

Spring 2021

數位控制系統
Digital Control Systems

DCS-34
Discretized Controller –
Techniques for Enhancing Performance
(T/2-Delay Compensation)

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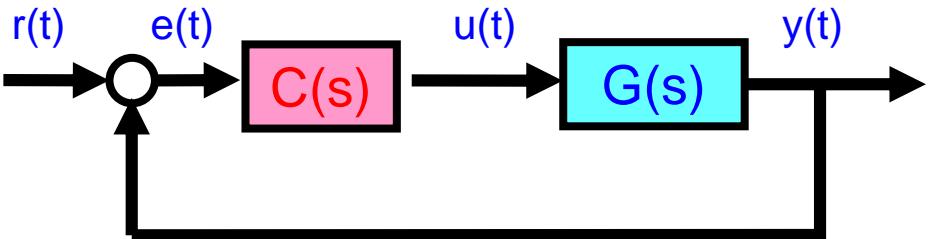
Feb – Jun, 2021

Figures and images used in these lecture notes are adopted from

1: B.D.O. Anderson, "Controller Design: Moving from Theory to Practice," IEEE Control Systems Magazine, 13(4), pp. 16-25, Aug. 1993

2: D. Raviv & E.W. Djaja, "Technique for Enhancing the Performance of Discretized Controllers," IEEE Control Systems Magazine, 19(3), pp. 52-57, June 1999

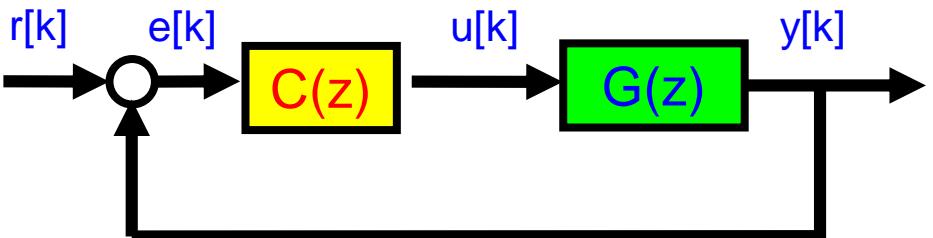
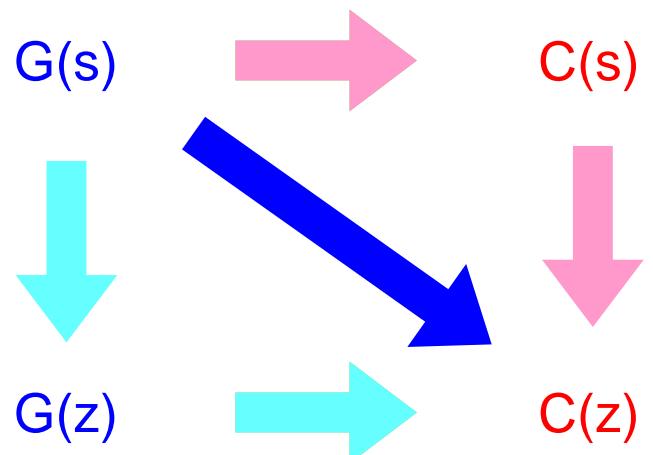
Introduction: CT and DT Plant-Controller



- Discrete Design
- Transform CT plant into DT plant
- By DT plant, design DT controller

▪ Direct Design

- Emulation
- By CT plant, design CT controller
- Transform CT controller into DT controller



- Basic principles of low-order controller design

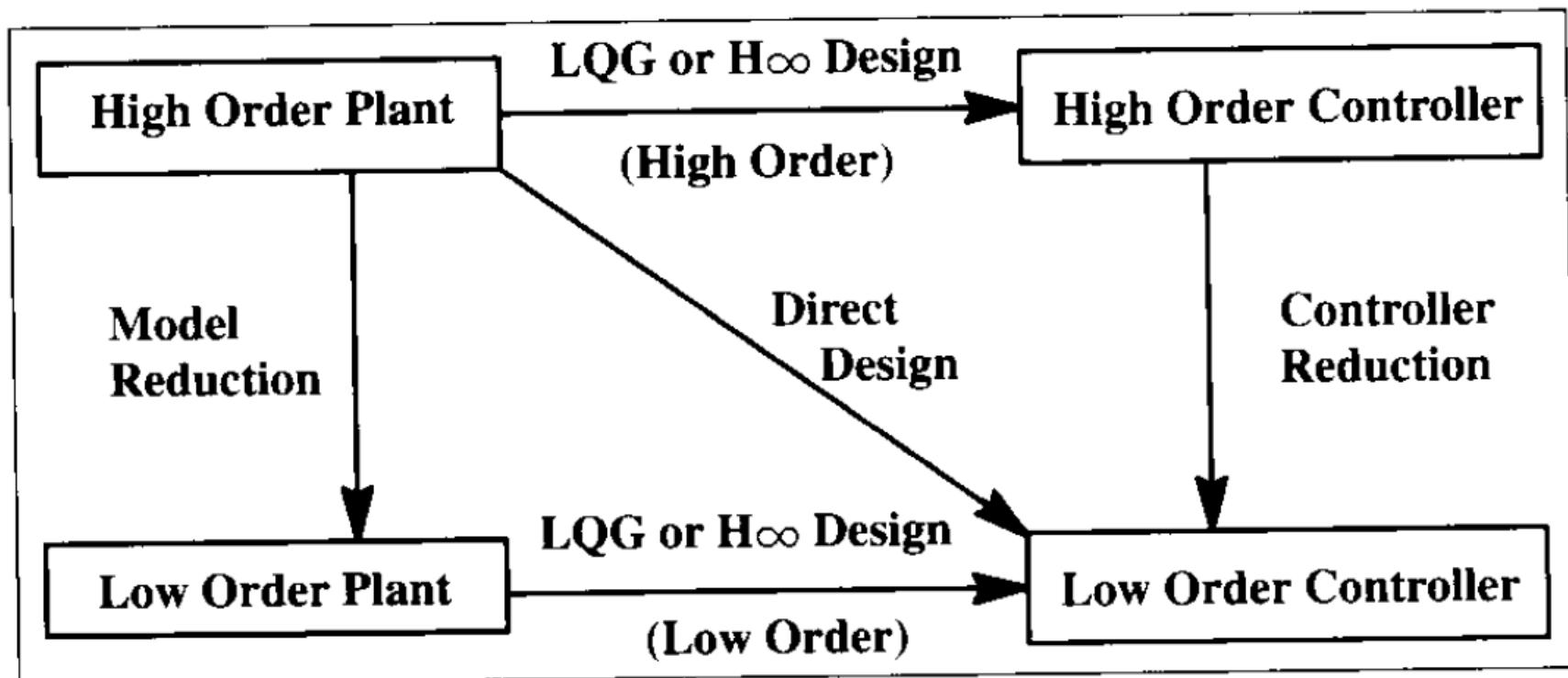


Fig. 1. Basic principles of low order controller design.

■ Study in Digital Control Systems

- Controller Design of Digital Control Systems

- **Design Process**

- > Discrete Design:

- » CT plant -> DT plant -> DT controller

- > Emulation:

- » CT plant -> CT controller -> DT controller

- > Direct Design: (B.D.O. Anderson, 1992 Bode Prize Lecture)

- » CT plant -> DT controller

- Discrete Design
 - By Transfer Function
 - By State Space
- Design by Emulation
 - Tustin's Method or bilinear approximation
 - Matched Pole-Zero method (MPZ)
 - Modified Matched Pole-Zero method (MMPZ)
 - Digital PID-Controllers
- Techniques for Enhancing the Performance

■ Textbook schemes for replacing a CT controller by a DT one

With $C(s)$ continuous time and $C_d(z)$ discrete time,

$$C_d(z) = C \left(\frac{z-1}{T} \right)$$

Euler or forward difference

$$C_d(z) = C \left(\frac{z-1}{zT} \right)$$

Balanced difference

$$C_d(z) = C \left(\frac{2z-1}{Tz+1} \right)$$

Tustin or bilinear

$$C_d(z) = C \left(\frac{\omega_1 z - 1}{\tan\left(\frac{\omega_1 T}{2}\right) Z + 1} \right)$$

Tustin with prewarping

$$C_d(z) = \frac{(z-1)}{Tz} \frac{1}{2\pi j} \int_{\gamma-j_\infty}^{\gamma+j_\infty} \frac{e^{sT}}{z-e^{sT}} \frac{G(s)}{s} ds$$

Step-invariance

$$C_d(z) = \frac{(z-1)^2}{Tz} \frac{1}{2\pi j} \int_{\gamma-j_\infty}^{\gamma+j_\infty} \frac{e^{sT}}{z-e^{sT}} \frac{G(s)}{s^2} ds$$

