

Spring 2019

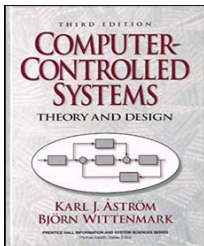
數位控制系統  
Digital Control Systems

DCS-31  
State Space Design

Feng-Li Lian

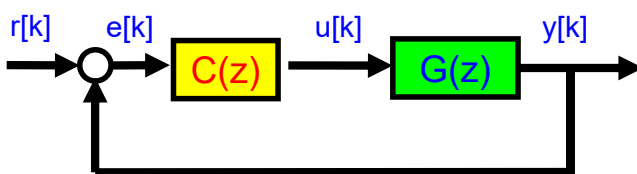
NTU-EE

Feb19 – Jun19



Introduction: Model and Analysis and Design

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DCS31-SSDesign-2



Plant (DT):

- Input-Output Model:

$$\frac{Y_d(z)}{U_d(z)} = G_d(z) = \frac{B_d(z)}{A_d(z)}$$

- State-Space Model:

$$\begin{aligned} \mathbf{x}[k+1] &= \mathbf{F}\mathbf{x}[k] + \mathbf{H}u[k] \\ y[k] &= \mathbf{C}\mathbf{x}[k] + \mathbf{D}u[k] \end{aligned}$$

- design  $u[k] \Rightarrow$

unstable  $\rightarrow$  stable

stable  $\rightarrow$  more stable

from  $y[k]$  to estimate  $\mathbf{x}[k]$

System Properties:

- Stability
- Controllability and Reachability
- Observability and Detectability

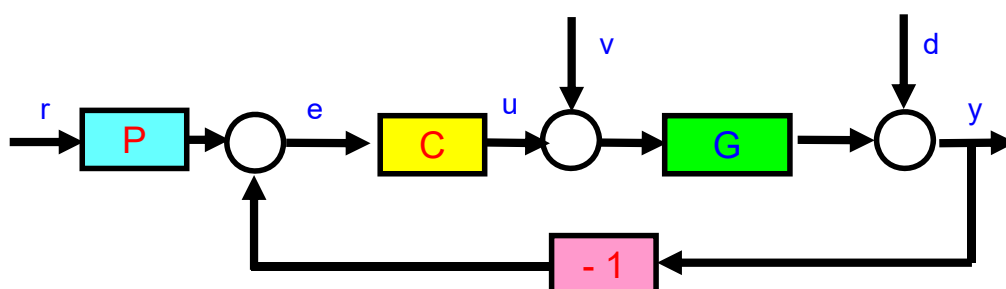
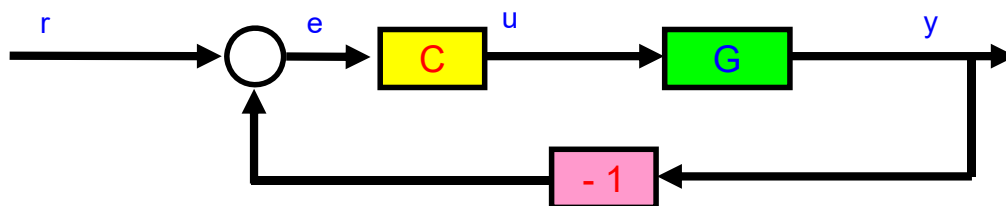
- Control System Design
- Regulation by State Feedback
- Observer Design
- Output Feedback
- Tracking Problem

- Control System Design:
  - Load disturbance (**actuator**)
  - Measurement noise (**sensor**)
  - Process disturbance (**un-modeled** dynamics)
- Control Objects:
  - **Regulation**:
    - ✓ Reduction of load disturbances
    - ✓ Fluctuations by measure noise
  - **Tracking**:

### Major Ingredients of a Design Problem:

- Purpose of the system
- Process model
- Model for disturbance
- Model variants and uncertainties
- Admissible control strategies
- Design parameters

### Block Diagram of a Typical Control System:



▪ The Process:

$$\frac{d}{dt}\mathbf{x} = \mathbf{A}\mathbf{x} + \mathbf{B}u$$

▪ Discrete-time model with  $h$ :

$$\mathbf{x}(k + 1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\text{where } \mathbf{F} = e^{\mathbf{A}h} \text{ and } \mathbf{H} = \int_0^h e^{\mathbf{A}s} ds \mathbf{B}$$

▪ Disturbances:

- **Impulse** signals: irregularly, widely spread, etc.
- **Step** signals:
- **Ramp** signals:
- **Sinusoidal** signals:

▪ Process Uncertainties:

- In the elements of **A, B, C, D** or **F, H, C, D**

## ■ Design Criteria:

### ➤ Regulation:

- ✓ Bring the state to zero after perturbations
- ✓ The rate of decay of state → C.L. poles

### ➤ Tracking:

- ✓ From commands to states → “model”

## ■ Admissible Controls:

### ➤ When all states are measured w/o errors:

- ✓ Linear feedback control law

$$u(k) = -\mathbf{K} \mathbf{x}(k) = - \begin{bmatrix} k_1 & k_2 & \cdots & k_n \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}$$

## ■ Design Parameters :

- ✓ Sampling period
- ✓ Desired C.L. poles
  
- ✓ Time histories of states and controls
- ✓ Magnitude of control signals
- ✓ Speed at which the system recovers from a disturbance

- The C.T. Model:

$$\frac{d}{dt}\mathbf{x} = \mathbf{A}\mathbf{x} + \mathbf{B}u$$

- The D.T. Model: (given  $h$ )

$$\mathbf{x}(k + 1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

- Characteristic Equation:

$$\mathbf{F} \Rightarrow z^n + a_1 z^{n-1} + \dots + a_n = 0$$

- System Model and Characteristic Equation:

$$\mathbf{x}(k + 1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\mathbf{A}(z) = z^n + a_1 z^{n-1} + \dots + a_n = 0$$

- If the system is “Controllable”  
the system is in the **Controllable Canonical Form:**

$$\mathbf{x}(k + 1) = \begin{bmatrix} -a_1 & -a_2 & \cdots & -a_{n-1} & -a_n \\ 1 & 0 & & & 0 \\ 0 & 1 & & & 0 \\ \vdots & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix} \mathbf{x}(k) + \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix} u(k)$$

$$y(k) = [b_1 \ b_2 \ \cdots \ b_n] \mathbf{x}(k)$$

- The State Feedback Law:

$$u(k) = - \begin{bmatrix} k_1 & k_2 & \cdots & k_n \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} = - \mathbf{K} \mathbf{x}(k)$$

