi \end{cases}
 \end{aligned}
 \Rightarrow
 \begin{cases} h(t) = \frac{\sin \omega_c t}{\pi t} \\ h[n] = \frac{\sin \omega_c n}{\pi n} \end{cases}$$



▪ Ideal Lowpass Filters with Linear Phase:

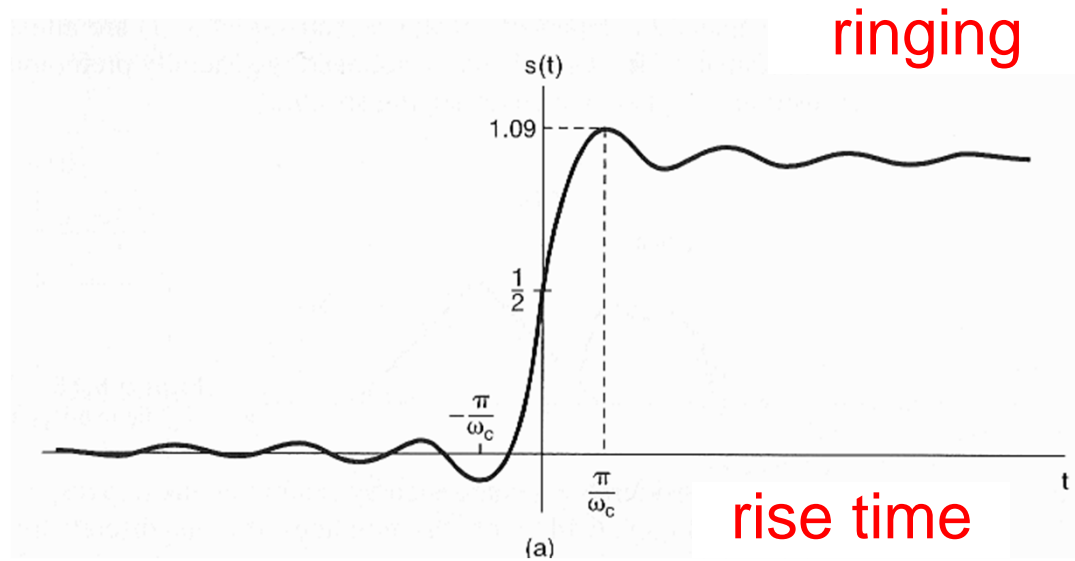
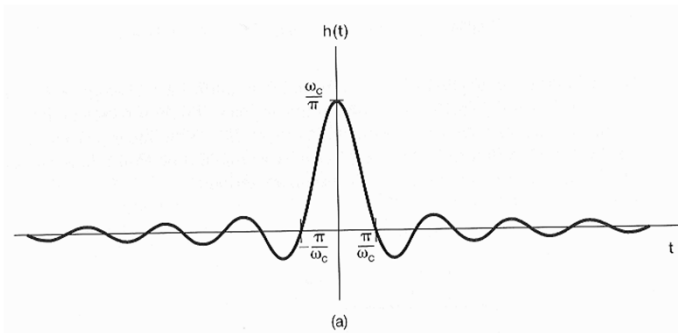


$\angle H(j\omega) = -\alpha\omega$

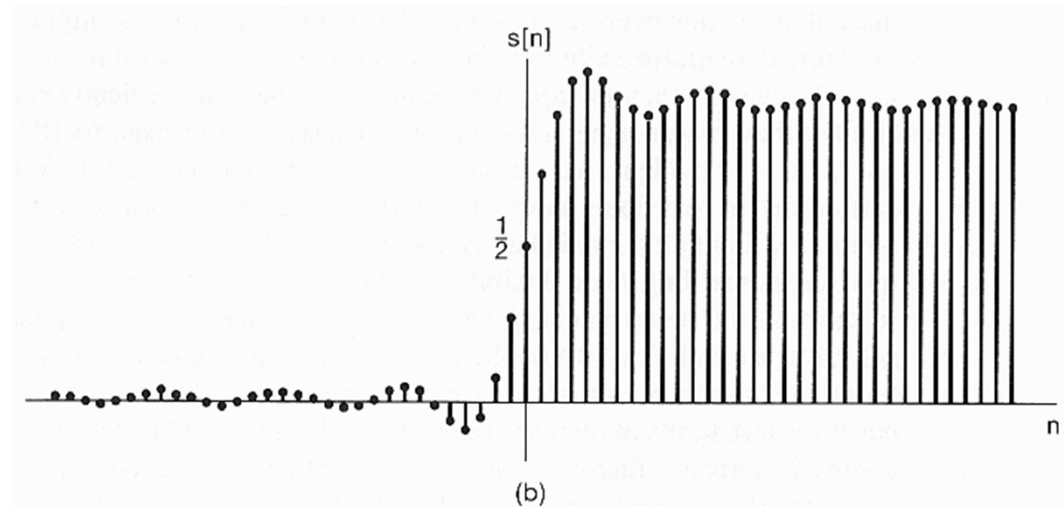
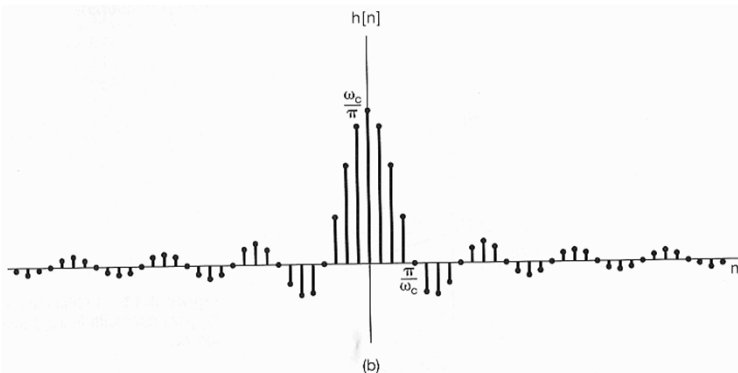


▪ Step Response of Ideal Lowpass Filters:

$$s(t) = \int_{-\infty}^t h(\tau) d\tau$$

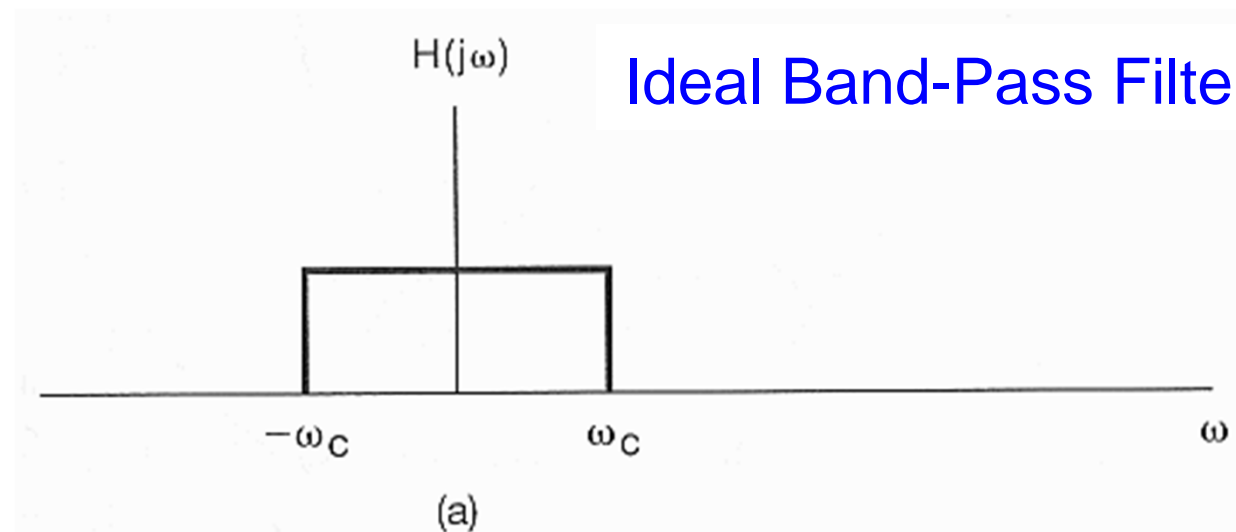
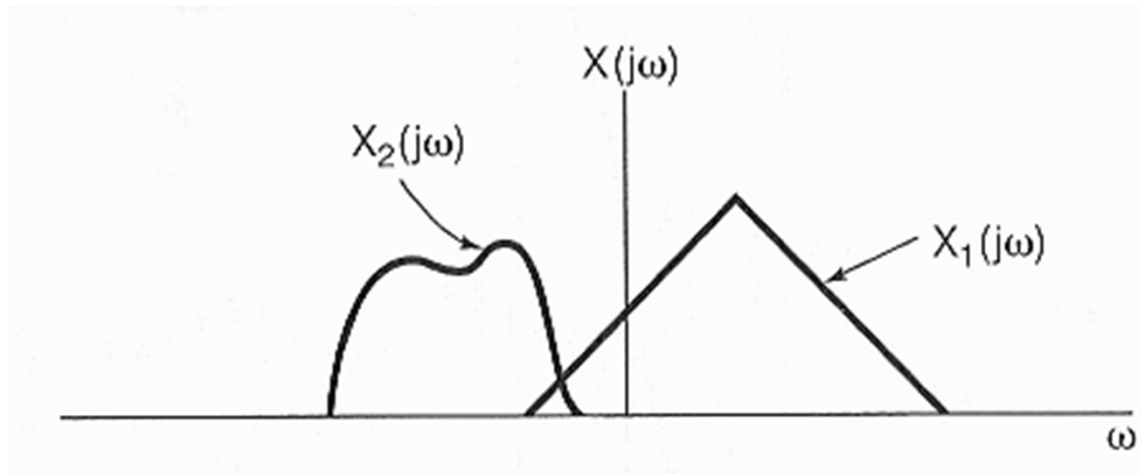