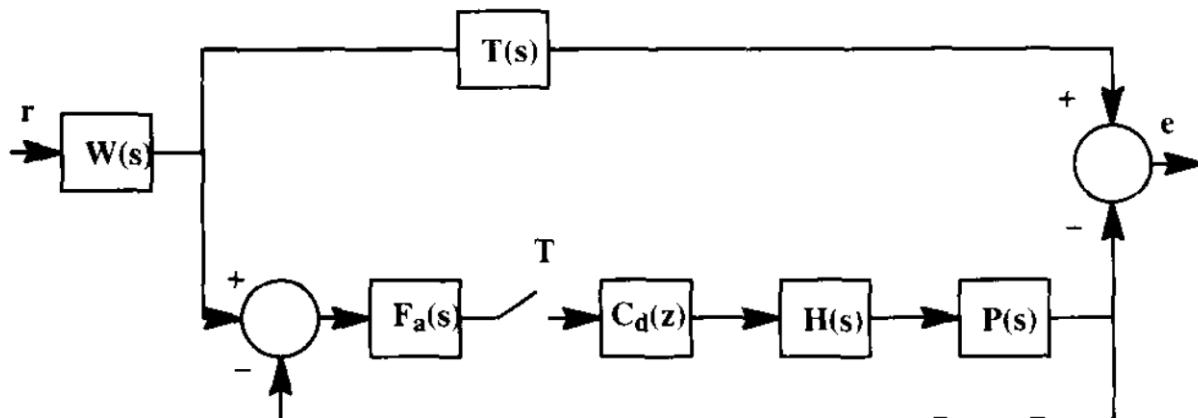
Ramp-invariance

Poles and zeros of $C_d(z)$ are images under $z = e^{sT}$ of those of $C(s)$, with $C_d(1) = C(0)$.

Zero-order hold equivalence.
First-order hold equivalence.
Triangular-hold equivalence.

■ Measuring the difference between using Continuous and Discrete controllers

- Data
Shaping or Weighting Filter $W(s)$, rational, stable and strictly proper
- Assumption
 $C_d(z)$ (unknown) is stabilizing



- Operator from $r \in L_2(0, \infty)$ to $e \in L_2(0, \infty)$ is
 - bounded
 - dependent on $C_d(z)$
 - not describable via a transfer function
 - periodically time-varying

Fig. 7. Measuring the difference between using continuous and discrete controllers.

- Digital control design through discretizing an analog controller

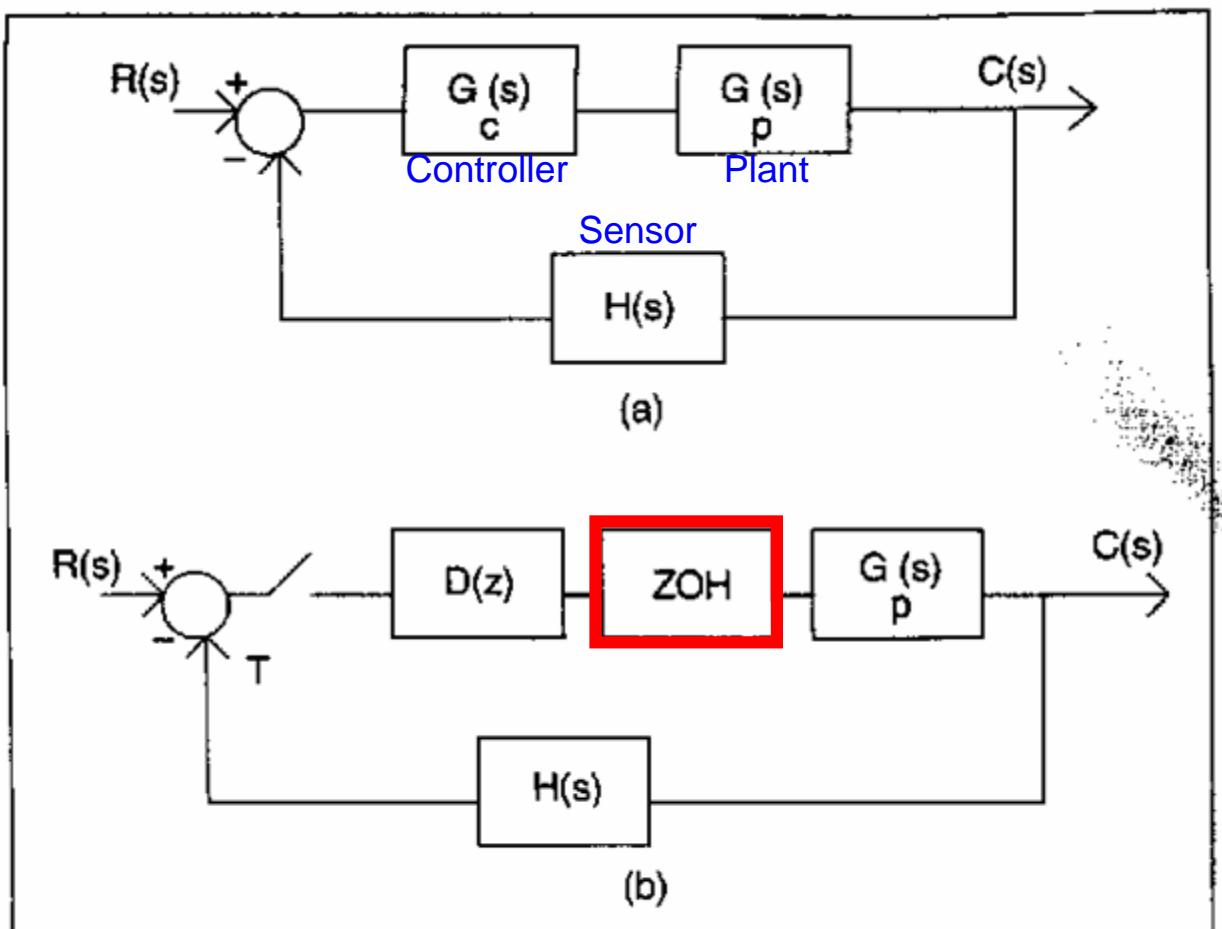


Fig. 1. (a) The analog closed-loop control system, (b) The digital closed-loop control system.

■ Given

- A process $G_p(s)$
- A sensor $H(s)$
- A presumably well designed **analog controller** $G_c(s)$

■ Find

- A digital controller $D(z)$
which produces **closed-loop behavior**
similar to the **analog system**
both in the **time** and **frequency** domains

■ Solutions:

- Analog control design followed by controller discretization
 - More convenient
 - Deal with sampling time T at the final phase
- Direct digital control design
- To enhance the performance by the first method
 - Add a pole-zero pair in the z-plane
 - To compensate for the low-frequencies and mid-frequencies phase and gain response effects contributed by ZOH

■ Potential problem:

- The ZOH causes a **delay** of approximately $T/2$

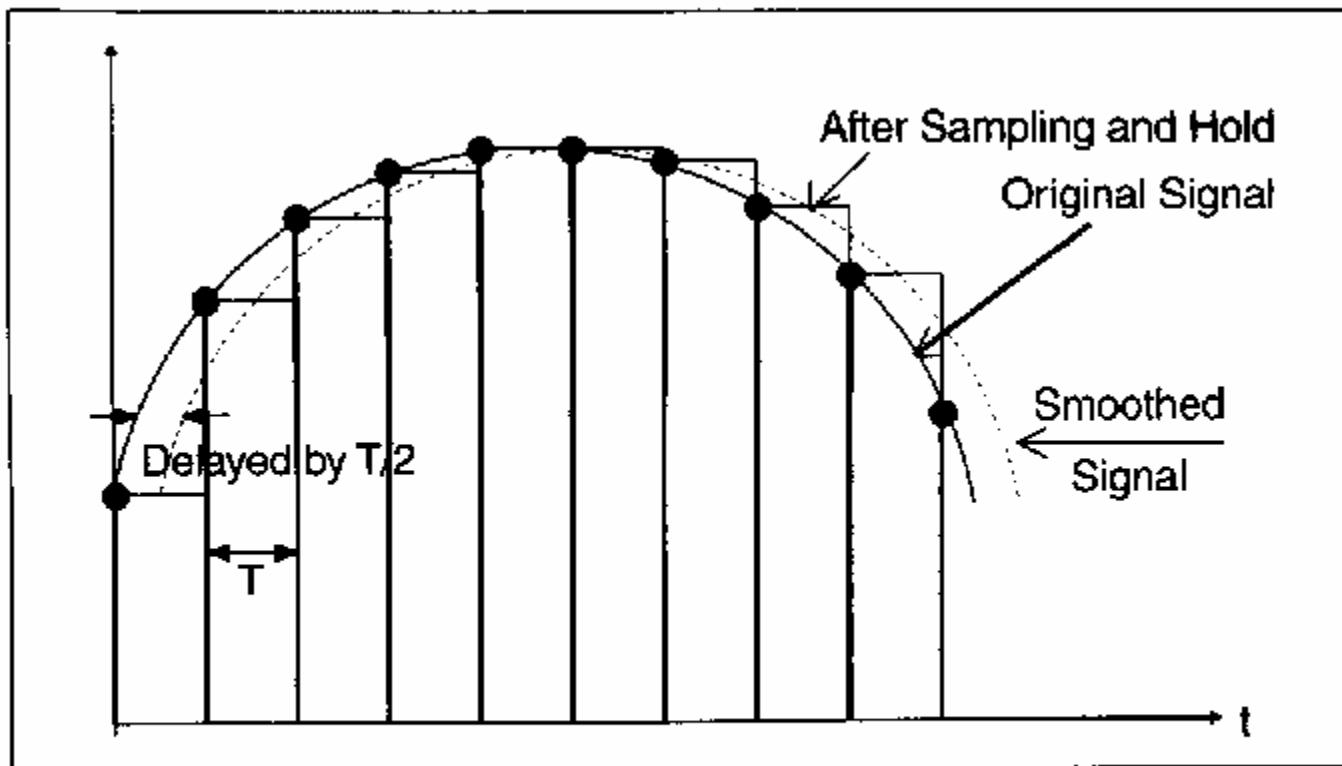


Fig. 2. A reconstructed signal using ZOH and its smoothed approximation.