- Then:

$$\begin{aligned} \mathbf{x}(k+1) &= \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}(-\mathbf{K}\mathbf{x}(k)) \\ &= (\mathbf{F} - \mathbf{H}\mathbf{K}) \mathbf{x}(k) \\ &= \left\{ \begin{bmatrix} -a_1 & -a_2 & \cdots & -a_{n-1} & -a_n \\ 1 & 0 & & & 0 \\ 0 & 1 & & & 0 \\ \vdots & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix} - \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix} \begin{bmatrix} k_1 & k_2 & \cdots & k_n \end{bmatrix} \right\} \mathbf{x}(k) \\ &= \begin{bmatrix} -(a_1 + k_1) & -(a_2 + k_2) & \cdots & -(a_{n-1} + k_{n-1}) & -(a_n + k_n) \\ 1 & 0 & \cdots & 0 & 0 \\ 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & 1 & 0 \end{bmatrix} \mathbf{x}(k) \end{aligned}$$

- Closed-Loop Characteristic Equation:

$$\begin{aligned} \det(\lambda \mathbf{I} - (\mathbf{F} - \mathbf{H}\mathbf{K})) \\ = \lambda^n + (a_1 + k_1)\lambda^{n-1} + \cdots + (a_n + k_n) \end{aligned}$$

- Desired Characteristic Equation:

$$\mathbf{P}(z) = \lambda^n + p_1\lambda^{n-1} + \cdots + p_n$$

- Then

$$p_i = a_i + k_i$$

$$k_i = p_i - a_i$$

$$u(k) = -\mathbf{K} \mathbf{x}(k)$$

- This is the Pole Placement

$$\mathbf{A}(z) \rightarrow \mathbf{P}(z)$$

- OR, the Eigenvalue Assignment

$$\text{eig}(\mathbf{F}) \rightarrow \text{eig}(\mathbf{F} - \mathbf{H}\mathbf{K})$$

- That is,

$$\mathbf{x}(k+1) = \begin{bmatrix} -a_1 & -a_2 & \cdots & -a_{n-1} & -a_n \\ 1 & 0 & & & 0 \\ 0 & 1 & & & \\ \vdots & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix} \mathbf{x}(k) + \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix} u(k)$$

$$u(k) = - \begin{bmatrix} k_1 & k_2 & \cdots & k_n \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}$$

$$\mathbf{x}(k+1) = \begin{bmatrix} -p_1 & -p_2 & \cdots & -p_{n-1} & -p_n \\ 1 & 0 & & & 0 \\ 0 & 1 & & & \\ \vdots & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix} \mathbf{x}(k)$$

- Now, we have (in controllable canonical form):

$$\mathbf{x}(k+1) = \begin{bmatrix} -a_1 & -a_2 & \cdots & -a_{n-1} & -a_n \\ 1 & 0 & & & 0 \\ 0 & 1 & & & \\ \vdots & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix} \mathbf{x}(k) + \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix} u(k)$$

$$\mathbf{x}_c(k+1) = \mathbf{F}_c \mathbf{x}_c(k) + \mathbf{H}_c u(k)$$

- For any other SS forms:

$$\mathbf{x}(k+1) = \mathbf{F} \mathbf{x}(k) + \mathbf{H} u(k)$$

- Assume that existing a nonsingular matrix  $\mathbf{T}$ :

$$\mathbf{x}_c(k) = \mathbf{T} \mathbf{x}(k)$$

$$\mathbf{x}(k) = \mathbf{T}^{-1} \mathbf{x}_c(k)$$



▪ Then:

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\mathbf{T}^{-1}\mathbf{x}_c(k+1) = \mathbf{F}\mathbf{T}^{-1}\mathbf{x}_c(k) + \mathbf{H}u(k)$$

$$\mathbf{x}_c(k+1) = \mathbf{T}\mathbf{F}\mathbf{T}^{-1}\mathbf{x}_c(k) + \mathbf{T}\mathbf{H}u(k)$$

$$\mathbf{x}_c(k+1) = \mathbf{F}_c\mathbf{x}_c(k) + \mathbf{H}_c u(k)$$

$$\mathbf{F}_c = \mathbf{T}\mathbf{F}\mathbf{T}^{-1}$$

$$\mathbf{H}_c = \mathbf{T}\mathbf{H}$$

$$\mathbf{x}_c(k) = \mathbf{T}\mathbf{x}(k)$$

$$\mathbf{x}(k) = \mathbf{T}^{-1}\mathbf{x}_c(k)$$

▪ If the system is “Controllable”

∃  $\mathbf{T}$ : nonsingular

such that  $\mathbf{x}_c(k) = \mathbf{T}\mathbf{x}(k)$

⇒ Controllable Canonical Form:

$$\mathbf{x}_c(k+1) = \begin{bmatrix} -a_1 & -a_2 & \cdots & -a_{n-1} & -a_n \\ 1 & 0 & & & 0 \\ 0 & 1 & & & \\ \vdots & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix} \mathbf{x}_c(k) + \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix} u(k)$$

$$y(k) = [b_1 \ b_2 \ \cdots \ b_n] \mathbf{x}_c(k)$$

$$\mathbf{x}_c(k+1) = \mathbf{F}_c\mathbf{x}_c(k) + \mathbf{H}_c u(k)$$

$$y(k) = \mathbf{C}_c\mathbf{x}_c(k)$$

$$\mathbf{F}_c = \mathbf{T}\mathbf{F}\mathbf{T}^{-1}$$

$$\mathbf{H}_c = \mathbf{T}\mathbf{H}$$

$$\mathbf{C}_c = \mathbf{C}\mathbf{T}$$

### ▪ The State Feedback Law:

$$\begin{aligned} u(k) &= -\mathbf{K}_c \mathbf{x}_c(k) \\ &= -\mathbf{K}_c \mathbf{T} \mathbf{x}(k) \\ &= -\mathbf{K} \mathbf{x}(k) \end{aligned}$$

