

Fall 2021 (110-1)

控制系統
Control Systems

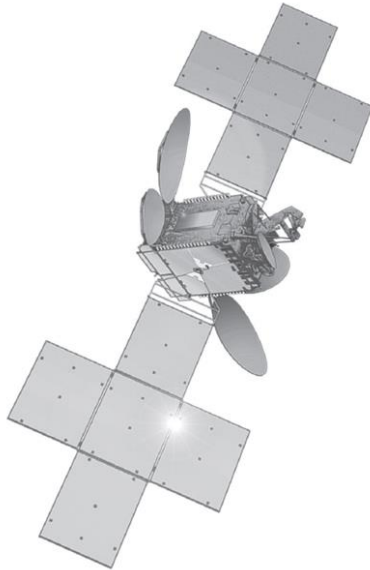
Unit 2B
Mechanical Systems – Rotational Motion

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NTU-EE

Sep 2021 – Jan 2022

- Communication satellite



Source: Courtesy Thaicom PLC and Space Systems/Loral

- The purpose is to control the **attitude** of the satellite, such as
 - ✓ **Antennas** point toward earth
 - ✓ **Solar panels** orient toward the sun

■ Model (Equations of Motion: Rotational motion)

$$M = I \alpha$$

- M ($N \cdot m^2$): the sum of all external moments about the center of mass,
- I ($Kg \cdot m^2$): the body's mass moment of inertia about its center of mass,
- α (rad/sec^2): the angular acceleration of the body

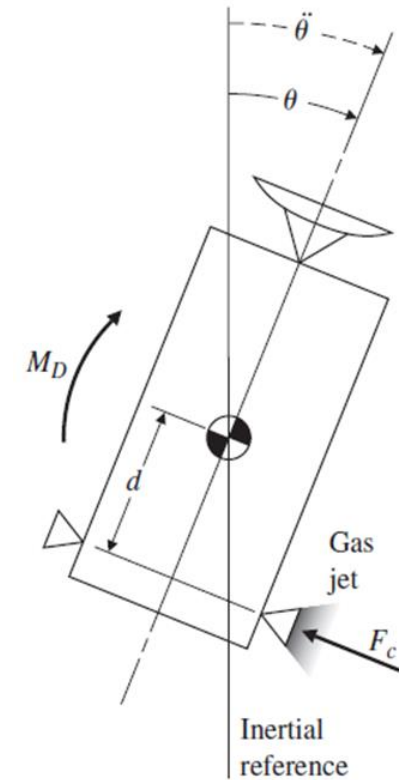
Example 2.3 (Rotational motion): Satellite Attitude Control Model

■ Model (Equations of Motion)

- Three axes, consider one axis at a time

$$F_c \cdot d + M_D = I \cdot \ddot{\theta}$$

- $F_c \cdot d$: Moments of control force
- M_D : Moments of small disturbance



■ Transfer Function

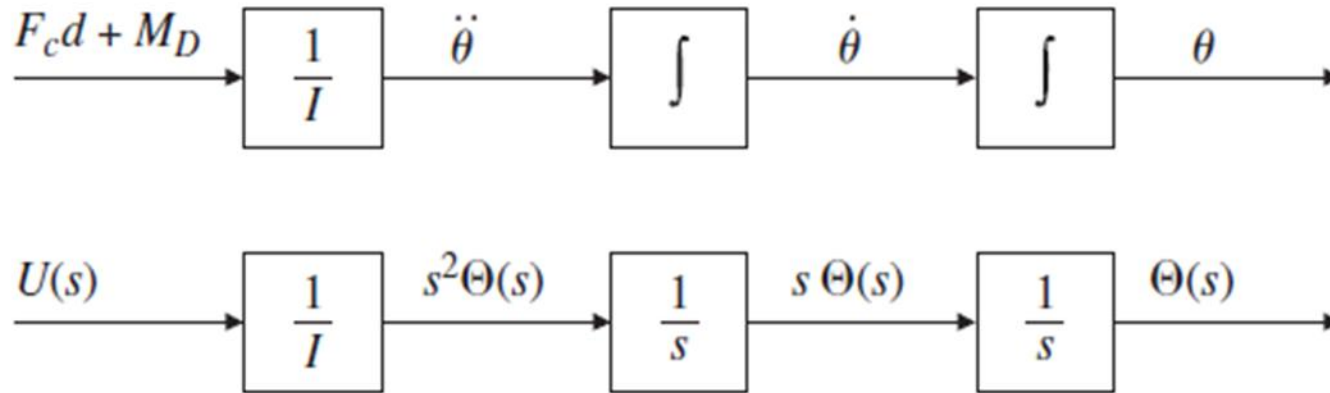
- Let $F_c \cdot d + M_D = u$

$$\frac{\Theta(s)}{U(s)} = \frac{1}{I} \cdot \frac{1}{s^2} \quad (\text{Double-Integrator plant})$$