■ A pole-zero compensation for delay:

$$C(z) = \frac{2z}{z + 1}$$

- Provides a phase of $(\omega T/2)$
- Which exactly cancels the frequency phase response of the ZOH obtained from

$$\frac{1 - e^{-sT}}{s}$$

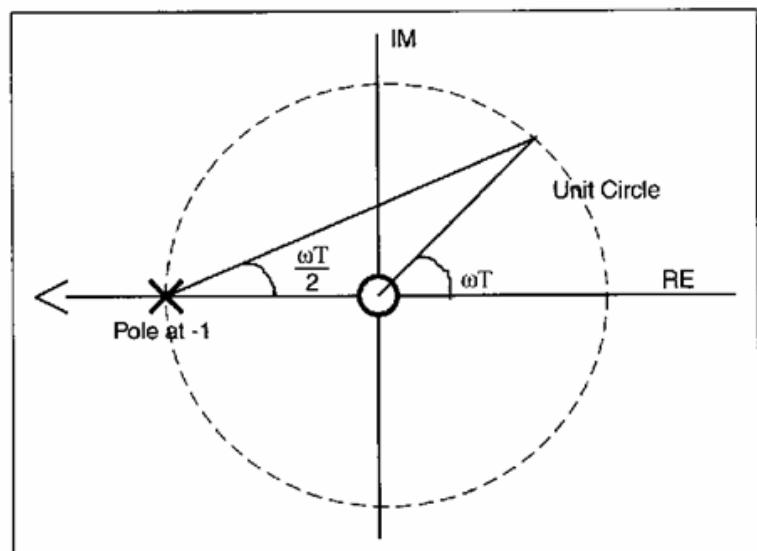


Fig. 3. The location of pole and zero of ZOH compensator in the Z-domain.

■ A pole-zero compensation for delay:

- The ZOH transfer function:

$$\frac{1 - e^{-sT}}{s} \approx \frac{T}{1 + \frac{sT}{2}} \quad \text{1st-order Pade approximation}$$

$$\Rightarrow \left. \frac{T}{1 + \frac{sT}{2}} \right|_{s=\frac{2}{T} \frac{z-1}{z+1}} = \frac{T}{2} \frac{z+1}{z} \quad \text{Tustin transformation}$$

- The characteristic polynomial

$$1 + \left(\frac{2z}{z+1} \right) D'(z) (1 - z^{-1}) \mathcal{Z} \left\{ \frac{G_p(s)}{s} \right\} = 0$$

$D'(z)$: any discretized $D(s)$

■ A pole-zero compensation for delay:

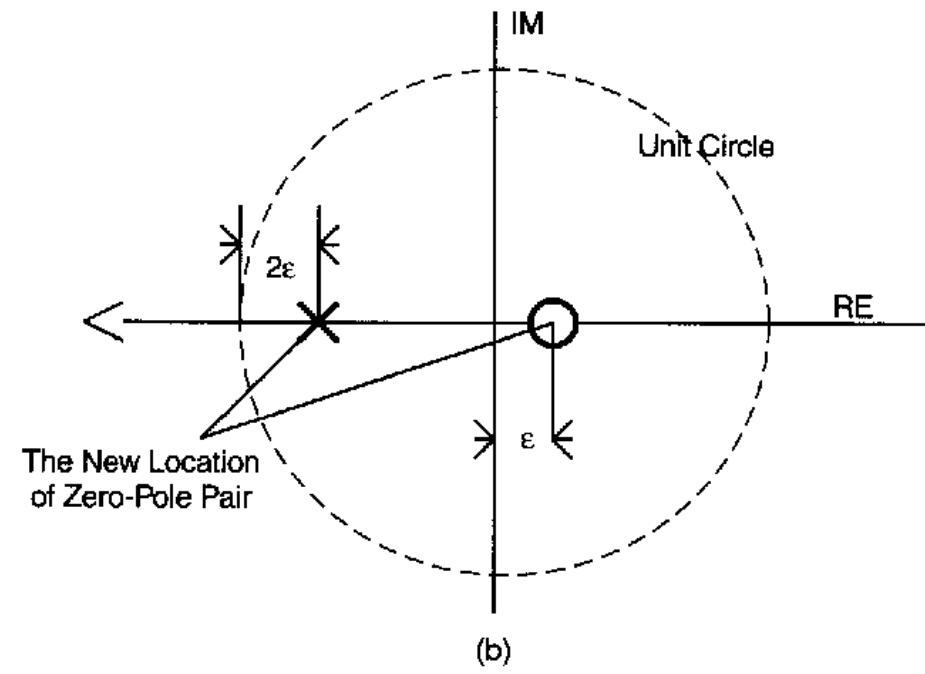
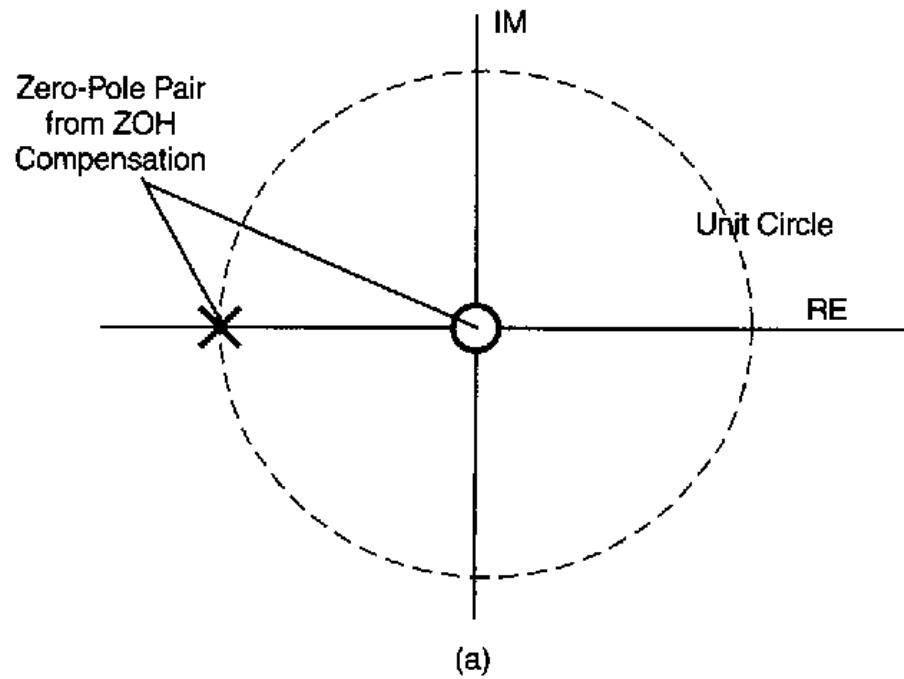
- IF the proposed compensation causes instability
a modified ZOH compensation

$$C'(z) = \frac{2(z-\varepsilon)}{z + 1 - 2\varepsilon}$$

- The characteristic polynomial

$$1 + \left(\frac{2(z-\varepsilon)}{z + 1 - 2\varepsilon} \right) D'(z) (1 - z^{-1}) \mathcal{Z} \left\{ \frac{G_p(s)}{s} \right\} = 0$$

- A pole-zero compensation for delay:



■ Lag Compensator:

$$G_p(s) = \frac{4 \times 10^6}{s(s + 20)(s + 200)}$$

$$H(s) = 1$$

- Design specifications:
 1. Velocity error constant K_v at least 1000 s^{-1}
 2. Attenuation of all sinusoidal inputs of frequency above 400 rad/sec by at least 16
 3. Steady-state error of (up to) 1% for sinusoidal inputs for frequencies less than 1 rad/sec