$$\Rightarrow \mathbf{K} = \mathbf{K}_c \mathbf{T}$$

$$\mathbf{F}_c = \mathbf{T} \mathbf{F} \mathbf{T}^{-1}$$

$$\mathbf{H}_c = \mathbf{T} \mathbf{H}$$

$$\mathbf{C}_c = \mathbf{C} \mathbf{T}$$

### ▪ How to find $\mathbf{T}$ :

$$\mathbf{x}(k+1) = \mathbf{F} \mathbf{x}(k) + \mathbf{H} u(k)$$

$$\mathbf{x}_c(k+1) = \mathbf{F}_c \mathbf{x}_c(k) + \mathbf{H}_c u(k)$$

$$\mathbf{W}_c = \begin{bmatrix} \mathbf{H} & \mathbf{F} \mathbf{H} & \dots & \mathbf{F}^{n-1} \mathbf{H} \end{bmatrix}$$

$$\mathbf{W}_{cc} = \begin{bmatrix} \mathbf{H}_c & \mathbf{F}_c \mathbf{H}_c & \dots & \mathbf{F}_c^{n-1} \mathbf{H}_c \end{bmatrix}$$

$$= \begin{bmatrix} (\mathbf{T} \mathbf{H}) & (\mathbf{T} \mathbf{F} \mathbf{T}^{-1})(\mathbf{T} \mathbf{H}) & \dots & (\mathbf{T} \mathbf{F} \mathbf{T}^{-1})^{n-1} (\mathbf{T} \mathbf{H}) \end{bmatrix}$$

$$= \begin{bmatrix} (\mathbf{T} \mathbf{H}) & (\mathbf{T} \mathbf{F} \mathbf{H}) & \dots & (\mathbf{T} \mathbf{F}^{n-1} \mathbf{H}) \end{bmatrix}$$

$$= \mathbf{T} \begin{bmatrix} (\mathbf{H}) & (\mathbf{F} \mathbf{H}) & \dots & (\mathbf{F}^{n-1} \mathbf{H}) \end{bmatrix}$$

$$= \mathbf{T} \mathbf{W}_c$$

$$\mathbf{x}_c(k) = \mathbf{T} \mathbf{x}(k)$$

$$\mathbf{x}(k) = \mathbf{T}^{-1} \mathbf{x}_c(k)$$

$$\mathbf{F}_c = \mathbf{T} \mathbf{F} \mathbf{T}^{-1}$$

$$\mathbf{H}_c = \mathbf{T} \mathbf{H}$$

- If the system is “Controllable”

→  $\mathbf{W}_c$  and  $\mathbf{W}_{cc}$  are nonsingular

→  $\mathbf{T} = (\mathbf{W}_{cc}) (\mathbf{W}_c)^{-1}$

- In Summary:

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\mathbf{T} = (\mathbf{W}_{cc}) (\mathbf{W}_c)^{-1}$$

$$\mathbf{x}_c(k+1) = \mathbf{F}_c\mathbf{x}_c(k) + \mathbf{H}_c u(k)$$

$$\mathbf{F}_c = \mathbf{T}\mathbf{F}\mathbf{T}^{-1}$$

$$\mathbf{H}_c = \mathbf{T}\mathbf{H}$$

$$\mathbf{x}_c(k) = \mathbf{T} \mathbf{x}(k)$$

$$\mathbf{C}_c = \mathbf{C}\mathbf{T}$$

$$u(k) = -\mathbf{K}_c \mathbf{x}_c(k) = -\mathbf{K} \mathbf{x}(k)$$

$$\mathbf{K} = \mathbf{K}_c \mathbf{T}$$

- Ackermann's formula

- Deadbeat Control:

- IF all C.L. poles = 0, i.e.,  $P(z) = z^n$

- By Cayley-Hamilton Theorem:

$$(\mathbf{F}_{cl})^n = 0, \quad \mathbf{F}_{cl} = \mathbf{F} - \mathbf{H}\mathbf{K}$$

- $\mathbf{x}(k) = 0$  at most  $n$  steps

$$b/c: \mathbf{x}(n) = (\mathbf{F}_{cl})^n \mathbf{x}(0)$$

- $h$ : one design parameter
- $x = 0$ : at most  $n$  steps
- settling time: at most  $nh$
- $h \downarrow \Rightarrow u \uparrow$

- Example:

$$\mathbf{x}(k+1) = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \mathbf{x}(k) + \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} u(k)$$

$$\mathbf{W}_c = \left[ \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} \quad \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} \right] = \begin{bmatrix} 0.5 & 1.5 \\ 1 & 1 \end{bmatrix}$$

- **Characteristic Polynomial:**

$$\begin{aligned} \det(z\mathbf{I} - \mathbf{F}) &= \det\left(z\mathbf{I} - \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}\right) \\ &= \det\left(\begin{bmatrix} z-1 & -1 \\ 0 & z-1 \end{bmatrix}\right) \\ &= (z-1)(z-1) = z^2 - 2z + 1 \end{aligned}$$

- **Desired Characteristic Polynomial:**

$$\mathbf{P}(z) = (z - 0.2)(z - 0.5) = z^2 - 0.7z + 0.1$$

- Example:

- **Eigenvalue Assignment:**

$$\begin{aligned} \det(z\mathbf{I} - (\mathbf{F} - \mathbf{H}\mathbf{K})) &= z^2 - 0.7z + 0.1 \\ &= \det\left(z\mathbf{I} - \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} \begin{bmatrix} k_1 & k_2 \end{bmatrix}\right) \\ &= \det\left(\begin{bmatrix} z-1+0.5k_1 & -1+0.5k_2 \\ k_1 & z-1+k_2 \end{bmatrix}\right) \\ &= (z-1+0.5k_1)(z-1+k_2) - k_1(-1+0.5k_2) \\ &= z^2 + (-2+0.5k_1+k_2)z + (-1+0.5k_1)(-1+k_2) \\ &\quad - k_1(-1+0.5k_2) \\ &= z^2 - 0.7z + 0.1 \\ &\Rightarrow k_1 = 0.4, k_2 = 1.1 \end{aligned}$$

### ▪ Example:

#### ▪ Matlab code:

- $F = [ 1 \ 1; 0 \ 1 ]$
- $H = [ 0.5; 1 ]$
- $Wc = [ H \ F^*H ]$
- $\text{rank}(Wc)$
- $\text{poly}(F)$
- $\text{eig}(F)$
- $P = \text{conv}( [ 1 \ -0.5 ], [ 1 \ -0.2 ] )$
- $\text{roots}(P)$
- $K = \text{place}( F, H, \text{roots}(P) )$