$$s[n] = \sum_{m=-\infty}^n h[m]$$



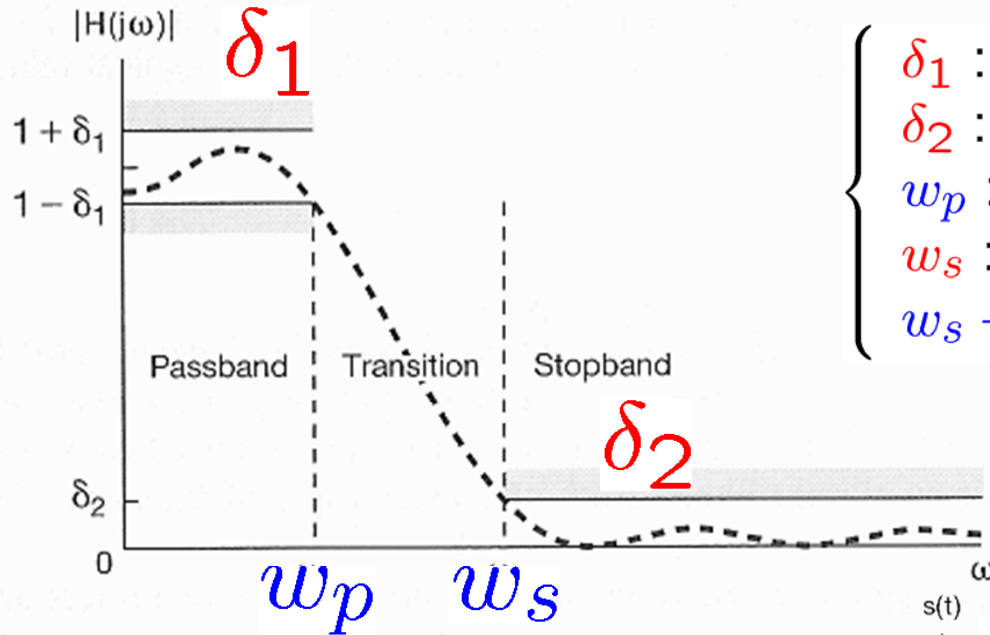
- The Magnitude-Phase Representation of the Fourier Transform
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- 1st-Order & 2nd-Order Discrete-Time Systems
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Overlapping Spectra:



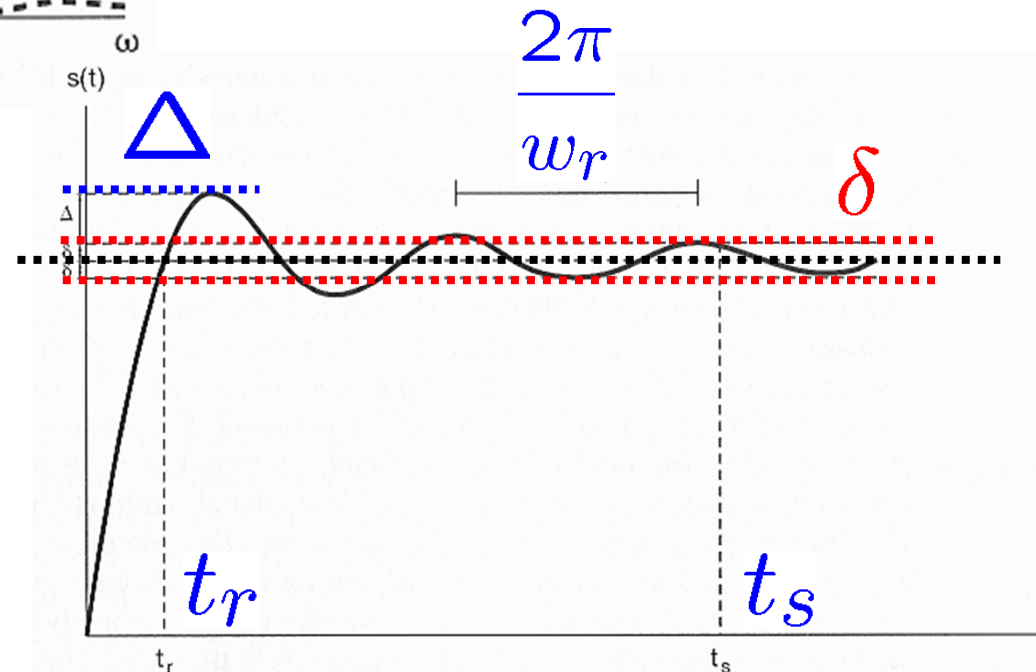
Ideal Band-Pass Filter ?

Desired Filter Characteristics:



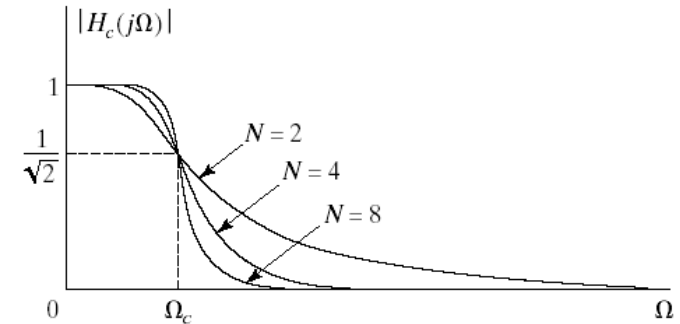
- δ_1 : allowable passband ripple
- δ_2 : allowable stopband ripple
- ω_p : passband edge
- ω_s : stopband edge
- $\omega_s - \omega_p$: transition band

- Δ : overshoot
- δ : steady-state error
- ω_r : ringing frequency
- t_r : rise time
- t_s : settling time



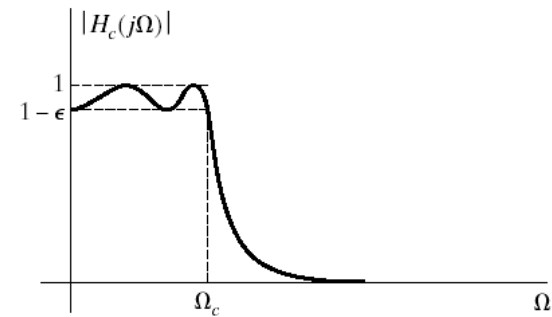
- Three Frequently Used Filters:
 - Butterworth, Chebyshev, Elliptic filters

$$|H_c(j\Omega)|^2 = \frac{1}{1 + (\frac{j\Omega}{j\Omega_c})^{2N}}$$



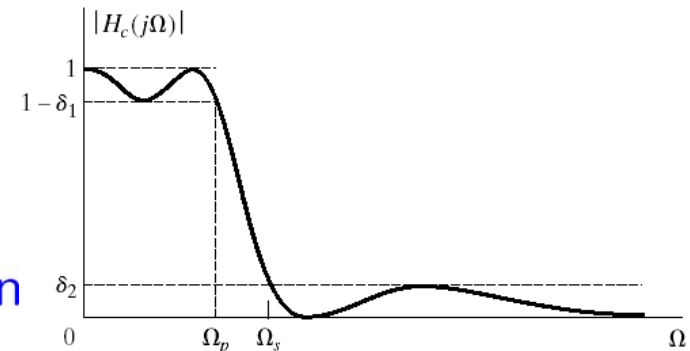
$$|H_c(j\Omega)|^2 = \frac{1}{1 + \epsilon^2 V_N^2(\frac{\Omega}{\Omega_c})}$$