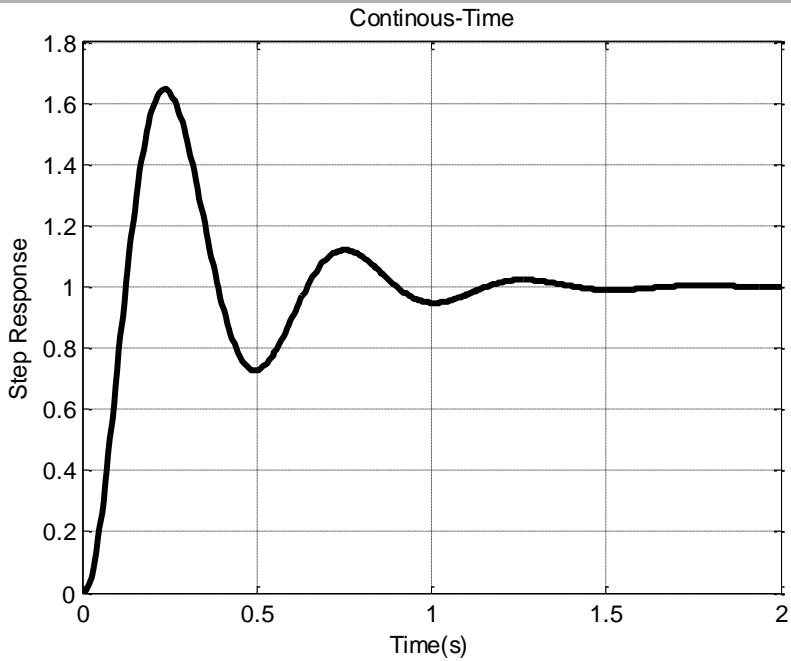
$$\Rightarrow G_c(s) = \frac{1}{80} \frac{(s+8)}{(s+0.1)}$$

- D'(z): by Tustin

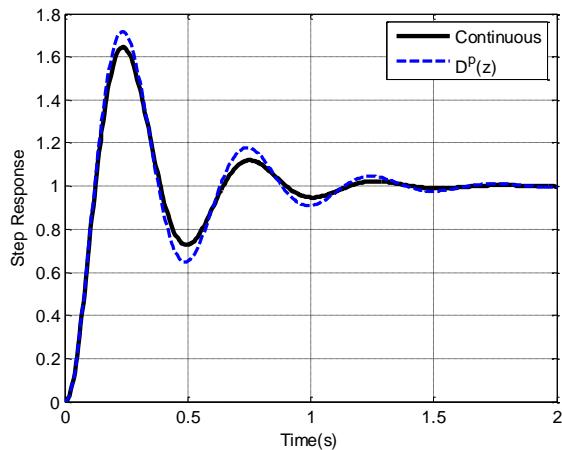
Table 1

	D'(z)	Multiplier	D(z)
T = 0.01 s	$\frac{0.0130z - 0.0120}{z - 0.9990}$	$\frac{2z}{z+1}$	$\frac{0.0260z^2 - 0.0240z}{z^2 + 0.0010z - 0.9990}$
T = 0.05 s	$\frac{0.0150z - 0.0100}{z - 0.9950}$	$\frac{2z}{z+1}$	$\frac{0.0299z^2 - 0.0200z}{z^2 + 0.0050z - 0.9950}$
T = 0.1 s	Unstable $\frac{0.0174z - 0.0075}{z - 0.9900}$	$\frac{2z}{z+1}$	Unstable $\frac{0.0348z^2 - 0.0150z}{z^2 + 0.0100z - 0.9900}$
T = 0.1 s	Unstable $\frac{0.0174z - 0.0075}{z - 0.9900}$	$\frac{2(z-0.2)}{(z+0.6)}$	$\frac{0.0348z^2 - 0.0219z + 0.0030}{z^2 - 0.3900z - 0.5940}$

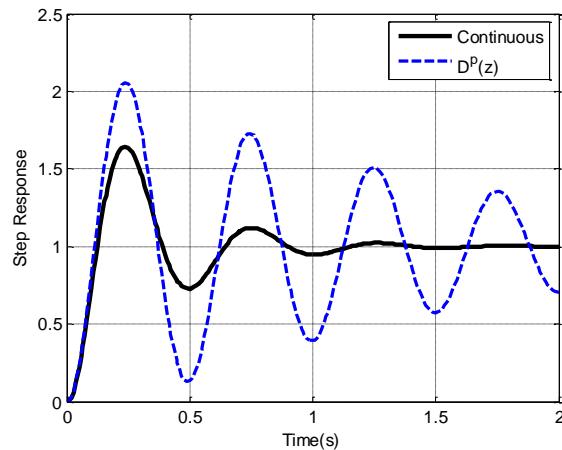
Examples – Lag



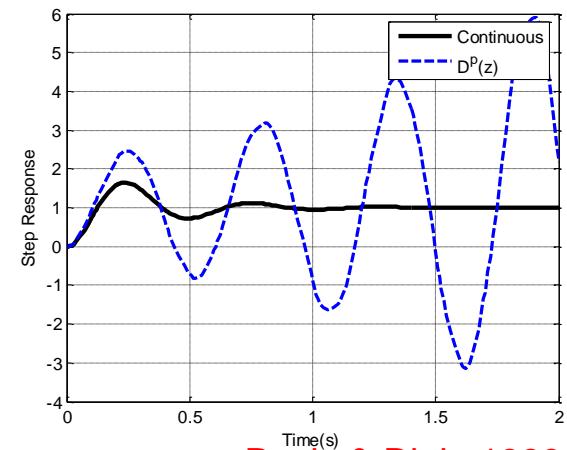
$T = 0.01s$



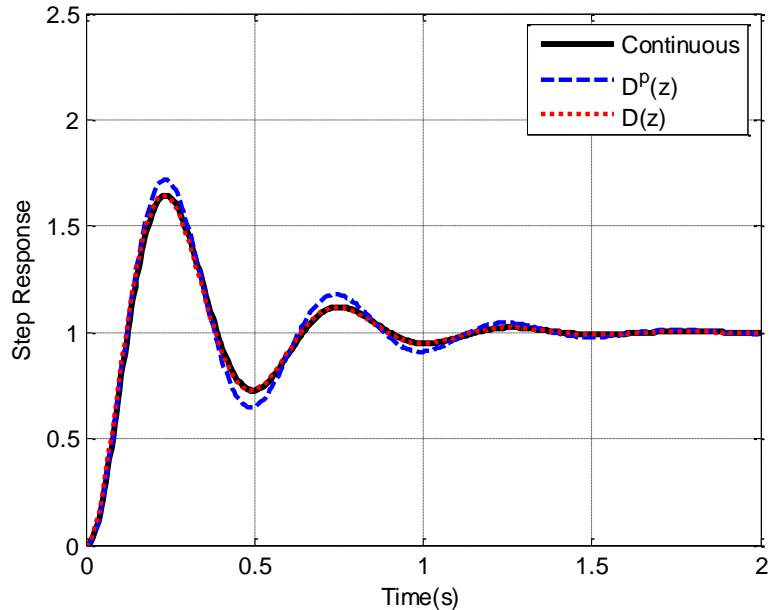
$T = 0.05s$



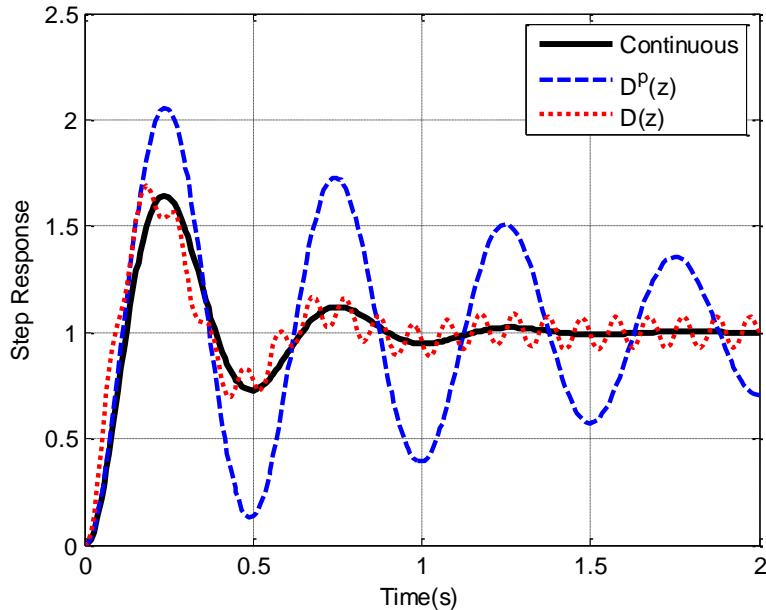
$T = 0.1s$



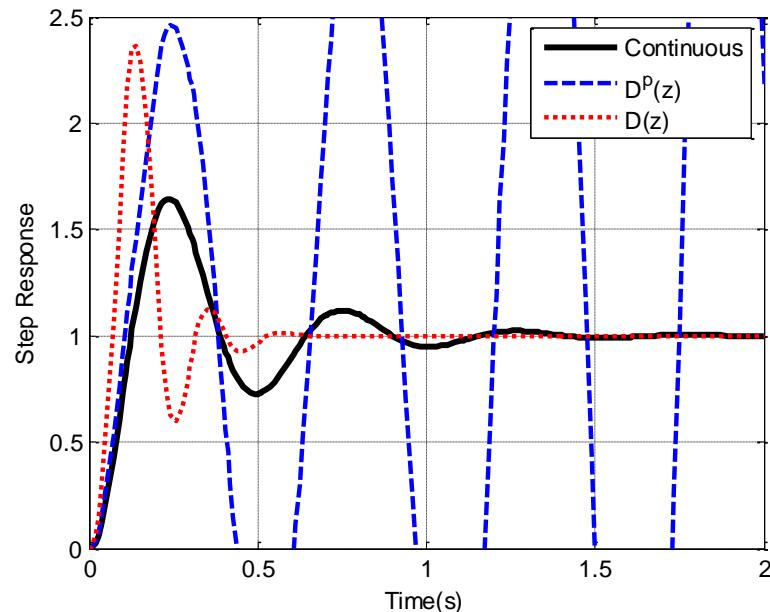
Examples – Lag



$T = 0.01s$



$T = 0.05s$



$T = 0.1s$

■ Lead-Lag Compensator:

