

Fall 2021 (110-1)

控制系統  
Control Systems

Unit 6G  
Bode's Gain-Phase Relationship

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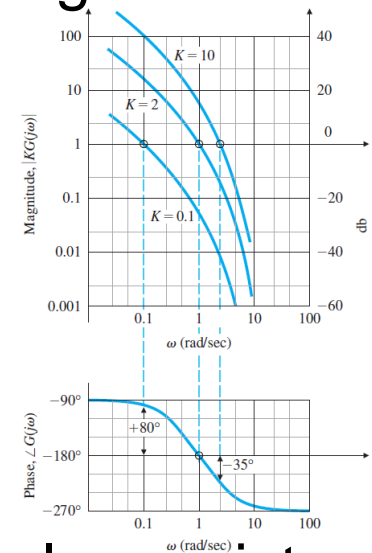
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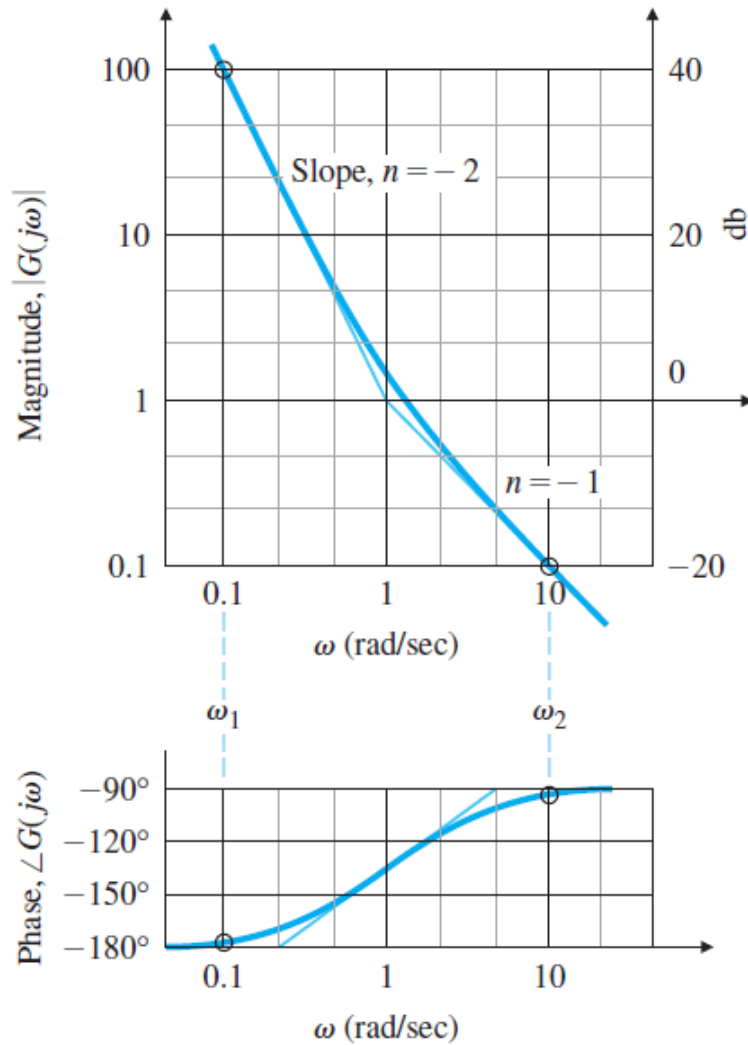
Sep 2021 – Jan 2022

- One of **Bode's important contributions** is the following theorem:
- For any **stable minimum-phase** system (no RHP zeros/poles),
- The **phase** of  $G(j\omega)$  is uniquely related to the **magnitude** of  $G(j\omega)$
- When the **slope** of  $|G(j\omega)|$  versus  $\omega$  on a log-log scale persists at a **constant value** for approximately **a decade of frequency**, the relationship is particularly simple and is given by:

$$\angle G(j\omega) \approx n \times 90^\circ$$

- $n$ : the **slope** of  $|G(j\omega)|$  in units of decade of amplitude **per decade** of frequency