$$V_N(x) = \cos(N \cos^{-1} x)$$



$$|H_c(j\Omega)|^2 = \frac{1}{1 + \epsilon^2 U_N^2(\Omega)}$$

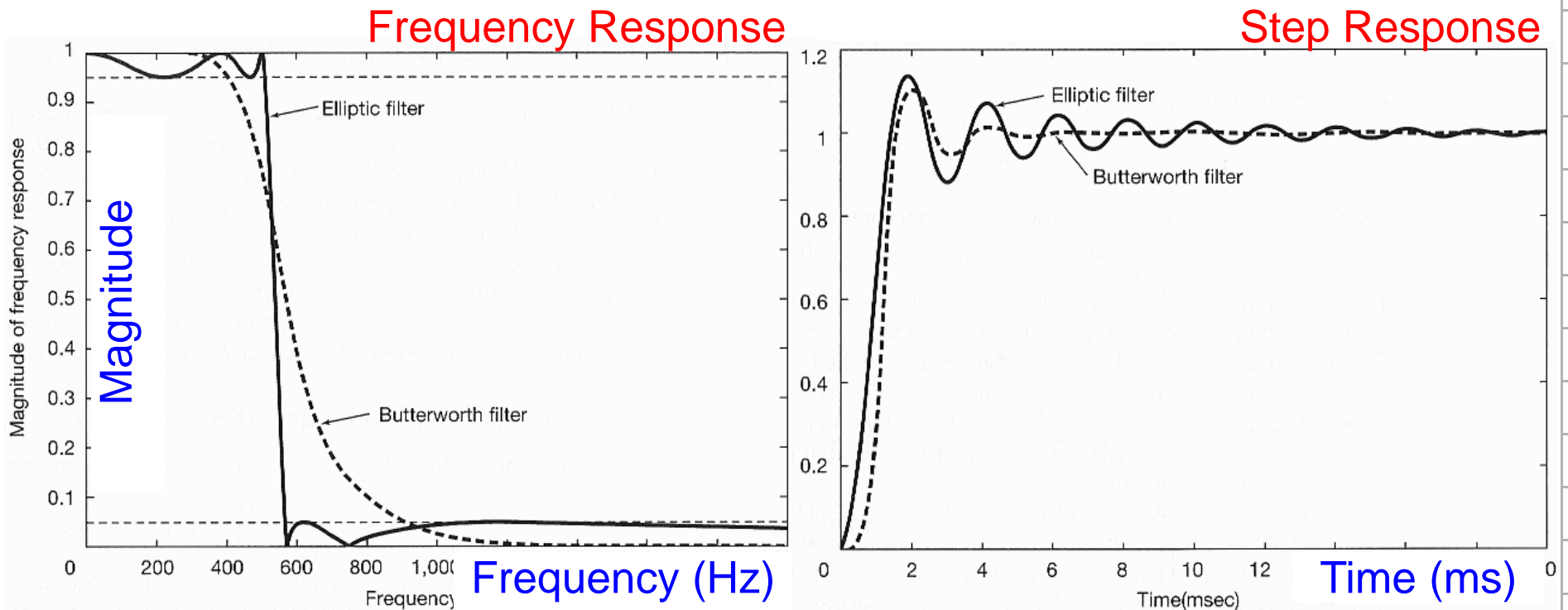
$U_N(x)$: Jacobian elliptic function



■ Example 6.3: Two Frequently Used Filters:

- Butterworth filter
- Elliptic filter

Fifth-order rational frequency response
Cutoff frequency = 500 Hz



- The Magnitude-Phase Representation of the Fourier Transform
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▪ DT Non-recursive Filters:

• Recursive or infinite impulse response (IIR) filters

> Impossible to design a causal, recursive filter with exactly linear phase (related to time delay)

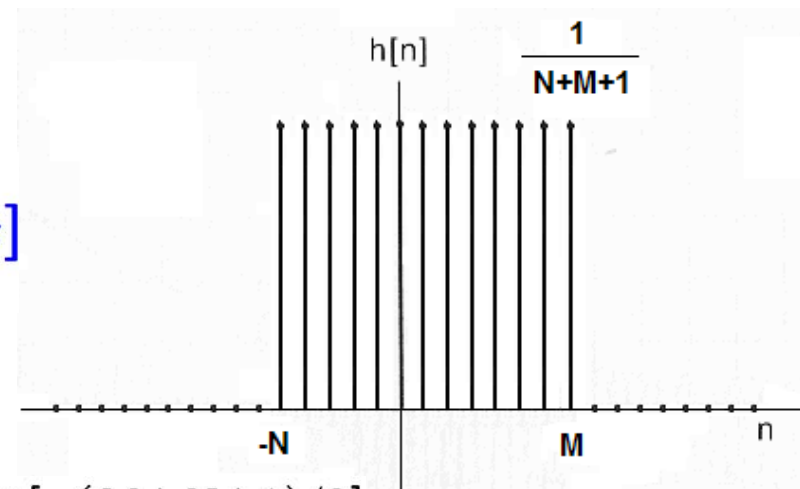
$$y[n] - a y[n - 1] = x[n] \quad |a| < 1 \Rightarrow H(e^{j\omega}) = \frac{1}{1 - ae^{-j\omega}}$$

• Non-recursive or finite impulse response (FIR) filters

> Can have exactly linear phase (related to time delay)

ss3-105

$$y[n] = \frac{1}{N + M + 1} \sum_{k=-N}^M x[n - k]$$

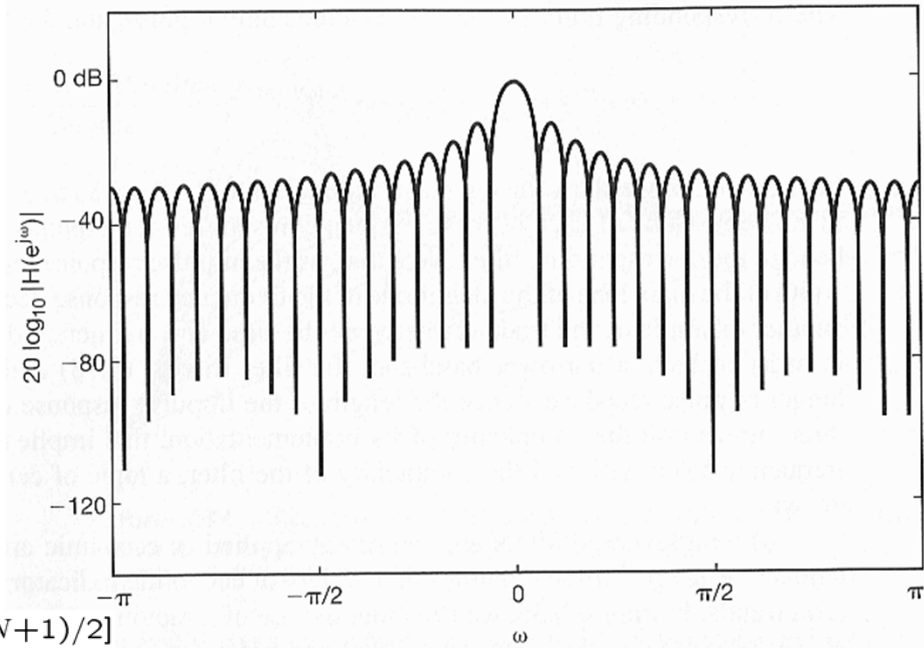


$$\Rightarrow H(e^{j\omega}) = \frac{1}{N + M + 1} e^{j\omega[(N-M)/2]} \frac{\sin[\omega(M+N+1)/2]}{\sin(\omega/2)}$$

ss3-106

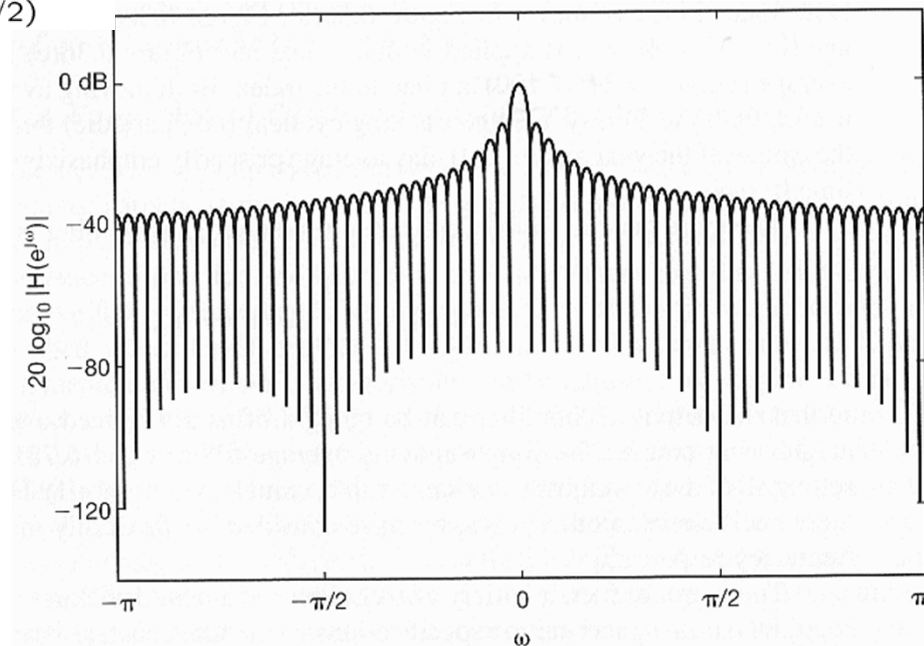
Log-Magnitude Plots:

$$N + M + 1 = 33$$

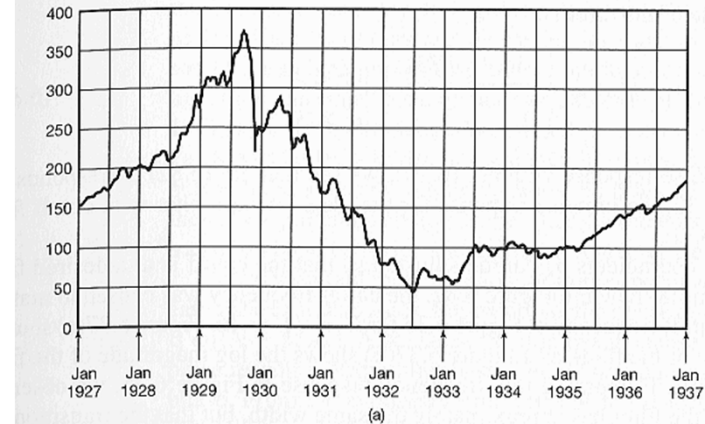


$$H(e^{jw}) = \frac{1}{N + M + 1} e^{jw[(N-M)/2]} \frac{\sin[w(M+N+1)/2]}{\sin(w/2)}$$