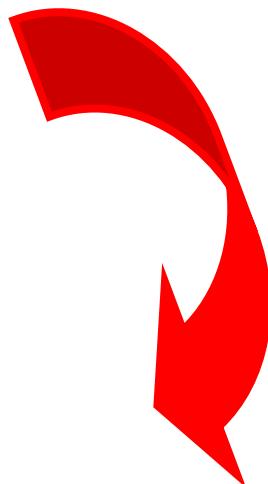
$$G_p(s) = \frac{1000}{s(1 + \frac{s}{10})(1 + \frac{s}{250})}$$

$$H(s) = 1$$

- Design specifications:
 1. Phase margin of at least 50°
 2. Velocity error constant K_v at least 1000 s^{-1}
 3. Attenuation of the input noise at 60 Hz and above by a factor of 100
 4. Steady-state error for frequencies less than 1 rad/sec less than 1%

$$\Rightarrow G_c(s) = \frac{(1 + \frac{s}{4.5})(1 + \frac{s}{10})}{(1 + \frac{s}{0.1})(1 + \frac{s}{110})}$$

$$T = 0.01s$$



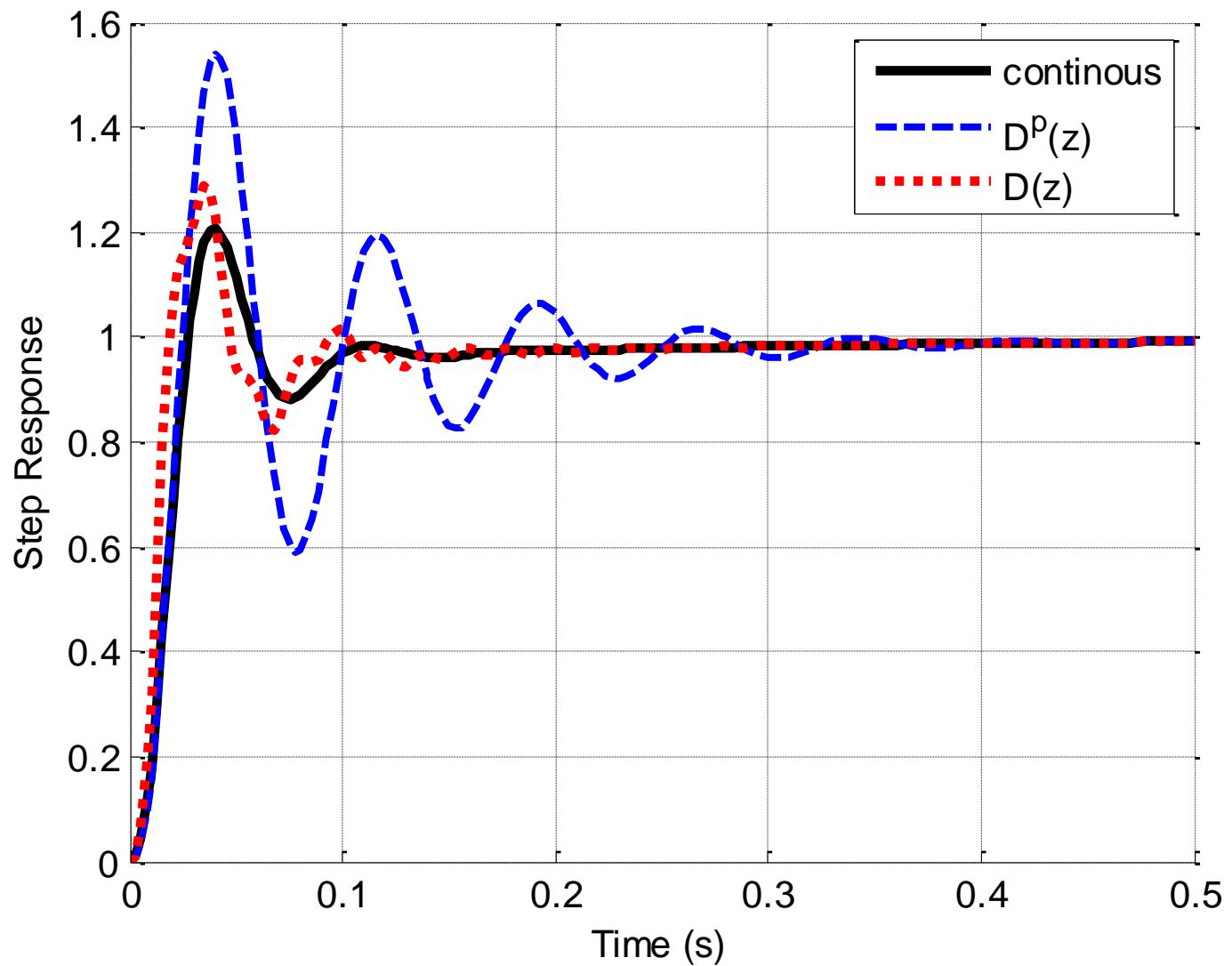
$$\Rightarrow D'(z) = \frac{0.6597z^2 - 1.2897z + 0.6300}{1.00z^2 - 1.2893z + 0.2900}$$

?

With the ZOH compensation of $\frac{2z}{z+1}$

$$\Rightarrow D(z) = \frac{1.3194z^3 - 2.5793z^2 + 1.26z}{z^3 - 0.2893z^2 - 0.9993z + 0.2900}$$