### ▪ Example:

#### ▪ Matlab code:

- $Fc = [ 2 \ -1; 1 \ 0 ]$
- $Hc = [ 1; 0 ]$
- $Wcc = [ Hc \ Fc^*Hc ]$
- $\text{rank}(Wcc)$
- $\text{poly}(Fc)$
- $\text{eig}(Fc)$
- $P = \text{conv}( [ 1 \ -0.5 ], [ 1 \ -0.2 ] )$
- $\text{roots}(P)$
- $Kc = \text{place}( Fc, Hc, \text{roots}(P) )$

- Example:

- Matlab code:

- $F_{bf} = F_c - H_c K_c$
- $T = W_{cc} * W_c^{-1}$
- $T * F * T^{-1}$
- $T * H$
- $K * T^{-1}$
- $K_c * T$

$$T = (W_{cc}) (W_c)^{-1}$$

$$F_c = T F T^{-1}$$

$$H_c = T H$$

$$C_c = C T$$

$$K = K_c T$$

- Example: (Choice of Design Parameters)

- The desired DT system is obtained by sampling:

$$s^2 + 2 \zeta \omega s + \omega^2$$

$$\rightarrow P(z) = z^2 + p_1 z + p_2$$

$$\rightarrow p_1 = -2 e^{-\zeta \omega h} \cos \left( \omega h \sqrt{1 - \zeta^2} \right)$$

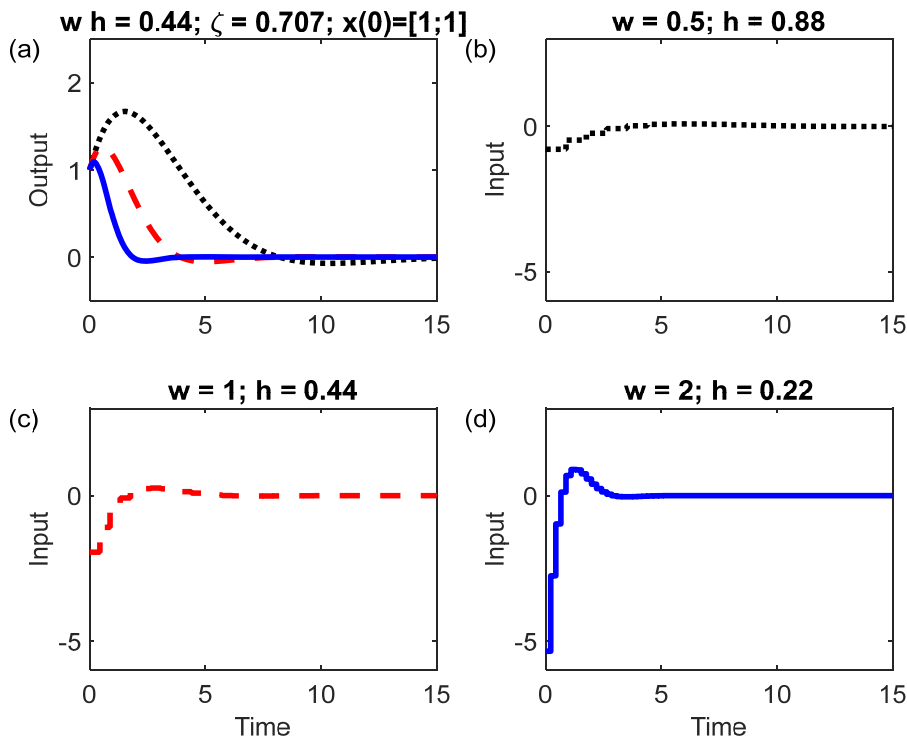
$$\rightarrow p_2 = e^{-2 \zeta \omega h}$$

$$\Rightarrow k_1 = f_1(p_1, p_2) = f(\omega, \zeta, h)$$

$$\Rightarrow k_2 = f_2(p_1, p_2) = f(\omega, \zeta, h)$$

▪ Example: (Choice of Design Parameters)

$\Rightarrow h = 0.88, 0.44, 0.22$



Observer Design

▪ D.T. Model:

$$\mathbf{x}(k + 1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$y(k) = \mathbf{C}\mathbf{x}(k)$$

$$u(k) = -\mathbf{K}\mathbf{x}(k)$$

▪ Given:

$$y(k), y(k - 1), \dots$$

$$u(k), u(k - 1), \dots$$

▪ To calculate or reconstruct:  $\mathbf{x}(k) = ?$

- Direction calculation
- Using dynamic model

- Direction calculation for  $n$  samples:  $k, k-1, \dots, k-n+1$ :

$$y(k-n+1) = \mathbf{C}\mathbf{x}(k-n+1) \quad \mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\begin{aligned} y(k-n+2) &= \mathbf{C}\mathbf{x}(k-n+2) \\ &= \mathbf{C} [ \mathbf{F}\mathbf{x}(k-n+1) + \mathbf{H}u(k-n+1) ] \\ &= \mathbf{C}\mathbf{F}\mathbf{x}(k-n+1) + \mathbf{C}\mathbf{H}u(k-n+1) \end{aligned}$$

$$\begin{aligned} y(k-n+3) &= \mathbf{C}\mathbf{x}(k-n+3) \\ &= \mathbf{C} \{ \mathbf{F}\mathbf{x}(k-n+2) + \mathbf{H}u(k-n+2) \} \\ &= \mathbf{C} \{ \mathbf{F} [ \mathbf{F}\mathbf{x}(k-n+1) + \mathbf{H}u(k-n+1) ] + \mathbf{H}u(k-n+2) \} \\ &= \mathbf{C}\mathbf{F}^2\mathbf{x}(k-n+1) + \mathbf{C}\mathbf{F}\mathbf{H}u(k-n+1) + \mathbf{C}\mathbf{H}u(k-n+2) \\ y(k) &= \mathbf{C}\mathbf{F}^{n-1}\mathbf{x}(k-n+1) + \mathbf{C}\mathbf{F}^{n-2}\mathbf{H}u(k-n+1) \\ &\quad + \dots + \mathbf{C}\mathbf{H}u(k-1) \end{aligned}$$