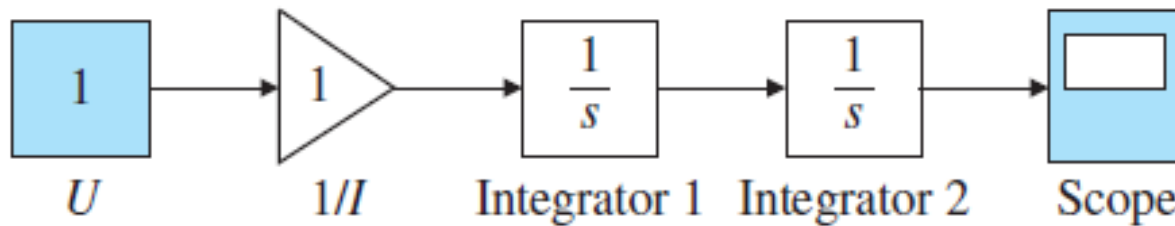
Example 2.3 (Rotational motion): Satellite Attitude Control Model

▪ Block diagram

$$\frac{\Theta(s)}{U(s)} = \frac{1}{I} \cdot \frac{1}{s^2} \quad (\text{Double-Integrator plant})$$

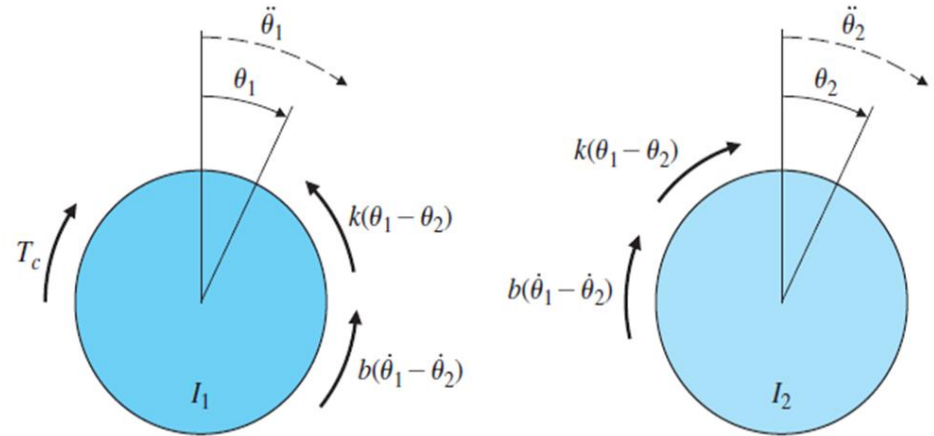
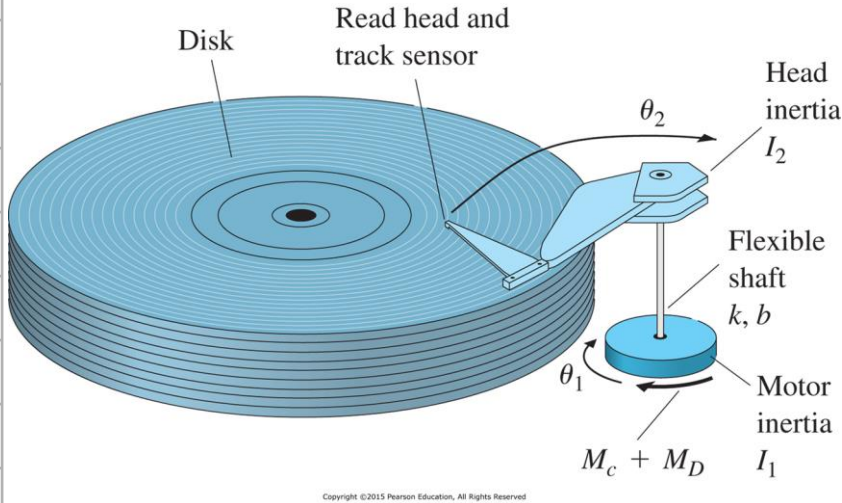


▪ Simulink



- Disk Read/Write Head

- The moment of each body: free body diagram



- Model (Equations of Motion: Rotational motion)

$$I_1 \ddot{\theta}_1 + b(\dot{\theta}_1 - \dot{\theta}_2) + k(\theta_1 - \theta_2) = M_c + M_D$$

$$I_2 \ddot{\theta}_2 + b(\dot{\theta}_2 - \dot{\theta}_1) + k(\theta_2 - \theta_1) = 0$$

- M_c : Moments of applied control
- M_D : Moments of small disturbance

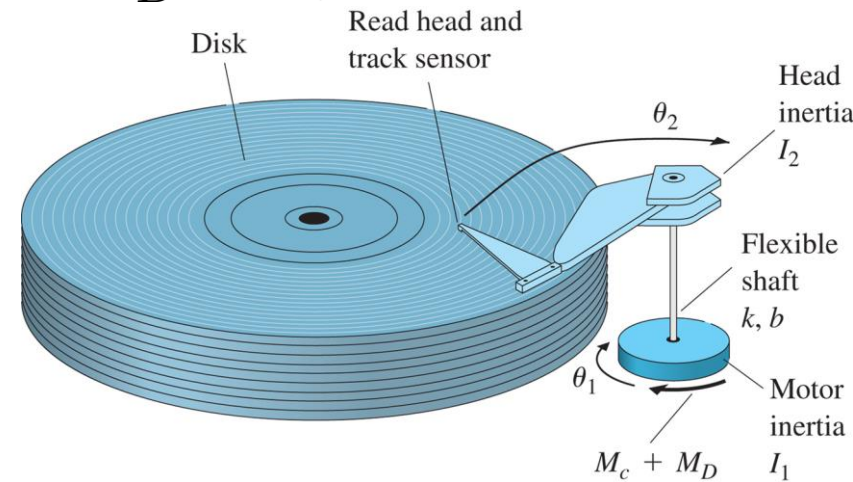
Example 2.4 Flexible Read/Write for a Disk Drive