Examples – Lead-Lag



Examples – Lead-Lag

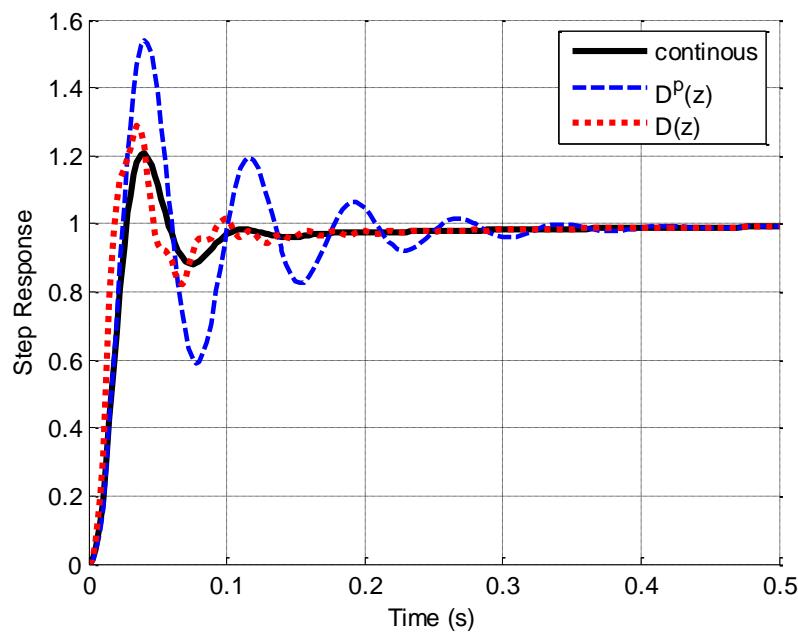
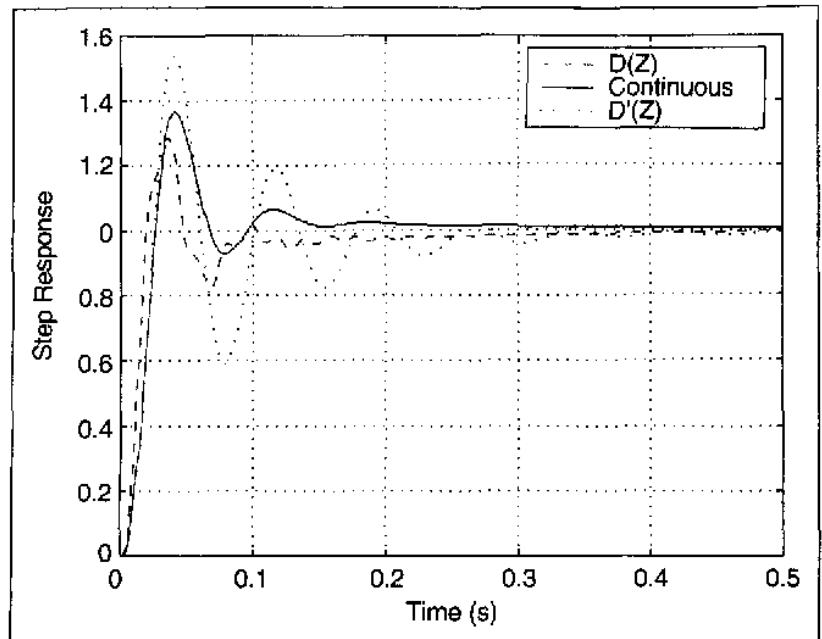
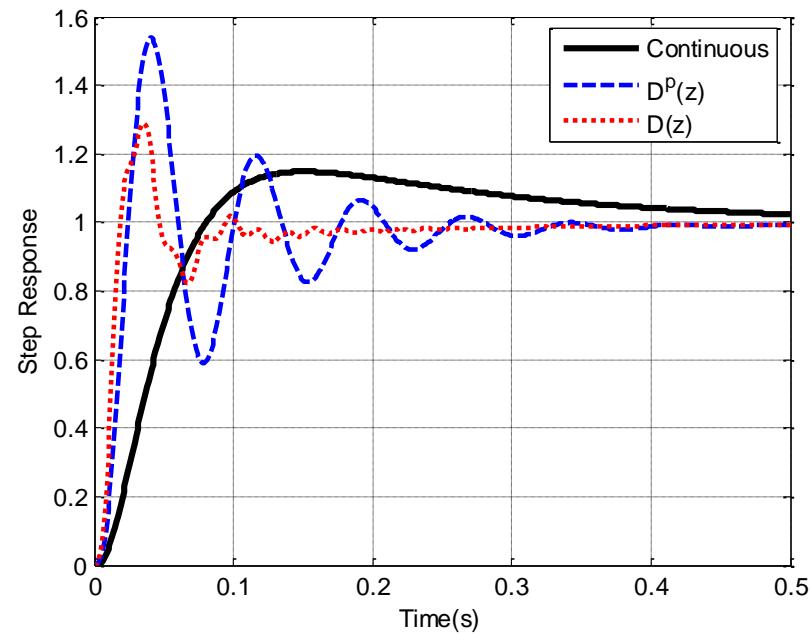


Fig. 6. Closed-loop step response of Example (b). $T = 0.01$ s.



■ Katz's Example:

$$G_p(s) = \frac{863.3}{s^2}$$

- Design specifications:
 1. Max phase lag at $f = 3$ Hz should not be more than 13°
 2. At any given frequency the CL gain should not exceed 5 dB beyond the CL dc gain
 3. Max tracking error due to an input disturbance moment of 0.028Nm should not be 0.01 rad

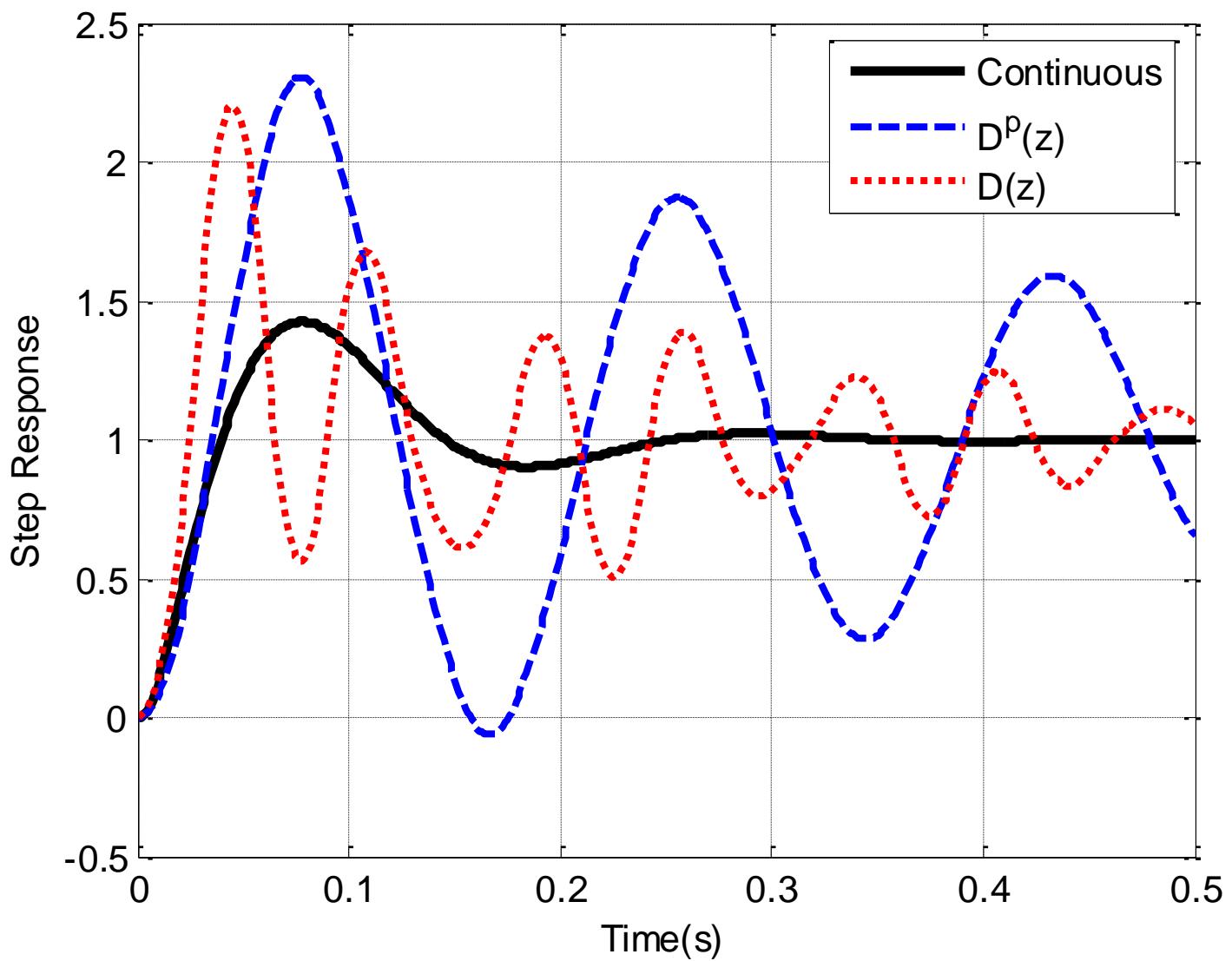
$$G_c(s) = 2940 \frac{(s + 29.4)}{(s + 294)^2}$$

$$T = 0.03s$$

$$\Rightarrow D'(z) = \frac{1.8958z^2 + 1.1685z - 0.7273}{z^2 + 1.1653z + 0.3395}$$

With the ZOH compensation of $\frac{2z}{z + 1}$

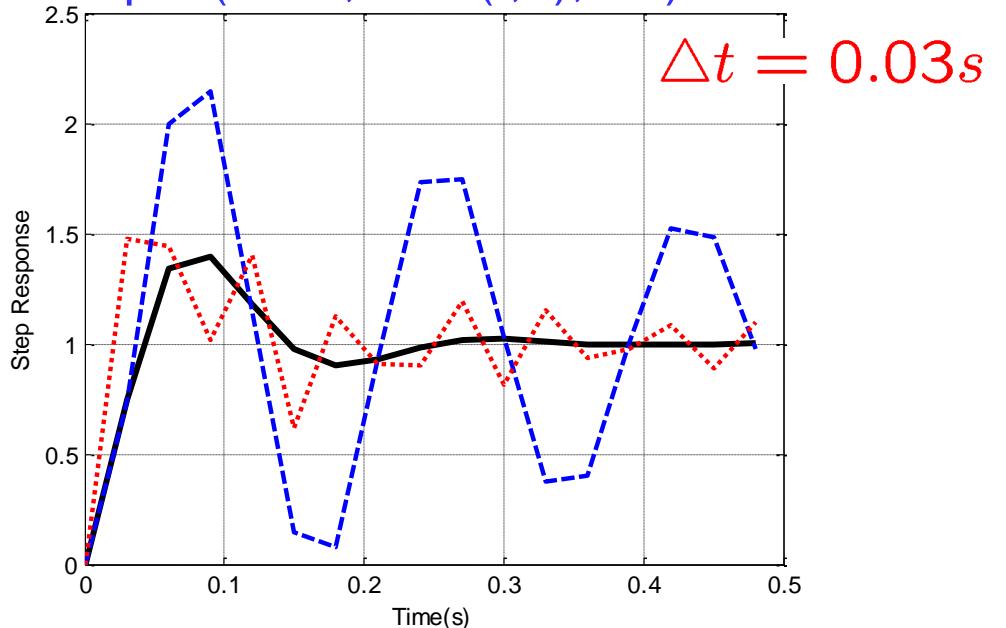
$$\Rightarrow D(z) = \frac{3.7916z^3 + 2.3369z^2 - 1.4546z}{z^3 + 2.1653z^2 + 1.5047z + 0.3395}$$