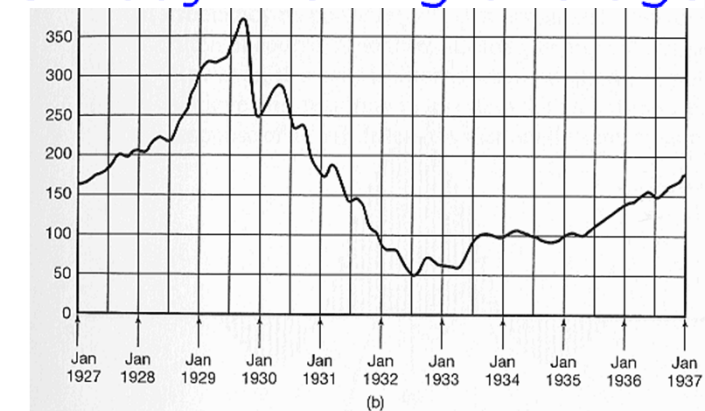
$$N + M + 1 = 65$$



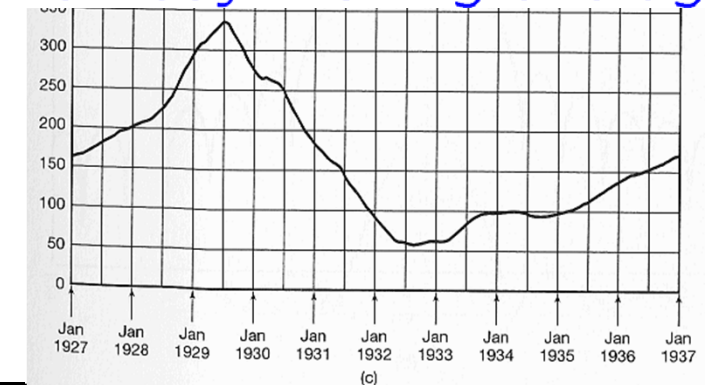
Lowpass Filtering on Dow Jones Weekly Stock Market Index:



51-day moving average



201-day moving average



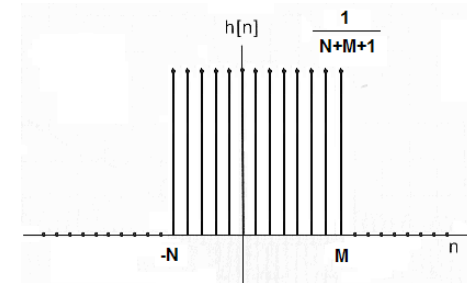
ss3-104

ss3-108

General Form of DT Non-recursive Filters:

$$y[n] = \sum_{k=-N}^M b_k x[n-k]$$

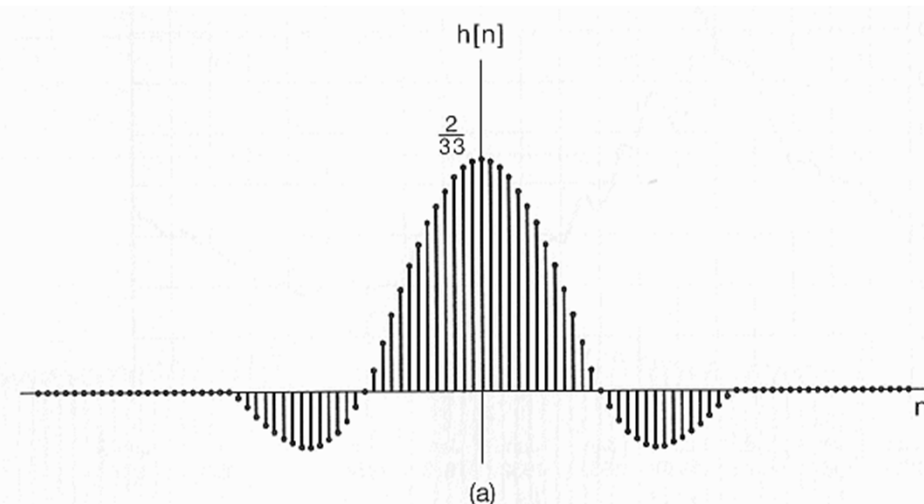
$$y[n] = \sum_{k=-N}^M \frac{1}{N+M+1} x[n-k]$$



- Let $N = M = 16$:

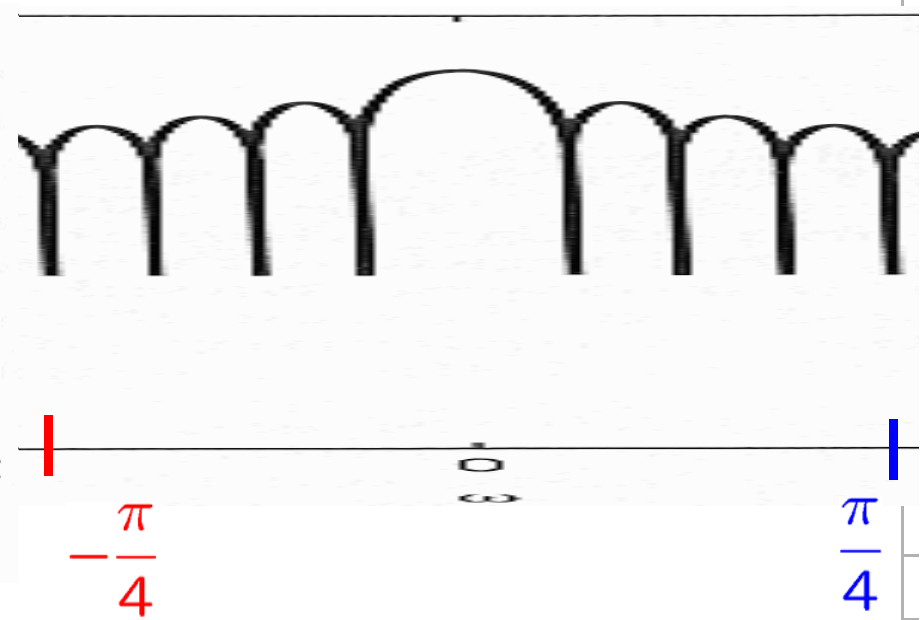
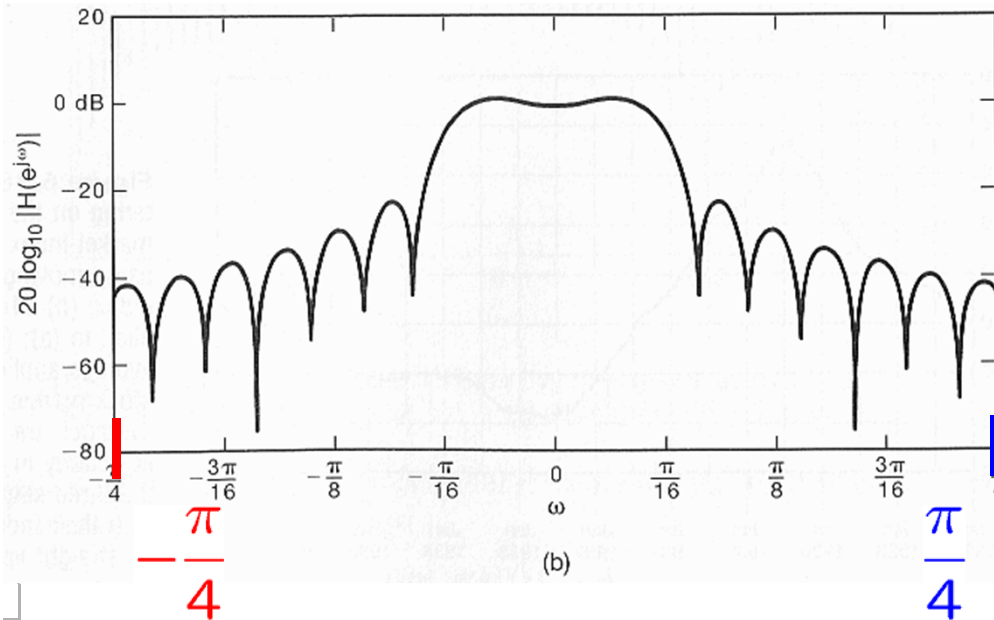
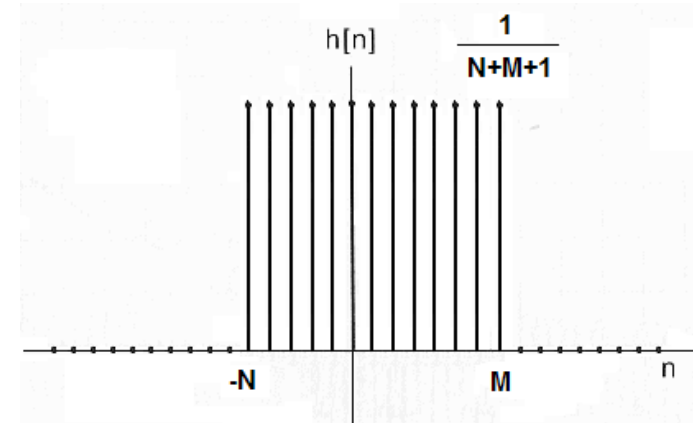
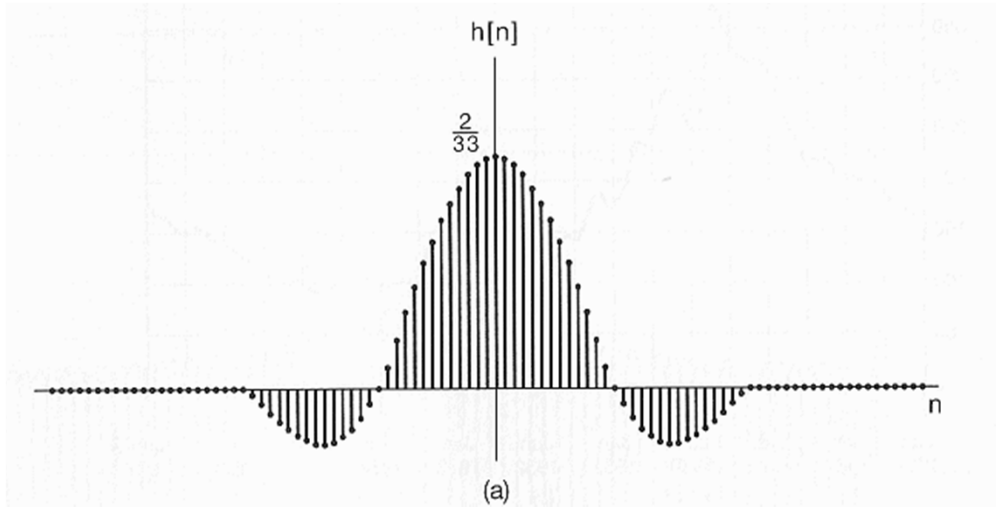
$$b_k = \begin{cases} \frac{\sin(2\pi k/33)}{\pi k}, & |k| \leq 32 \\ 0, & |k| > 32 \end{cases}$$