## ■ Slope:

- At  $\omega_1 = 0.1$ ,  $(n = -2)$
- At  $\omega_2 = 10$ ,  $(n = -1)$

## ■ Phase:

- At  $\omega_1 = 0.1$ ,  $-180^\circ$
- At  $\omega_2 = 10$ ,  $-90^\circ$

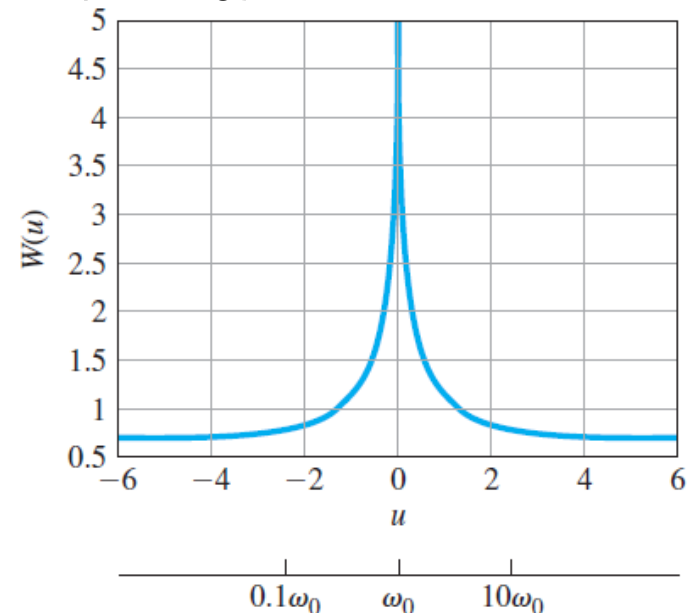
- An exact statement of **the Bode Gain-Phase Theorem** is:

$$\angle G(j\omega) = \frac{1}{\pi} \int_{-\infty}^{+\infty} \left( \frac{dM}{du} \right) W(u) du \quad \text{in radians}$$

- Where

- $M$  = log magnitude =  $\ln |G(j\omega)|$
- $u$  = normalized frequency =  $\ln(\omega / \omega_0)$
- $dM/du \sim$  slope  $n$
- $W(u)$  = weighting function  
=  $\ln(\coth|u|/2)$

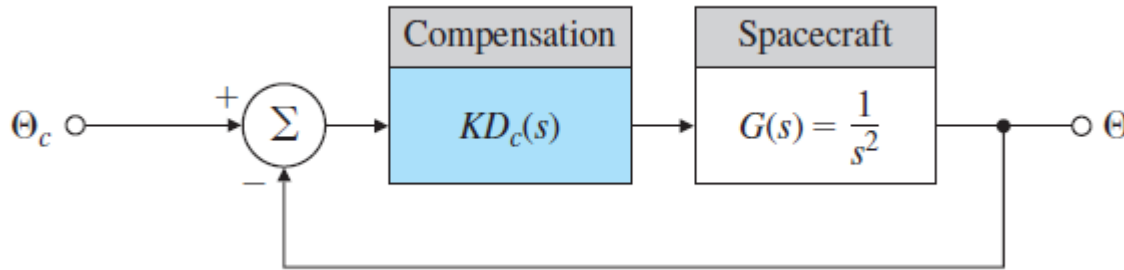
$$W(u) \approx \frac{\pi^2}{2} \delta(u)$$



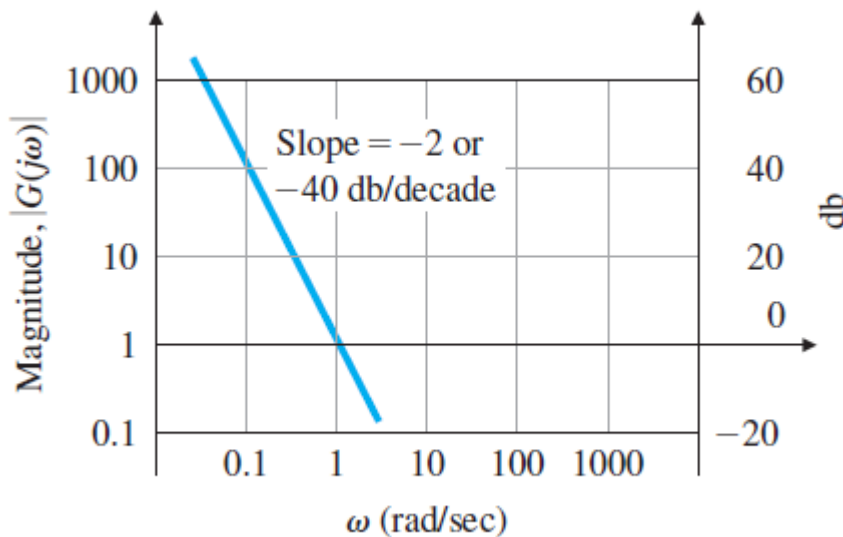
- But, usually use  $\angle G(j\omega) \approx n \times 90^\circ$
- When  $|KG(j\omega)| = 1$ 
  - $\angle G(j\omega) \approx -90^\circ$  if  $n = -1$
  - $\angle G(j\omega) \approx -180^\circ$  if  $n = -2$
- For **stability**, we want:
  - $\angle G(j\omega) > -180^\circ$  for **PM** to be  $> 0$
- Therefore, **adjust the  $|KG(j\omega)|$  curve**
- So that it has a **slope of  $-1$**  at the **crossover frequency  $\omega_c$**
- If the **slope =  $-1$**  for a decade above/below  $\omega_c$ , then **PM  $\approx 90^\circ$**
- However, to ensure **a reasonable PM**,  
it is usually necessary only to insist that  
**a  $-1$  slope** persist for a decade in frequency centered **at  $\omega_c$**