$$\begin{bmatrix} y(k-n+1) \\ y(k-n+2) \\ \vdots \\ y(k) \end{bmatrix} = \begin{bmatrix} \mathbf{C} \\ \mathbf{C}\mathbf{F} \\ \vdots \\ \mathbf{C}\mathbf{F}^{n-1} \end{bmatrix} \mathbf{x}(k-n+1) + \begin{bmatrix} 0 & 0 & \dots & 0 \\ \mathbf{C}\mathbf{H} & 0 & \dots & 0 \\ \mathbf{C}\mathbf{F}\mathbf{H} & \mathbf{C}\mathbf{H} & & 0 \\ \vdots & & & \\ \mathbf{C}\mathbf{F}^{n-2}\mathbf{H} & \mathbf{C}\mathbf{F}^{n-3}\mathbf{H} & & 0 \end{bmatrix} \begin{bmatrix} u(k-n+1) \\ u(k-n+2) \\ \vdots \\ u(k-1) \end{bmatrix}$$

$$\Rightarrow \mathbf{Y}_k = \mathbf{W}_o \mathbf{x}(k-n+1) + \mathbf{W}_u \mathbf{U}_{k-1}$$

$$\Rightarrow \mathbf{x}(k-n+1) = \mathbf{W}_o^{-1} \mathbf{Y}_k - \mathbf{W}_o^{-1} \mathbf{W}_u \mathbf{U}_{k-1}$$



▪ From state-state form:

$$\mathbf{x}(k) = \mathbf{F}^{n-1}\mathbf{x}(k-n+1) + \mathbf{F}^{n-2}\mathbf{H}u(k-n+1) + \dots + \mathbf{H}u(k-1)$$

$$\Rightarrow \mathbf{x}(k-n+1) = \mathbf{W}_o^{-1}\mathbf{Y}_k - \mathbf{W}_o^{-1}\mathbf{W}_u\mathbf{U}_{k-1}$$

$$\mathbf{x}(k) = \mathbf{F}^{n-1}\mathbf{W}_o^{-1}\mathbf{Y}_k - \mathbf{F}^{n-1}\mathbf{W}_o^{-1}\mathbf{W}_u\mathbf{U}_{k-1}$$

$$+ \left[ \mathbf{F}^{n-2}\mathbf{H} \quad \mathbf{F}^{n-3}\mathbf{H} \quad \dots \quad \mathbf{H} \right] \begin{bmatrix} u(k-n+1) \\ u(k-n+2) \\ \vdots \\ u(k-1) \end{bmatrix}$$

$$\Rightarrow \mathbf{x}(k) = \mathbf{A}_y \mathbf{Y}_k + \mathbf{B}_u \mathbf{U}_{k-1}$$

$$\mathbf{A}_y = \mathbf{F}^{n-1}\mathbf{W}_o^{-1}$$

$$\mathbf{B}_u = \left[ \mathbf{F}^{n-2}\mathbf{H} \quad \mathbf{F}^{n-3}\mathbf{H} \quad \dots \quad \mathbf{H} \right] - \mathbf{F}^{n-1}\mathbf{W}_o^{-1}\mathbf{W}_u$$

▪ Estimation using dynamic model:

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\hat{\mathbf{x}}(k+1) = \mathbf{F}\hat{\mathbf{x}}(k) + \mathbf{H}u(k)$$

• If  $\hat{\mathbf{x}}(0) = \mathbf{x}(0) \Rightarrow \hat{\mathbf{x}}(k) = \mathbf{x}(k)$

• If  $\hat{\mathbf{x}}(0) \neq \mathbf{x}(0) \Rightarrow \hat{\mathbf{x}}(k) \rightarrow \mathbf{x}(k)$

only if asymptotically stable

- Improvement by using measured outputs:

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\begin{aligned} \hat{\mathbf{x}}(k+1|k) &= \mathbf{F}\hat{\mathbf{x}}(k|k-1) + \mathbf{H}u(k) \\ &\quad + \mathbf{L} [ y(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1) ] \end{aligned}$$

- Estimation error:

$$\tilde{\mathbf{x}} = \mathbf{x} - \hat{\mathbf{x}}$$

$$\begin{aligned} \tilde{\mathbf{x}}(k+1|k) &= \mathbf{F}\tilde{\mathbf{x}}(k|k-1) \\ &\quad - \mathbf{L} [ \mathbf{C}\mathbf{x}(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1) ] \\ &\quad - \mathbf{L}\mathbf{C} [ \mathbf{x}(k) - \hat{\mathbf{x}}(k|k-1) ] \\ &\quad - \mathbf{L}\mathbf{C}\tilde{\mathbf{x}}(k|k-1) \\ &= [ \mathbf{F} - \mathbf{L}\mathbf{C} ] \tilde{\mathbf{x}}(k|k-1) \end{aligned}$$

- Hence,

- If  $\mathbf{L}$  is chosen such that the system is asymptotic stable

$$\begin{aligned} \Rightarrow \tilde{\mathbf{x}} &\rightarrow 0 \\ \Rightarrow \mathbf{x} &\rightarrow \hat{\mathbf{x}} \end{aligned} \quad \tilde{\mathbf{x}}(k+1|k) = [ \mathbf{F} - \mathbf{L}\mathbf{C} ] \tilde{\mathbf{x}}(k|k-1)$$

- That is,

- Given  $\mathbf{F}$  and  $\mathbf{C}$
- To find  $\mathbf{L}$

$\Rightarrow \mathbf{F} - \mathbf{L}\mathbf{C}$  has prescribed eigenvalues

- In Summary: Observer Dynamics

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$y(k) = \mathbf{C}\mathbf{x}(k)$$

- If the system is completely observable

$\exists \mathbf{L}$  such that  $\mathbf{F} - \mathbf{L}\mathbf{C}$  of

$$\begin{aligned} \hat{\mathbf{x}}(k+1|k) = & \mathbf{F}\hat{\mathbf{x}}(k|k-1) + \mathbf{H}u(k) \\ & + \mathbf{L} [ y(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1) ] \end{aligned}$$

has the following desired char. poly.

$$P(z) = z^n + p_1z^{n-1} + \dots + p_n$$

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$y(k) = \mathbf{C}\mathbf{x}(k)$$