$$h[n] = \begin{cases} \frac{\sin(2\pi n/33)}{\pi n}, & |n| \leq 32 \\ 0, & |n| > 32 \end{cases}$$

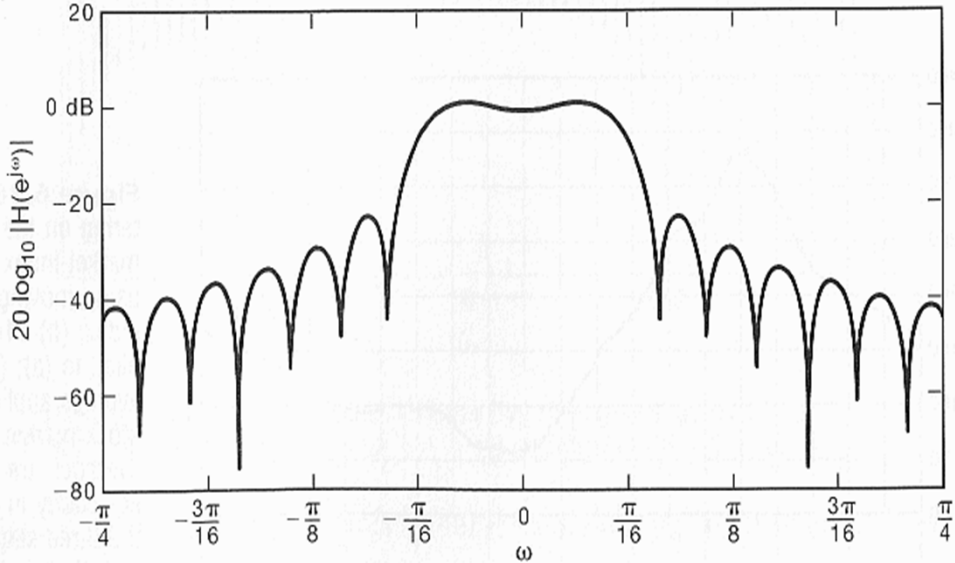


ss6-82

General Form of DT Non-recursive Filters:

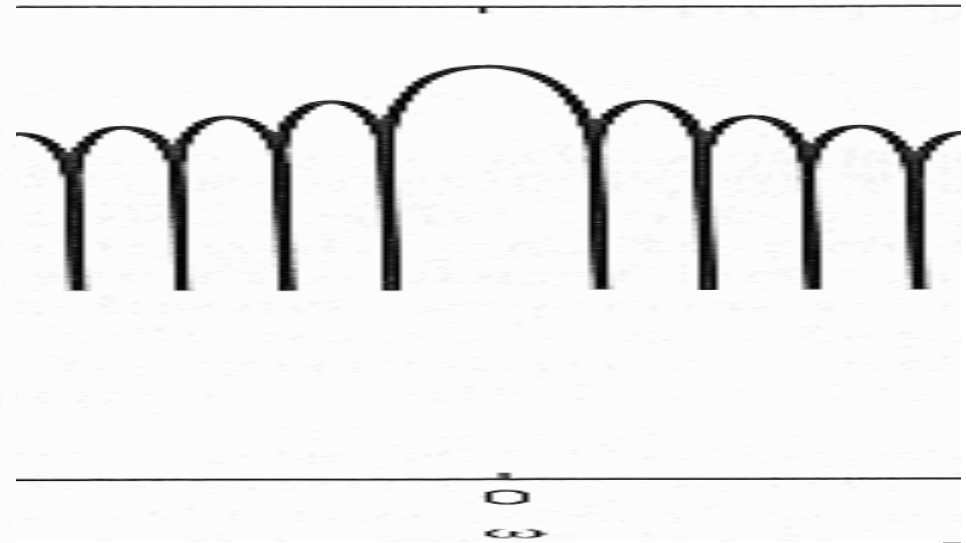


■ Comparison on a Linear Amplitude Scale:

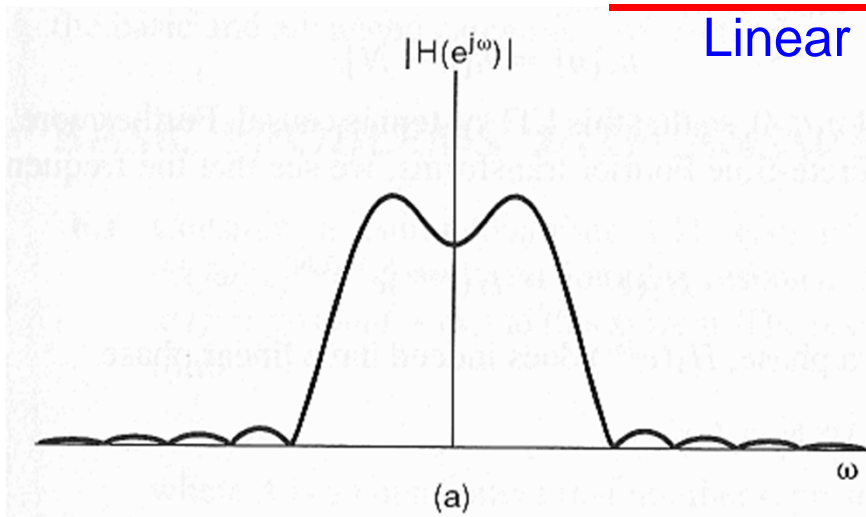


(b)