- A very **simple design criterion**:
- Adjust the **slope** of the **magnitude curve**  $|KG(j\omega)|$
- So that it crosses over **magnitude 1** with **a slope of -1**  
for a decade **around**  $\omega_c$
- This criterion will usually be sufficient  
to provide **an acceptable PM** and **adequate system damping**.
- To achieve the desired **speed of response**,
- the **system gain** is adjusted
- so that the **crossover point** is at a frequency  
that will yield the **desired bandwidth** or **speed of response**.
- **Natural Freq**  $\omega_n \sim$  **Bandwidth**  $\omega_{BW} \sim$  **Crossover Freq**  $\omega_c$

## Example 6.14: Use of Simple Design Criterion for Spacecraft Attitude Control



$$K D_c(s) = K ( T_D s + 1 )$$

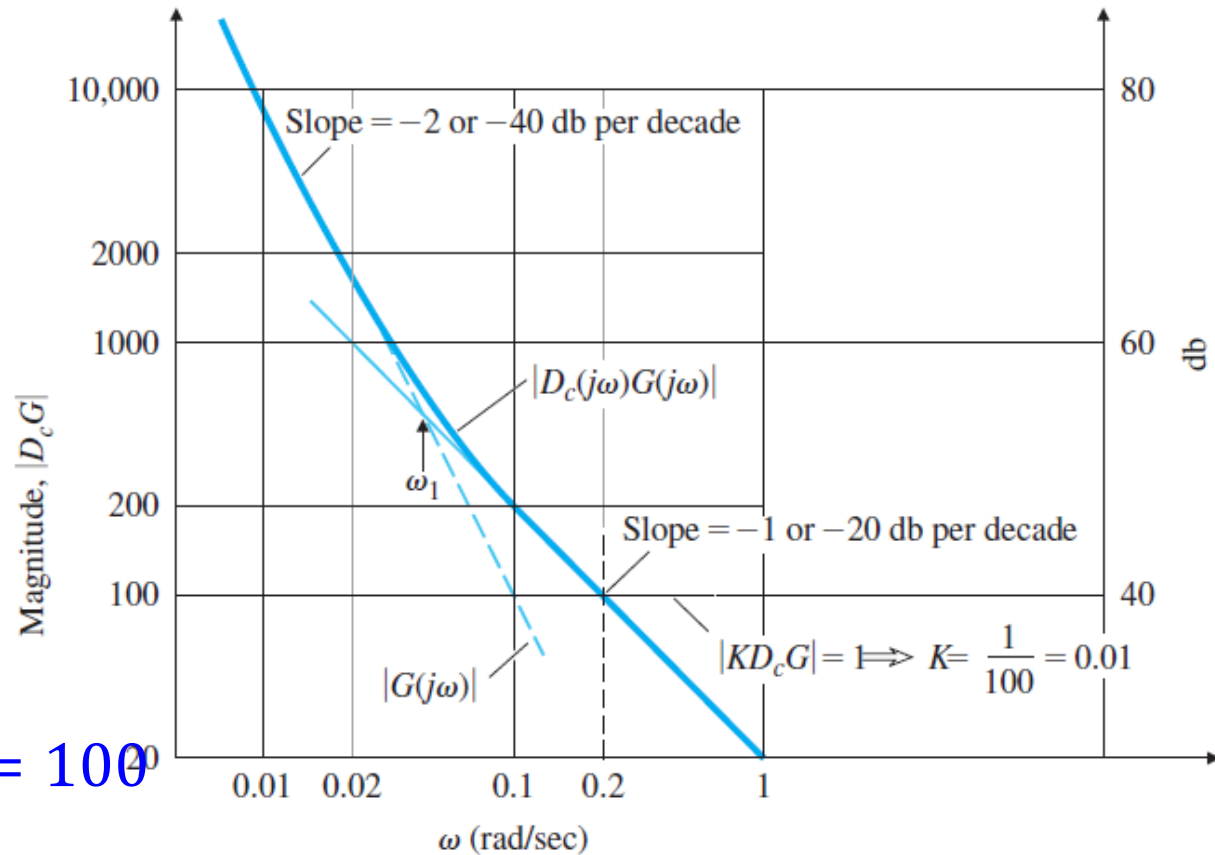


- Adjust  $K$
- to provide desired bandwidth
- Adjust break point  $\omega_1 = 1/T_D$
- to provide the -1 slope at the crossover frequency

**0.2 rad/sec**

# Example

1. Plot  $|G(j\omega)|$
2. Modify the plot to include  $|D_c(j\omega)|$  with  $\omega_1 = 0.05$   
 $T_D = 20$   
 $\rightarrow$  slope=-1 at 0.2

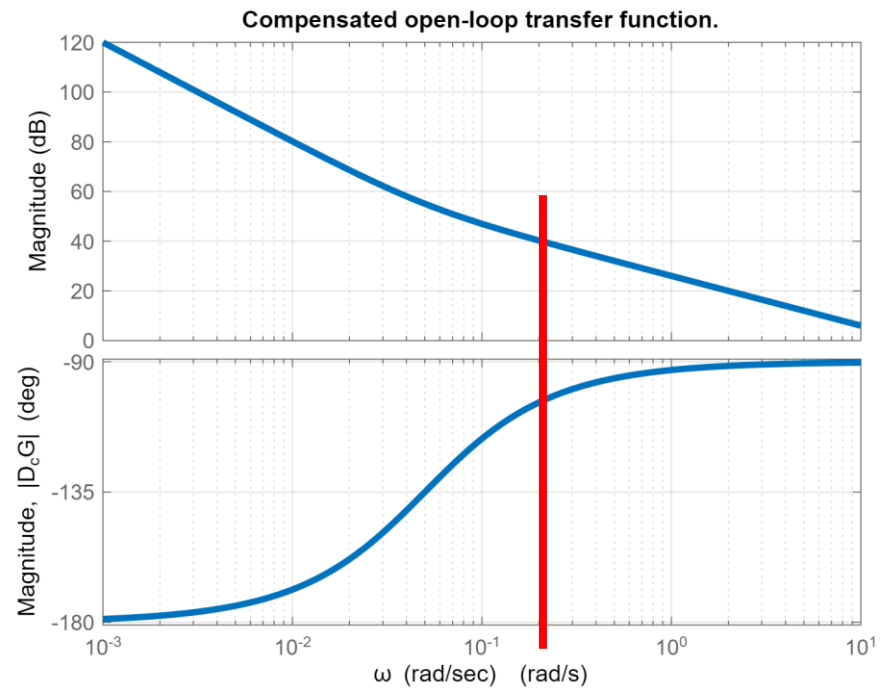
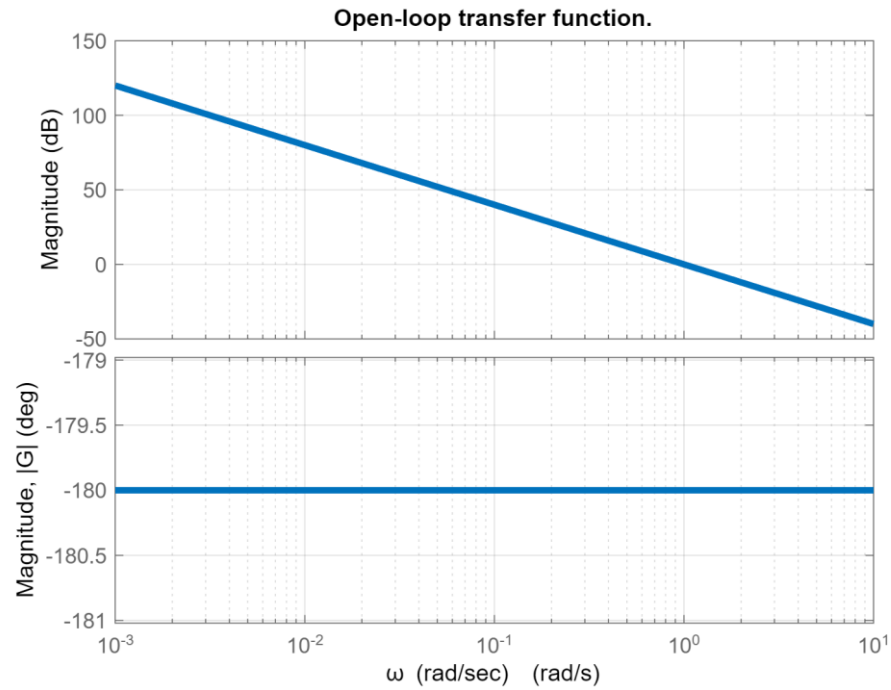