- If the system is “Controllable”

$$\mathbf{W}_c = \begin{bmatrix} \mathbf{H} & \mathbf{F}\mathbf{H} & \dots & \mathbf{F}^{n-1}\mathbf{H} \end{bmatrix} \quad \text{is nonsingular}$$

$$\rightarrow u(k) = -\mathbf{K}\mathbf{x}(k)$$

$$\rightarrow \text{Desired eigenvalues: } \text{eig}(\mathbf{F} - \mathbf{H}\mathbf{K})$$

- If the system is “Observable”

$$\mathbf{W}_o = \begin{bmatrix} \mathbf{C} \\ \mathbf{C}\mathbf{F} \\ \vdots \\ \mathbf{C}\mathbf{F}^{n-1} \end{bmatrix} \quad \text{is nonsingular}$$

$$\rightarrow \mathbf{L} [ y(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1) ]$$

$$\rightarrow \text{Desired eigenvalues: } \text{eig}(\mathbf{F} - \mathbf{L}\mathbf{C})$$

### ▪ Deadbeat Observer:

- Choose  $\mathbf{L}$ , such that  $\text{eig}(\mathbf{F} - \mathbf{LC}) = 0$
- $\tilde{\mathbf{x}}(k) = 0$  at most  $n$  steps
- It is equivalent to the **direct calculation!**

### ▪ D.T. Model:

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$y(k) = \mathbf{C}\mathbf{x}(k)$$

### ▪ If all states are measured directly:

$$u(k) = -\mathbf{K}\mathbf{x}(k) \quad \text{gives desired C.L. poles}$$

### ▪ If the states **CANNOT** measured:

$$\hat{\mathbf{x}}(k|k-1) = \mathbf{F}\hat{\mathbf{x}}(k-1|k-2) + \mathbf{H}u(k-1)$$

$$+ \mathbf{L} [ y(k-1) - \mathbf{C}\hat{\mathbf{x}}(k-1|k-2) ]$$

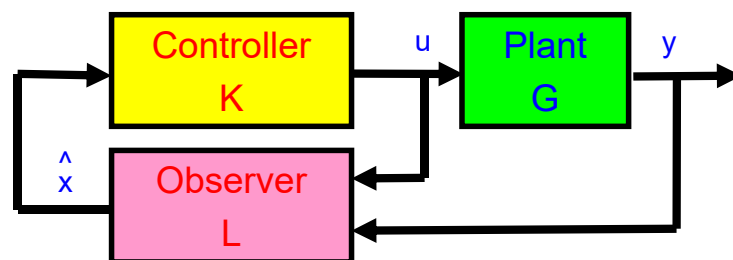
$$u(k) = -\mathbf{K}\hat{\mathbf{x}}(k|k-1)$$

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$y(k) = \mathbf{C}\mathbf{x}(k)$$

$$\hat{\mathbf{x}}(k|k-1) = \mathbf{F}\hat{\mathbf{x}}(k-1|k-2) + \mathbf{H}u(k-1) \\ + \mathbf{L} [ y(k-1) - \mathbf{C}\hat{\mathbf{x}}(k-1|k-2) ]$$

$$u(k) = -\mathbf{K}\hat{\mathbf{x}}(k|k-1)$$



### ▪ Closed-Loop System:

$$\tilde{\mathbf{x}} = \mathbf{x} - \hat{\mathbf{x}}$$

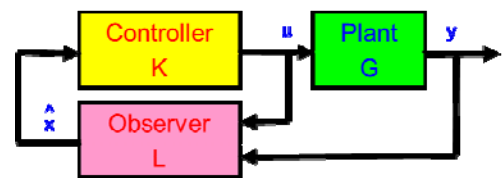
$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$\hat{\mathbf{x}}(k+1|k) = \mathbf{F}\hat{\mathbf{x}}(k|k-1) + \mathbf{H}u(k) \\ + \mathbf{L} [ y(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1) ]$$

$$u(k) = -\mathbf{K}\hat{\mathbf{x}}(k|k-1)$$

$$\tilde{\mathbf{x}}(k+1|k) = \mathbf{F}\tilde{\mathbf{x}}(k|k-1) \\ - \mathbf{L} [ \mathbf{C}\mathbf{x}(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1) ] \\ = [ \mathbf{F} - \mathbf{L}\mathbf{C} ] \tilde{\mathbf{x}}(k|k-1)$$

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) - \mathbf{H}\mathbf{K}\hat{\mathbf{x}}(k|k-1)$$



$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) - \mathbf{H}\mathbf{K}\hat{\mathbf{x}}(k|k-1)$$

$$\tilde{\mathbf{x}} = \mathbf{x} - \hat{\mathbf{x}}$$

$$= \mathbf{F}\mathbf{x}(k) - \mathbf{H}\mathbf{K}(\mathbf{x}(k) - \tilde{\mathbf{x}}(k|k-1))$$

$$= [\mathbf{F} - \mathbf{H}\mathbf{K}]\mathbf{x}(k) + \mathbf{H}\mathbf{K}\tilde{\mathbf{x}}(k|k-1)$$

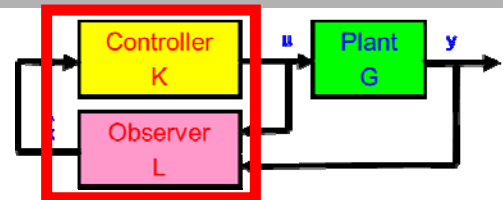
$$\tilde{\mathbf{x}}(k+1|k) = [\mathbf{F} - \mathbf{L}\mathbf{C}]\tilde{\mathbf{x}}(k|k-1)$$

⇒ system order of  $2n$

⇒ eig( C.L. system ) =

eig(  $\mathbf{F} - \mathbf{H}\mathbf{K}$  ) & eig(  $\mathbf{F} - \mathbf{L}\mathbf{C}$  )

$$u(k) = -\mathbf{K}\hat{\mathbf{x}}(k|k-1)$$



$$\hat{\mathbf{x}}(k+1|k) = \mathbf{F}\hat{\mathbf{x}}(k|k-1) + \mathbf{H}u(k)$$

$$+ \mathbf{L}[y(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1)]$$

$$= \mathbf{F}\hat{\mathbf{x}}(k|k-1) - \mathbf{H}\mathbf{K}\hat{\mathbf{x}}(k|k-1)$$

$$+ \mathbf{L}[y(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1)]$$

$$= [\mathbf{F} - \mathbf{H}\mathbf{K} - \mathbf{L}\mathbf{C}]\hat{\mathbf{x}}(k|k-1)$$

$$+ \mathbf{L}y(k)$$

→ eig(  $\mathbf{F} - \mathbf{H}\mathbf{K} - \mathbf{L}\mathbf{C}$  )