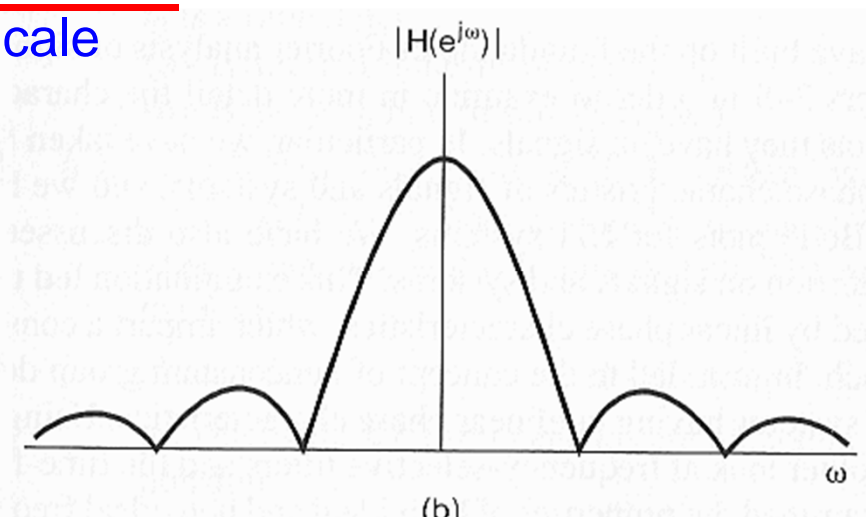
Log Scale



Linear Scale



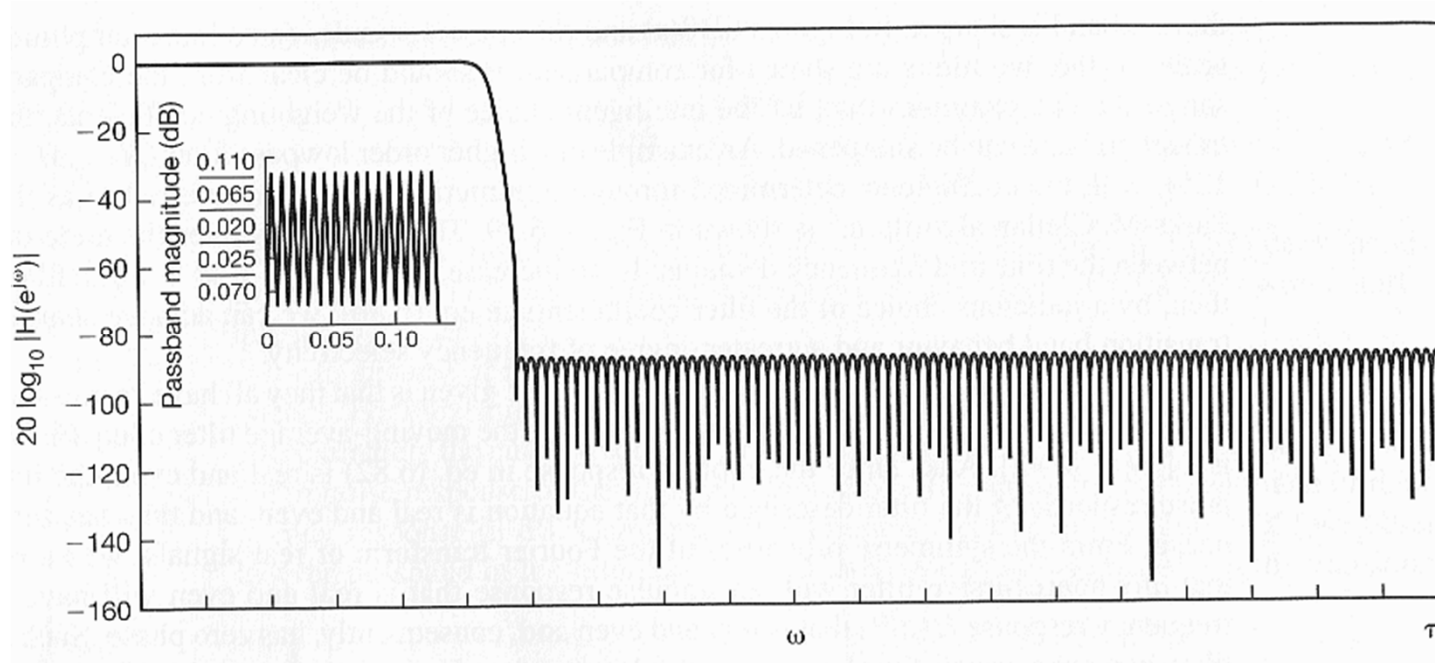
(a)



(b)

Lowpass Non-recursive Filter with 251 Coefficients:

$$y[n] = \sum_{k=-N}^M b_k x[n - k]$$



Coefficients determined by the Parks-McClellan algorithm

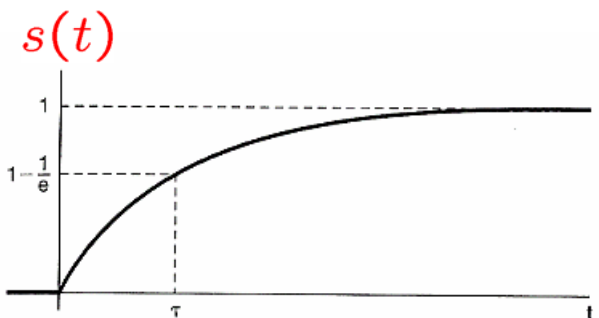
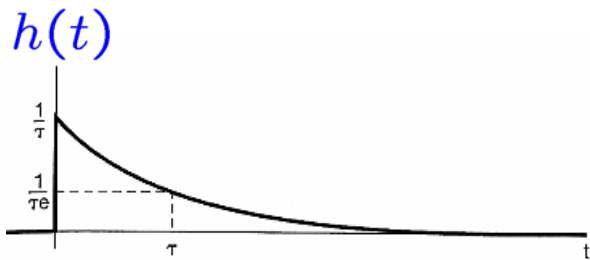
$$\frac{d}{dt}y(t) + ay(t) = ax(t)$$

$$\Rightarrow H(j\omega) = \frac{a}{j\omega + a}$$

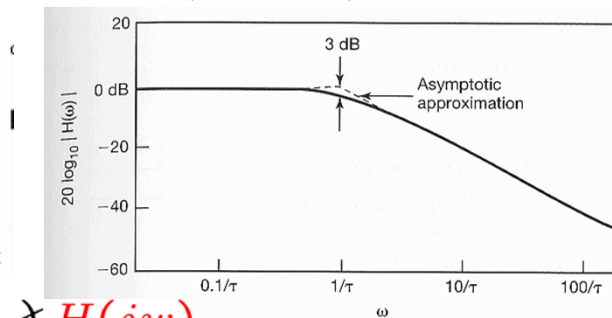
$$\Rightarrow H(s) = \frac{a}{s + a}$$

$$h(t) = a e^{-at} u(t)$$

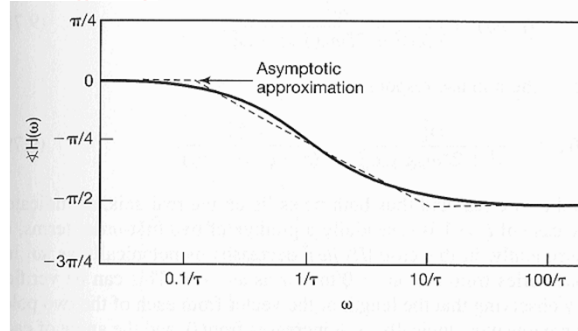
$$s(t) = [1 - e^{-at}] u(t)$$



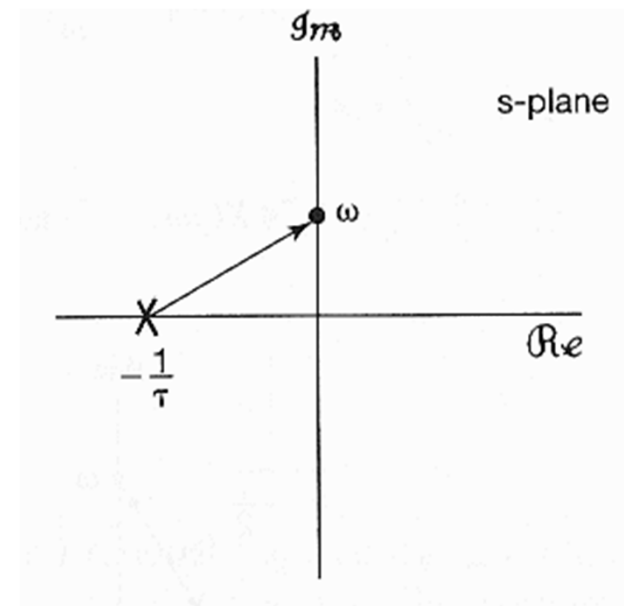
$20 \log_{10} |H(j\omega)|$



$\angle H(j\omega)$



$H(s)$



$$y[n] - a y[n - 1] = x[n] \quad |a| < 1$$

$$\Rightarrow H(e^{j\omega}) = \frac{1}{1 - a e^{-j\omega}}$$

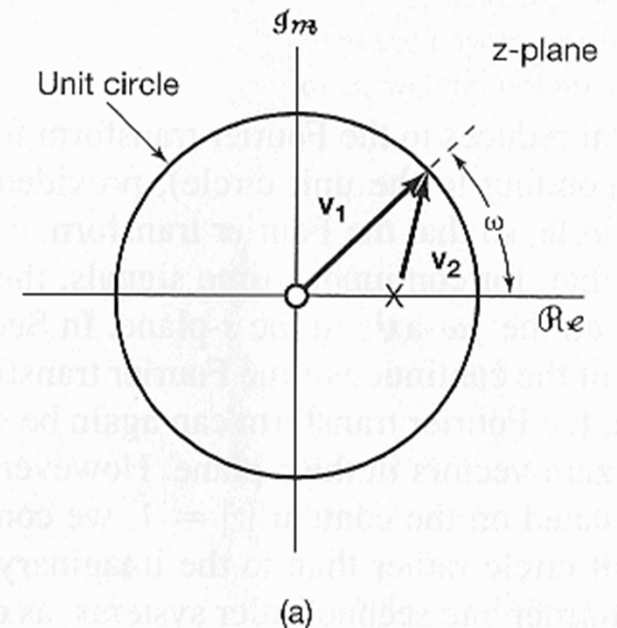
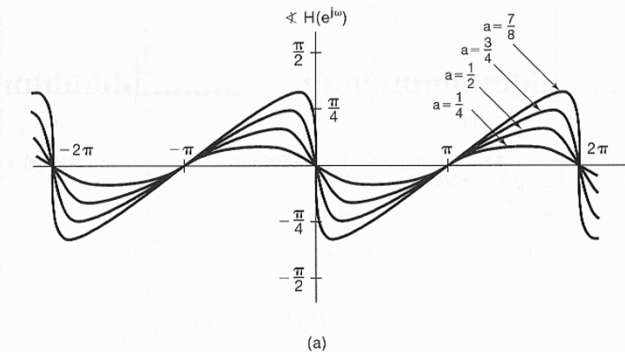
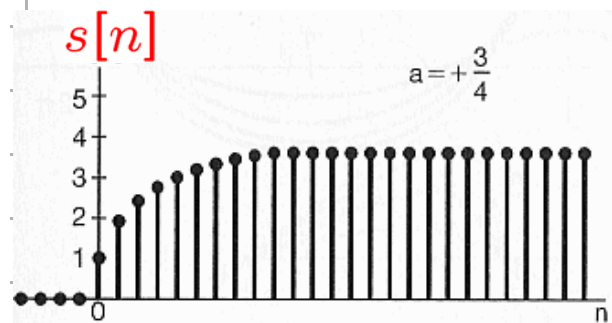
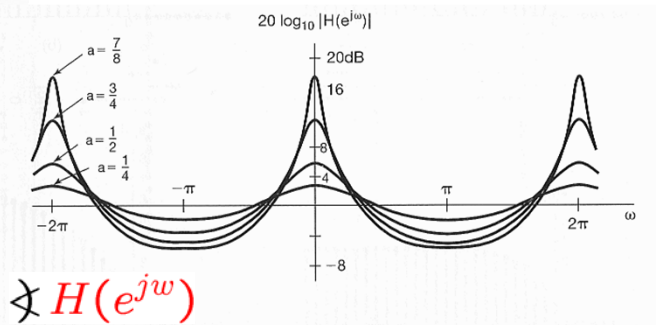
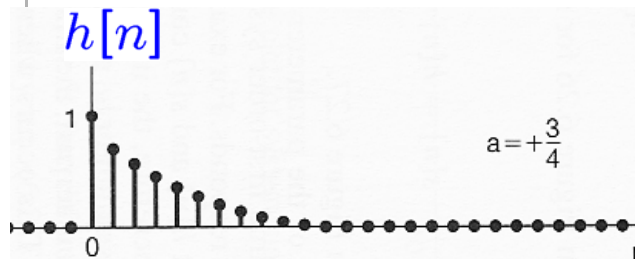
$$\Rightarrow H(z) = \frac{z}{z - a}, \quad |z| > |a|$$