3. Determine  $|D_c G| = 100$  where the  $|D_c G|$  curve crosses the line  $\omega = 0.2$

4. Compute 
$$K = \frac{1}{|D_c G|_{\omega=0.2}} = \frac{1}{100} = 0.01$$

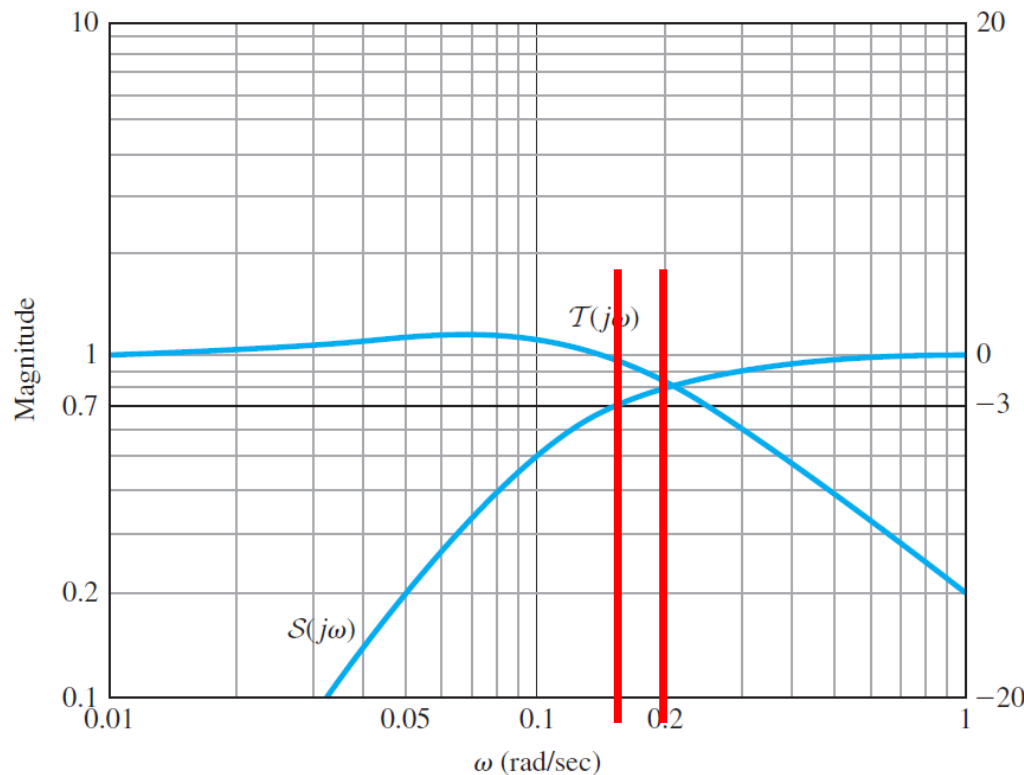
$$\Rightarrow K D_c(s) = 0.01 (20s + 1)$$





# Example

- The closed-loop frequency-response magnitude  $T(j\omega)$  and the sensitivity function  $S(j\omega)$
- Desired Bandwidth = 0.2 rad/sec
- Disturbance Rejection (-3db) at 0.15 rad/sec



- Overshoot = 14%