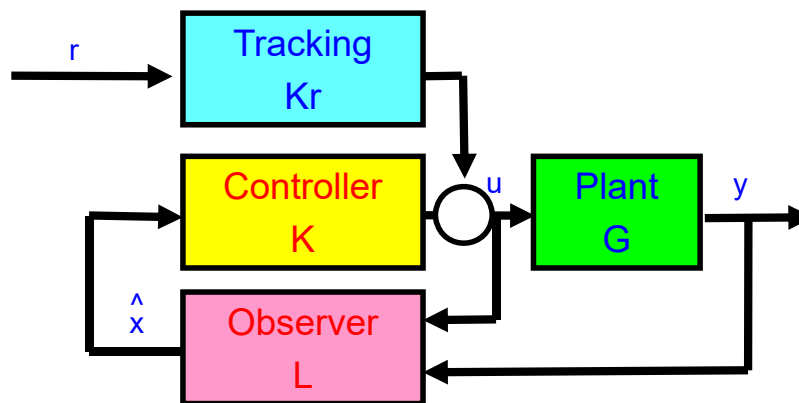
- Objective of Tracking Problem:

- Make the **states** and the **outputs** of the system respond to **command signals** in a specific way

- Regulation & Tracking:

- **Regulation:**  $u(k) = -\mathbf{K} \hat{\mathbf{x}}(k)$

- **Tracking:**  $u(k) = -\mathbf{K} \hat{\mathbf{x}}(k) + \mathbf{K}_r r(k)$



- Plant, Observer & Controller Models:

$$\mathbf{x}(k+1) = \mathbf{F}\mathbf{x}(k) + \mathbf{H}u(k)$$

$$y(k) = \mathbf{C}\mathbf{x}(k)$$

$$\hat{\mathbf{x}}(k+1|k) = \mathbf{F}\hat{\mathbf{x}}(k|k-1) + \mathbf{H}u(k)$$

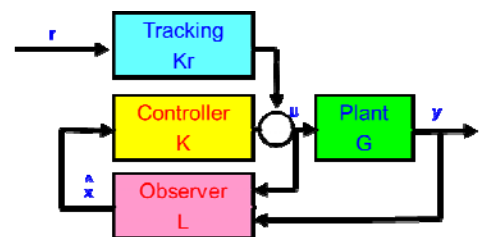
$$+ \mathbf{L} [ y(k) - \mathbf{C}\hat{\mathbf{x}}(k|k-1) ]$$

$$u(k) = -\mathbf{K} \hat{\mathbf{x}}(k) + \mathbf{K}_r r(k)$$

$$\tilde{\mathbf{x}} = \mathbf{x} - \hat{\mathbf{x}} \quad \hat{\mathbf{x}} = \mathbf{x} - \tilde{\mathbf{x}}$$

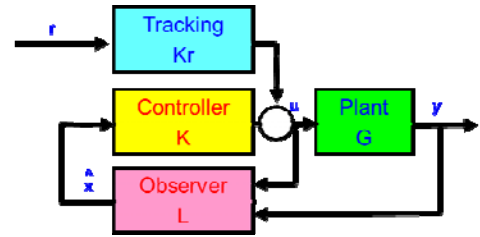
$$u(k) = -\mathbf{K} \mathbf{x} + \mathbf{K} \tilde{\mathbf{x}} + \mathbf{K}_r r(k)$$

$$\begin{aligned} \mathbf{x}(k+1) &= \mathbf{F}\mathbf{x}(k) - \mathbf{H}\mathbf{K} \mathbf{x}(k) + \mathbf{H}\mathbf{K} \tilde{\mathbf{x}} + \mathbf{H}\mathbf{K}_r r(k) \\ &= [ \mathbf{F} - \mathbf{H}\mathbf{K} ] \mathbf{x}(k) + \mathbf{H}\mathbf{K} \tilde{\mathbf{x}} + \mathbf{H}\mathbf{K}_r r(k) \end{aligned}$$



Plant, Observer & Controller Models:

$$u(k) = -\mathbf{K} \hat{\mathbf{x}}(k) + \mathbf{K}_r r(k)$$



$$\mathbf{x}(k+1) = [\mathbf{F} - \mathbf{H}\mathbf{K}] \mathbf{x}(k) + \mathbf{H}\mathbf{K} \tilde{\mathbf{x}} + \mathbf{H}\mathbf{K}_r r(k)$$

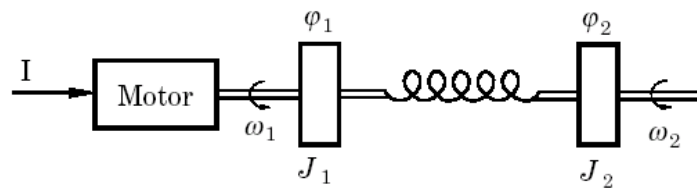
$$y(k) = \mathbf{C}\mathbf{x}(k)$$

$$\tilde{\mathbf{x}}(k+1|k) = [\mathbf{F} - \mathbf{L}\mathbf{C}] \tilde{\mathbf{x}}(k|k-1)$$

$$\hat{\mathbf{x}}(k+1|k) = [\mathbf{F} - \mathbf{H}\mathbf{K} - \mathbf{L}\mathbf{C}] \hat{\mathbf{x}}(k|k-1) + \mathbf{L} y(k) + \mathbf{H}\mathbf{K}_r r(k)$$

Design Example

A Flexible Robot Arm:



- States:

$$x_1 = \phi_1 - \phi_2$$

$$x_2 = \omega_1 / \omega_0$$

$$x_3 = \omega_2 / \omega_0$$

wehre  $\omega_0 = \sqrt{k(J_1 + J_2)/(J_1 J_2)}$



- C.T. Model of a Flexible Robot Arm:

$$\frac{dx}{dt} = w_0 \begin{bmatrix} 0 & 1 & -1 \\ \alpha - 1 & -\beta_1 & \beta_1 \\ \alpha & \beta_2 & -\beta_2 \end{bmatrix} x + \begin{bmatrix} 0 \\ \gamma \\ 0 \end{bmatrix} u + \begin{bmatrix} 0 \\ \delta \\ 0 \end{bmatrix} v$$

$$y = \begin{bmatrix} 0 & 0 & w_0 \end{bmatrix} x$$

$$\text{wehre } \begin{cases} \alpha & = J_1/(J_1 + J_2) \\ \beta_1 & = d/J_1 w_0 \\ \beta_2 & = d/J_2 w_0 \\ \gamma & = k_I/J_1 w_0 \\ \delta & = 1/J_1 w_0 \end{cases}$$