$$\Rightarrow h[n] = a^n u[n]$$

$$\Rightarrow s[n] = \frac{1 - a^{n+1}}{1 - a} u[n]$$

$H(z)$

$20 \log_{10} |H(e^{j\omega})|$

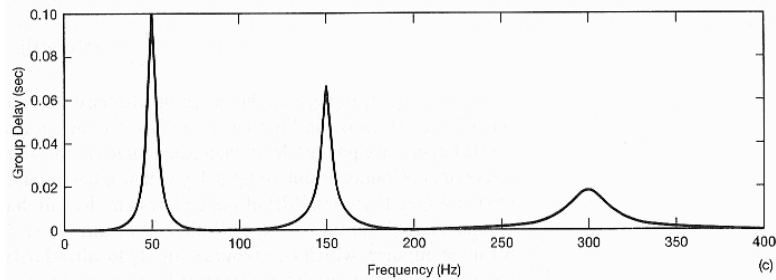
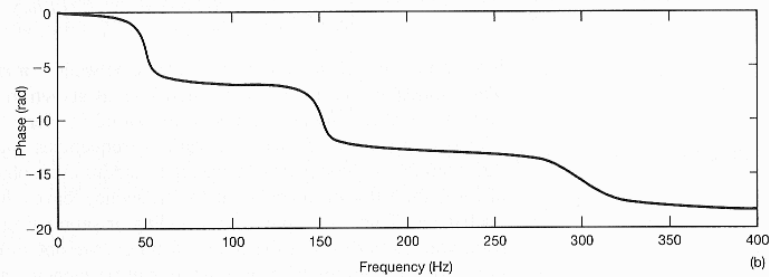
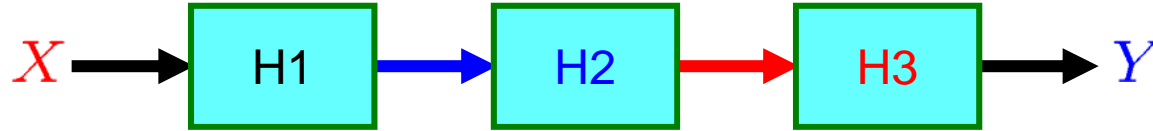


(a)

Summary: Chap 6 - 3

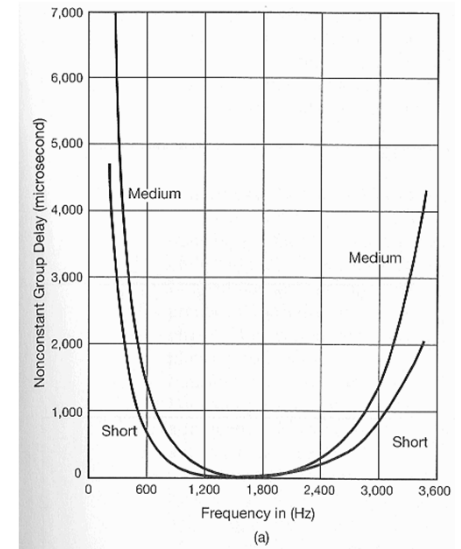
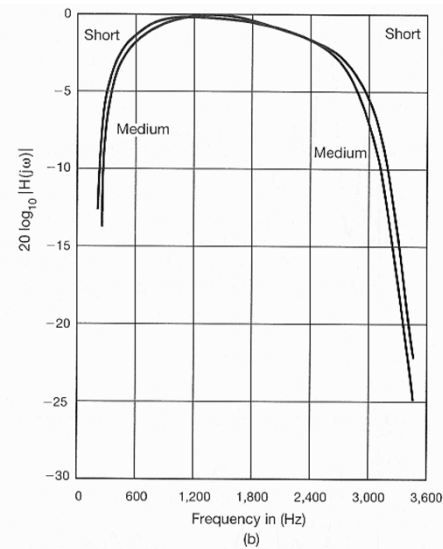
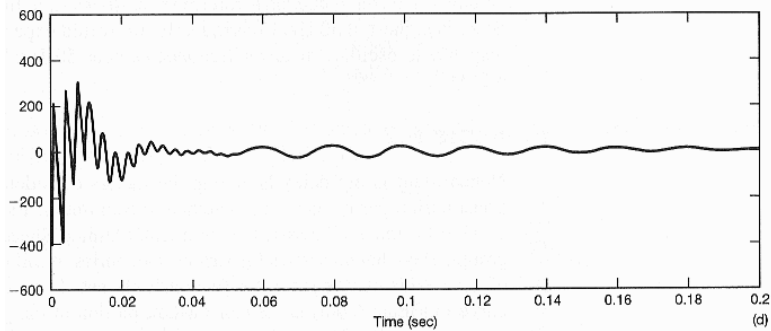
$$x(t) = \delta(t)$$

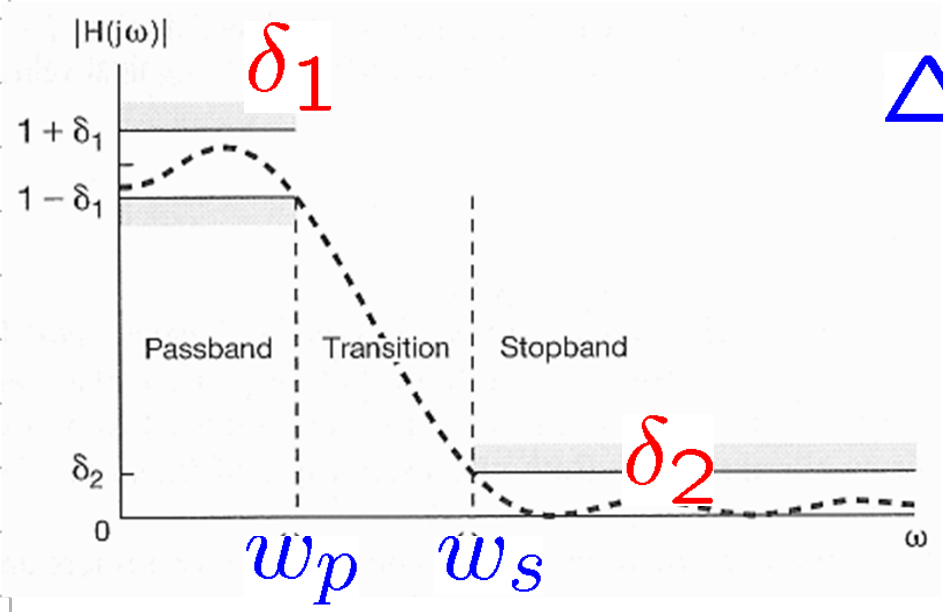
$$X(j\omega) = 1, \forall \omega$$



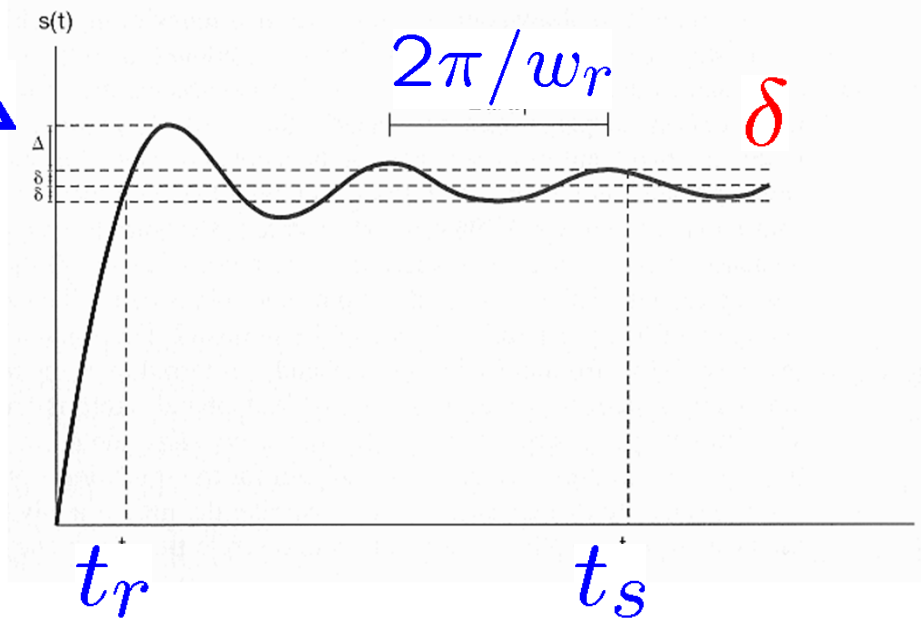
$$\tau(\omega) = - \frac{d}{d\omega} \{ \angle H(j\omega) \}$$