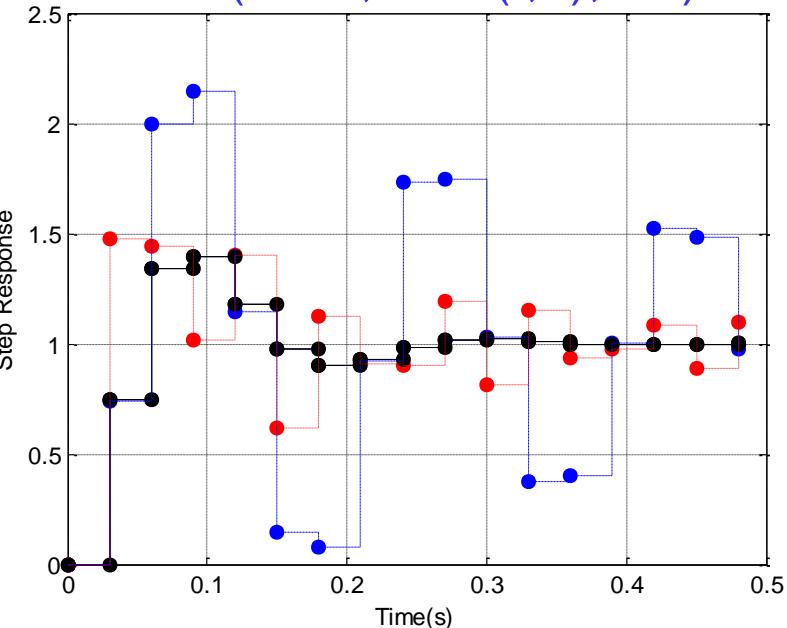
Examples – Katz

$T = 0.03s$

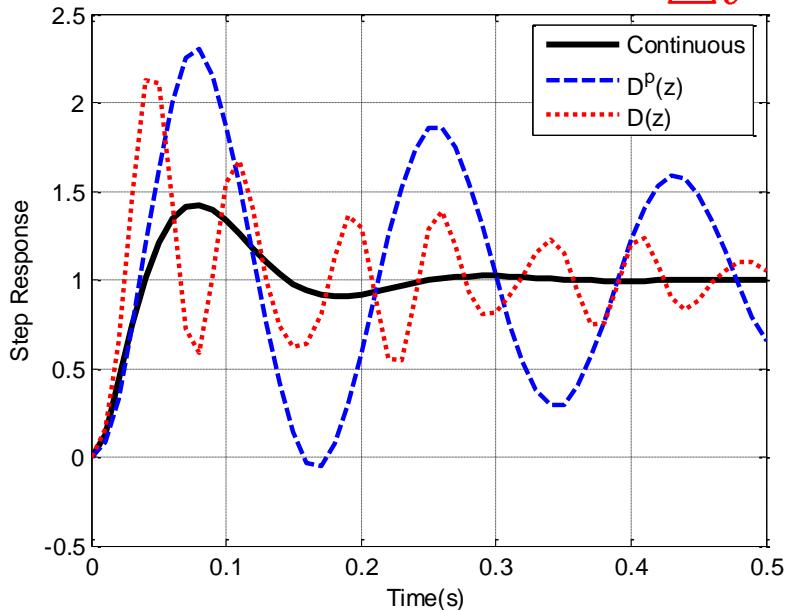
`>> plot(time, data(:,1), 'k-')`



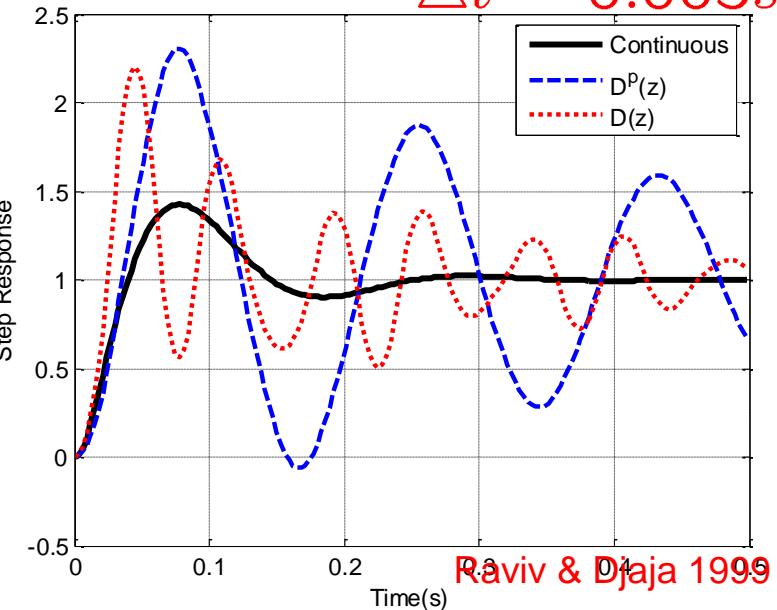
`>> stairs(time, data(:,1), 'k-')`

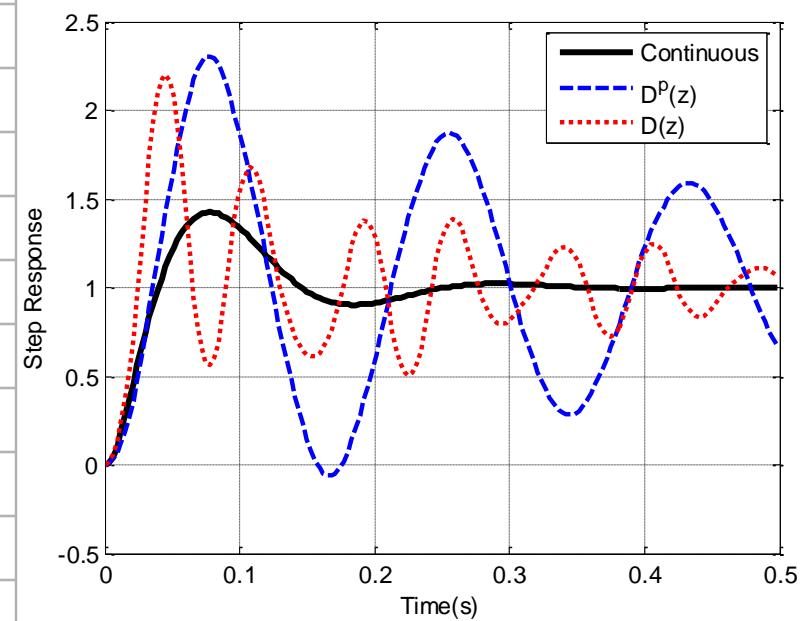


$\Delta t = 0.01s$

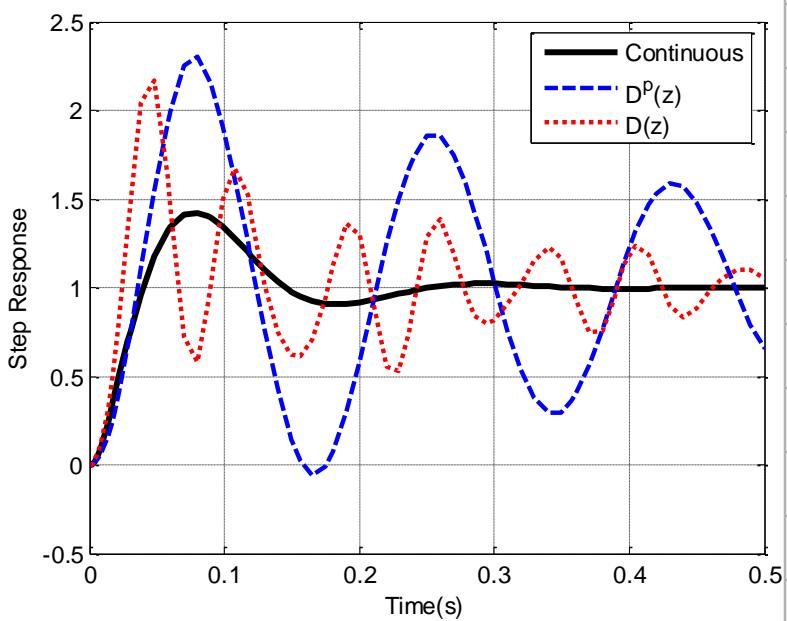


$\Delta t = 0.003s$



$\Delta t = 0.003s$ 

Sample time = -1 (inherited)