- Numerical Values used in simulation:

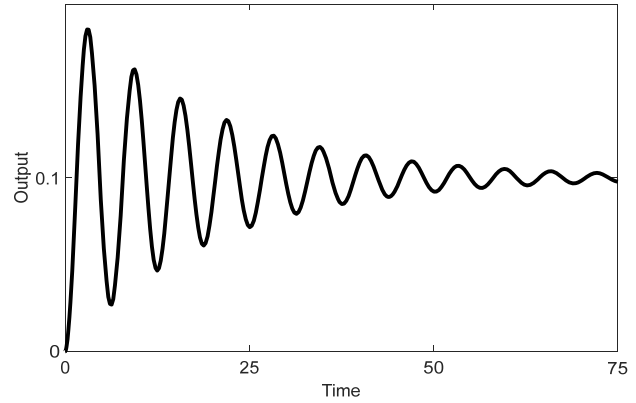
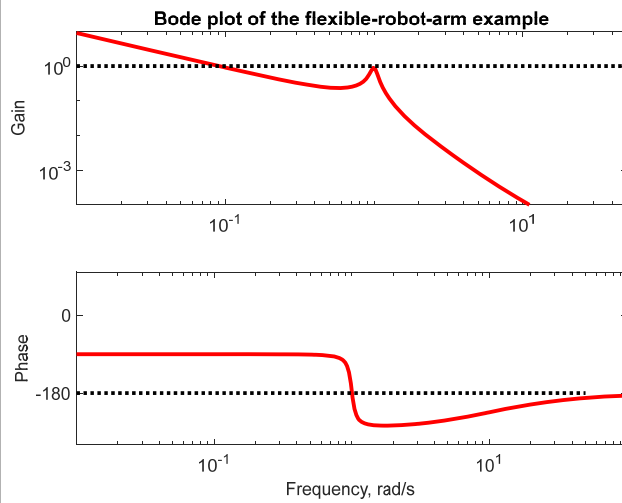
$$\begin{cases} J_1 & = 10/9 \\ J_2 & = 10 \\ k & = 1 \\ d & = 0.1 \\ k_I & = 1 \\ w_0 & = 1 \end{cases}$$

- Poles & Zeros:

$$\begin{cases} \text{Zeros: } & z_1 = -10 \\ \text{Poles: } & p_1 = 0, p_{23} = -0.05 \pm 0.999i \end{cases}$$

⇒ a pure integrator,  $\zeta_p = 0.05$ ,  $w_p = 1$  rad/s

## ■ Bode plot & impulse response:



## ■ Specifications:

- $\zeta_m = 0.7$ ,  $w_m = 0.5$  rad/s

## ■ Sampling Time:

- $wh = 0.1 - 0.6$ 
  - $\Rightarrow h = 0.5$  s
  - $\Rightarrow w_N = \pi/h = 6$  rad/s

▪ State Feedback Design:

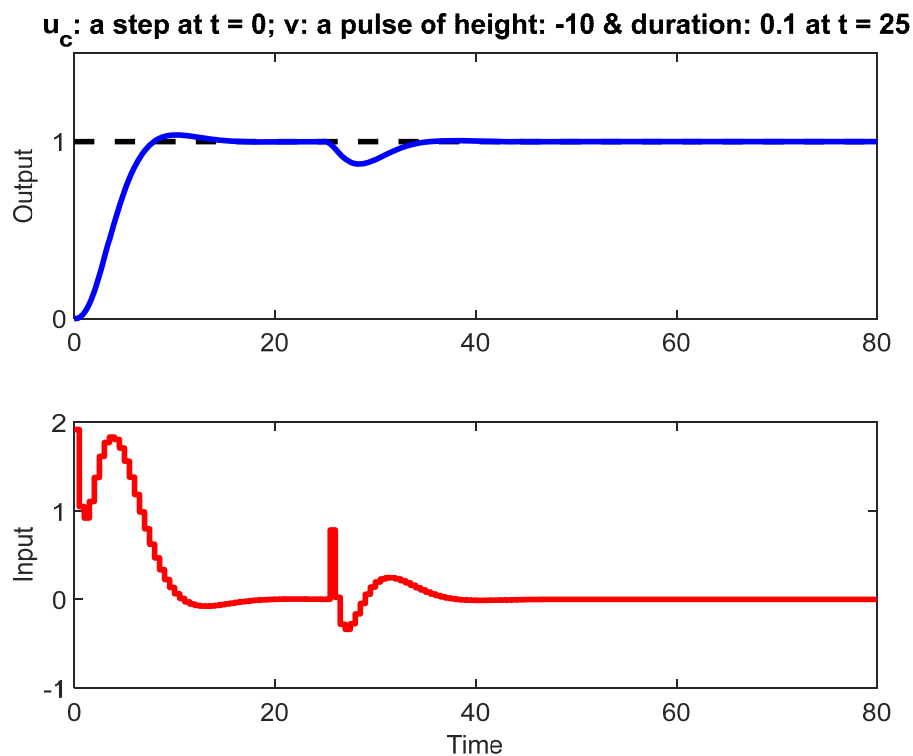
- $u(k) = -\mathbf{K}\mathbf{x}(k) + \mathbf{K}_c u_c(k)$

▪ Desired Poles:

- $(s^2 + 2\zeta_m w_m s + w_m^2)(s + \alpha_1 w_m) = 0$

⇒ Sampled form with  $h = 0.5$  s

⇒  $\alpha_1 = 2$



■ Observer Design:

- $\text{eig}(F - LC)$ : similar to C.L. Poles
- $(s^2 + 2\zeta_m\alpha_0\omega_ms + (\alpha_0\omega_m)^2)(s + \alpha_0\alpha_1\omega_m) = 0$

$\Rightarrow \alpha_0$  farther away from the origin

$\Rightarrow \alpha_0 = 2, \alpha_1 = 2$