$$y(t)$$

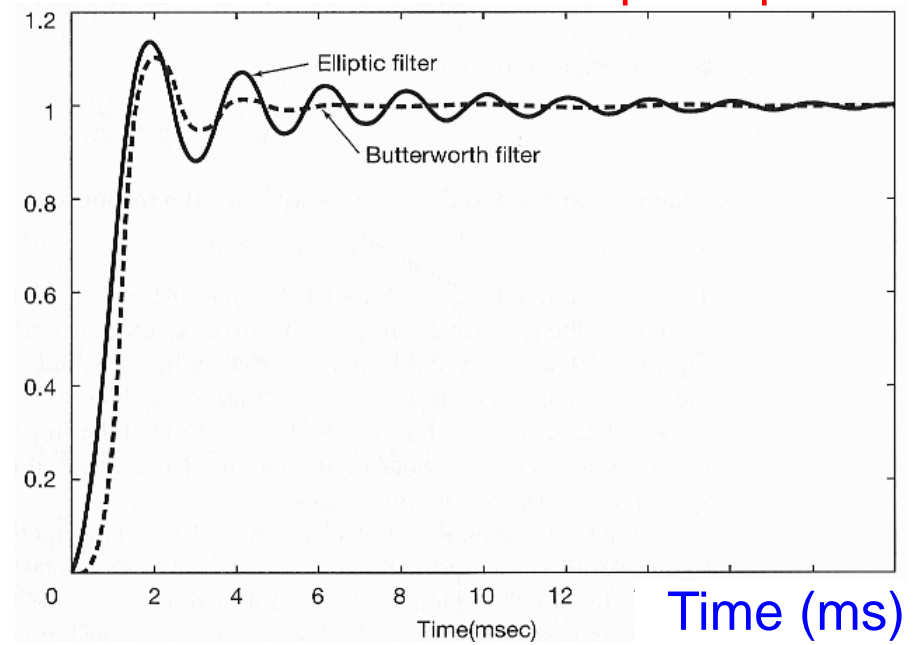
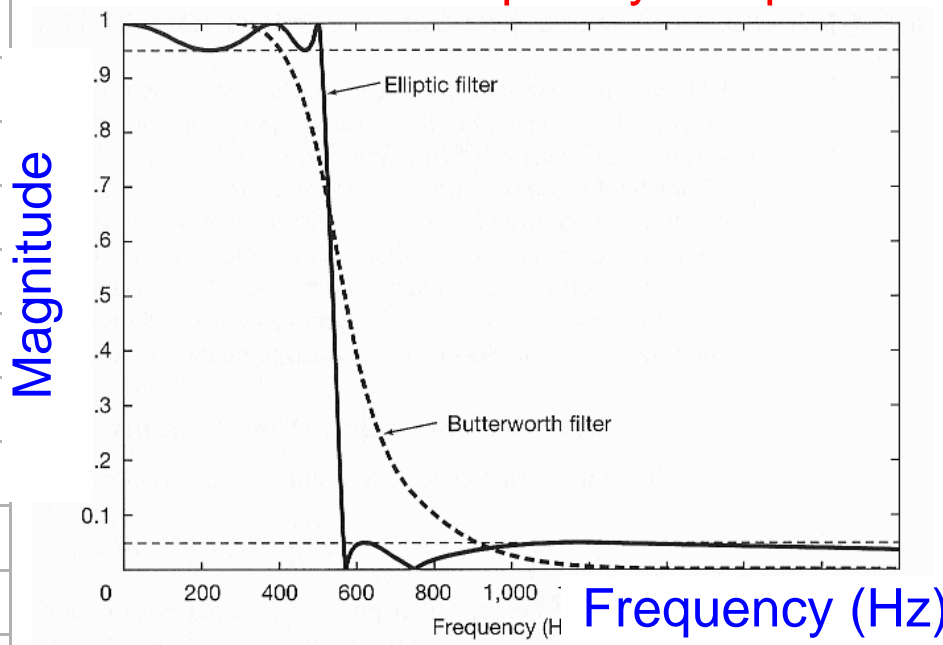




Frequency Response



Step Response



Time (ms)

Lowpass Filters:

$$\frac{1}{N + M + 1}$$

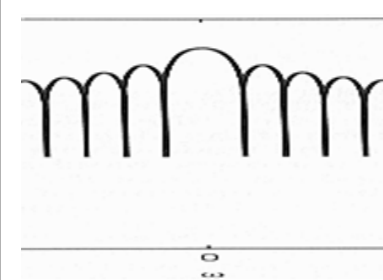
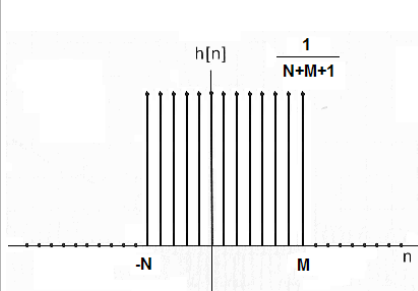


Fig 6.35

$$\frac{\sin(2\pi n/33)}{\pi n}$$

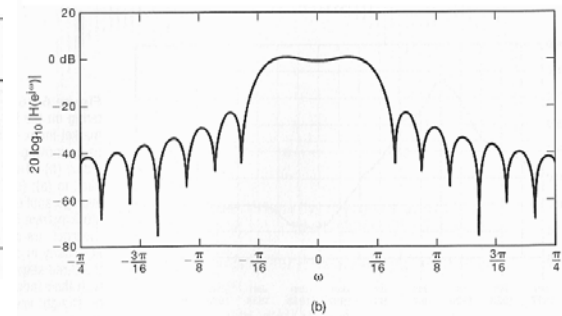
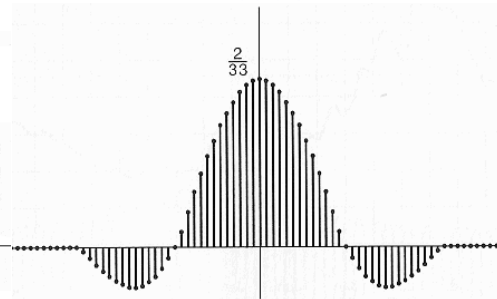
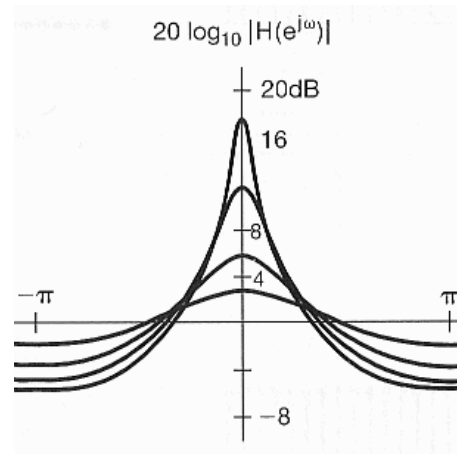
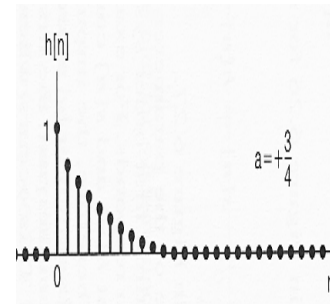


Fig 6.37

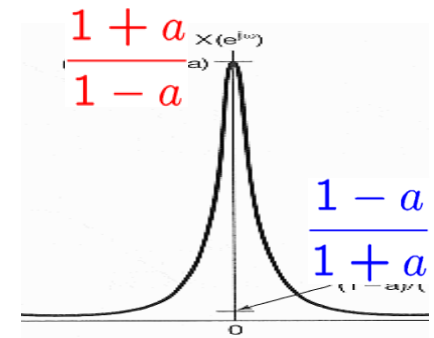
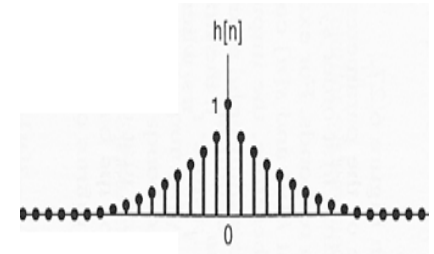
$$h[n] = a^n u[n]$$



$$H(e^{j\omega}) = \frac{1}{1 - ae^{-j\omega}}$$

Fig 6.28

$$x[n] = a^{|n|}$$



$$X(e^{j\omega}) = \frac{1 - a^2}{1 - 2a \cos \omega + a^2}$$

Ex 5.2

- The Magnitude-Phase Representation of the FT
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order CT Systems
- 1st-Order & 2nd-Order DT Systems
- Time- & Frequency-Domain Analysis of Systems