■ Rattan's Example:

$$G_p(s) = \frac{10}{s(s+1)}$$

$$\Rightarrow G_c(s) = \frac{1 + 0.416s}{1 + 0.319s}$$

$$T = 0.15s$$

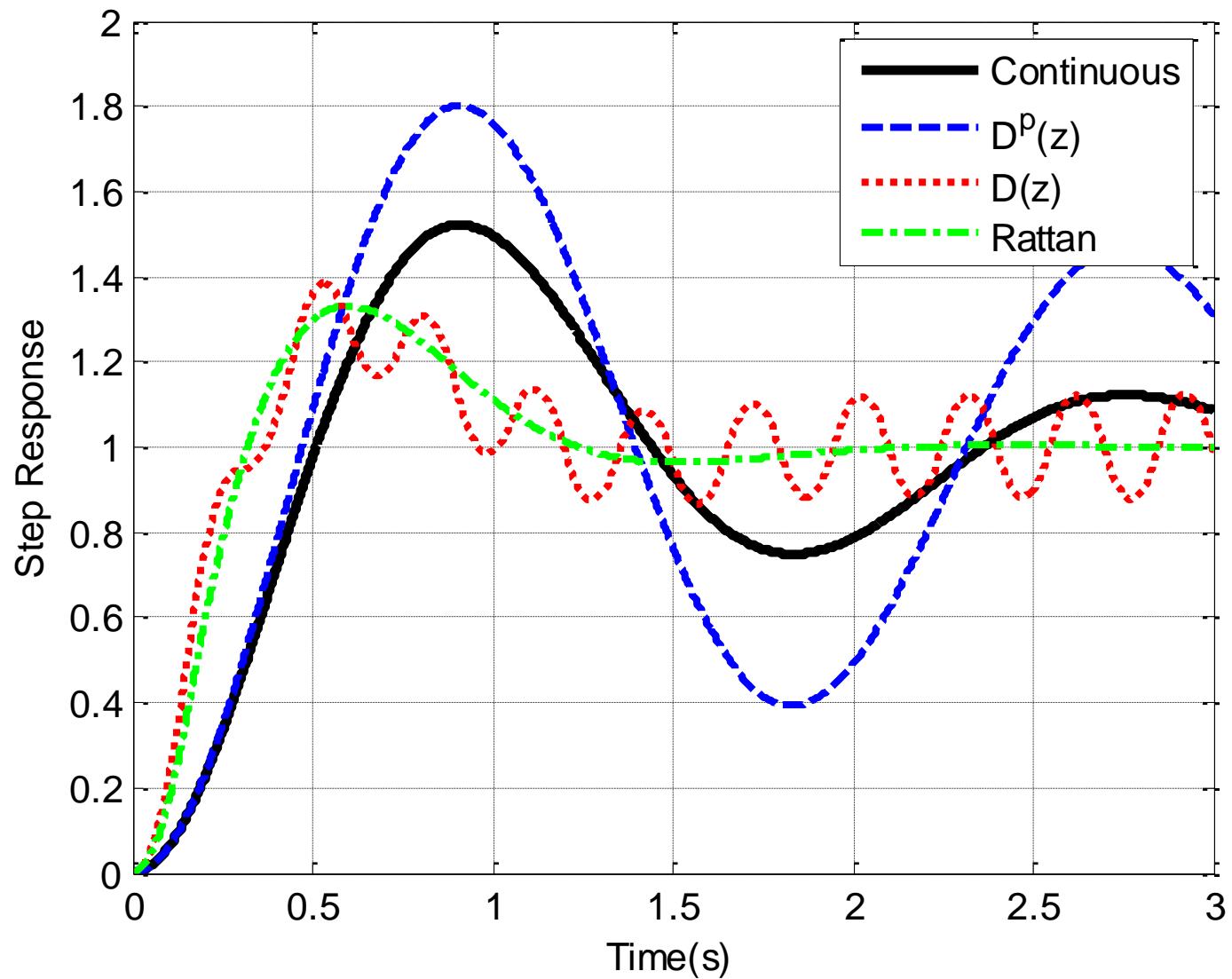
$$\Rightarrow D_{\text{Rattan}}(z) = \frac{3.436z - 2.191}{z + 0.2390}$$

$$\Rightarrow D'(z) = \frac{2.294z - 1.5935}{z - 0.2991}$$

Tustin transformation

$$\Rightarrow D(z) = \frac{4.5888z^2 - 3.6459z + 0.3187}{z^2 + 0.5009z - 0.2393}$$

Examples – Rattan



Examples – Rattan

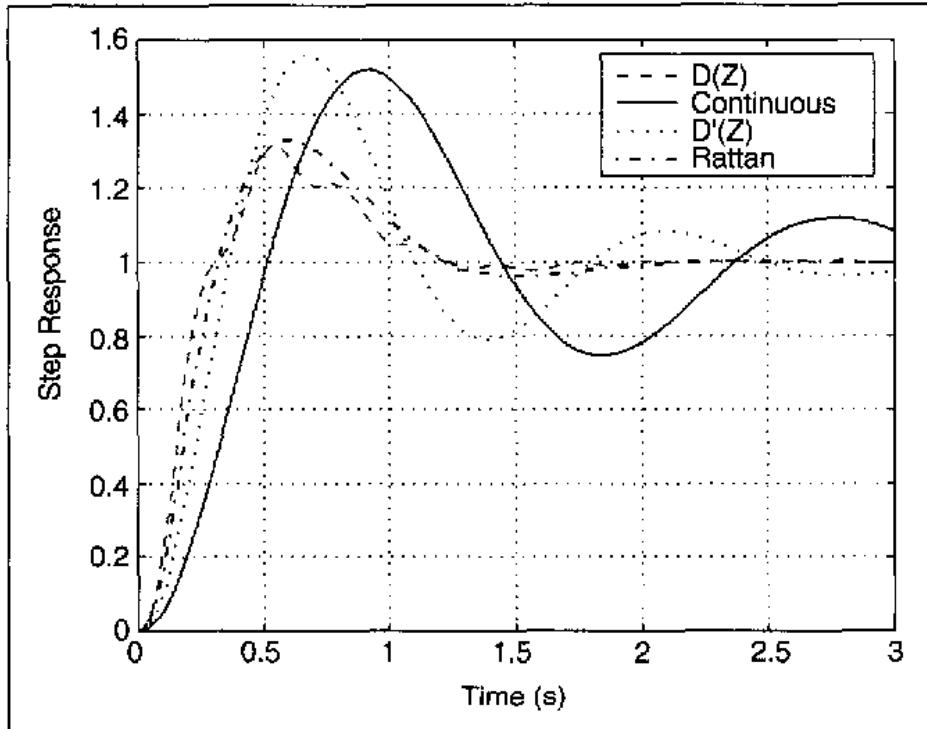
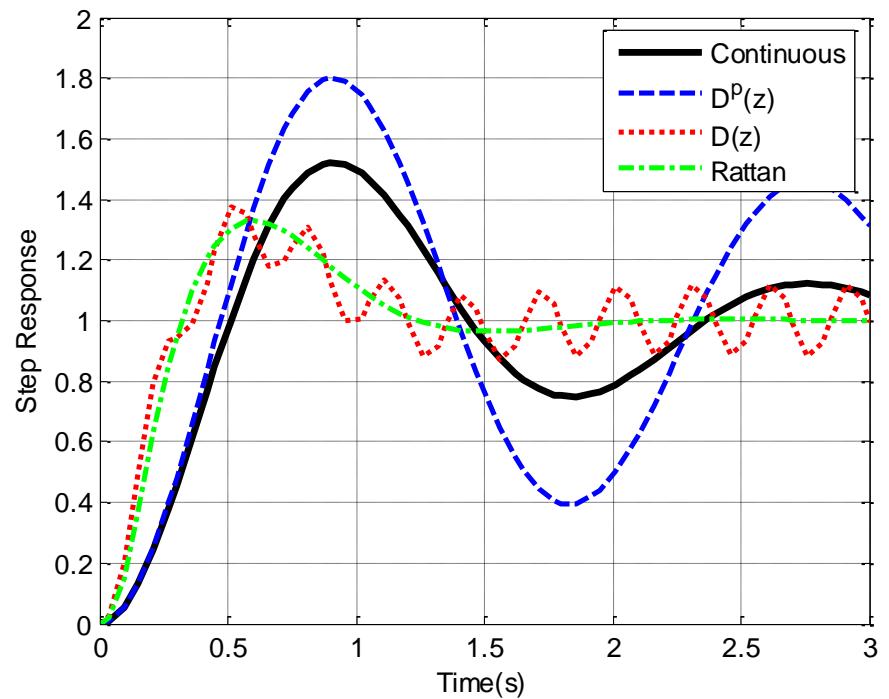


Fig. 8. Closed-loop step response of Example (d). $T = 0.15$ s.