Model (Equations of Motion)

- Simplify the model, consider the case $M_D = 0, b = 0$

$$I_1 \ddot{\theta}_1 + k(\theta_1 - \theta_2) = M_c$$

$$I_2 \ddot{\theta}_2 + k(\theta_2 - \theta_1) = 0$$



Transfer Function

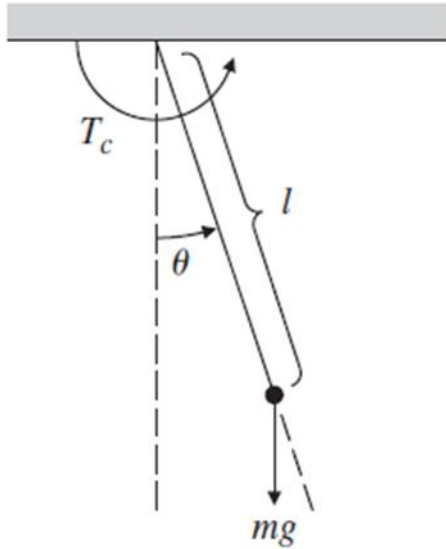
$$\frac{\Theta_2(s)}{M_c(s)} = \frac{k}{I_1 I_2 s^2 \left(s^2 + \frac{k}{I_1} + \frac{k}{I_2} \right)}$$

$$\frac{\Theta_1(s)}{M_c(s)} = \frac{I_2 s^2 + k}{I_1 I_2 s^2 \left(s^2 + \frac{k}{I_1} + \frac{k}{I_2} \right)}$$

- “**Noncollocated case**”: there is **flexibility** between the sensor and the actuator

- “**Collocated case**”: the sensor and the actuator are **rigidly attached** to one another

- Pendulum



- Model (Equations of Motion)

$$T_c - mgl \sin \theta = I \ddot{\theta}$$

- The moments of inertia about the pivot point is

$$I = ml^2$$

$$\ddot{\theta} + \frac{g}{l} \sin \theta = \frac{T_c}{ml^2}$$

- The model is nonlinear due to $\sin \theta$
- When the motion is small, i.e., θ small, $\sin \theta \approx \theta$

$$\ddot{\theta} + \frac{g}{l} \theta = \frac{T_c}{ml^2} \quad \text{(Linearization model)}$$

Example 2.5 Pendulum

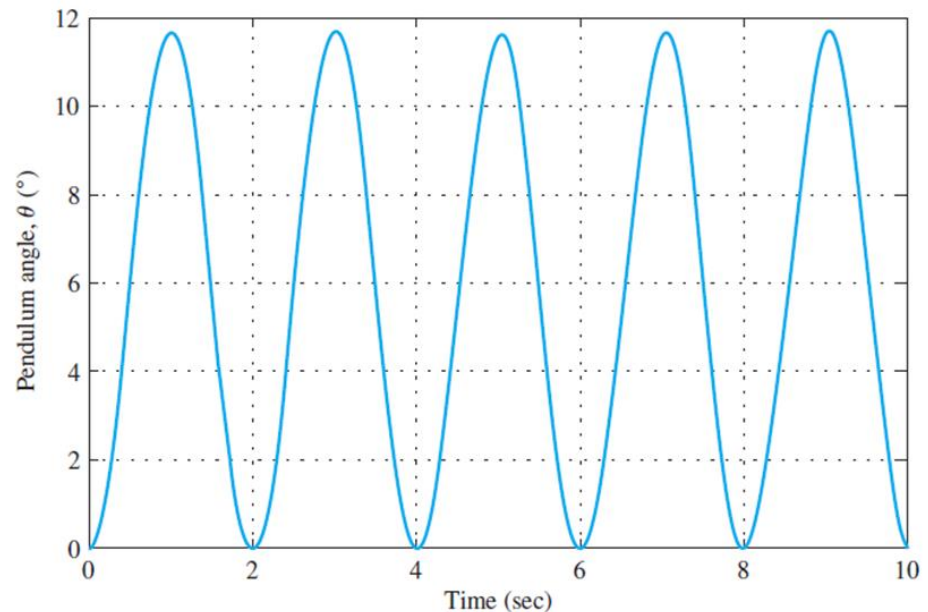
Transfer Function

$$\frac{\Theta(s)}{T_c(s)} = \frac{\frac{1}{ml^2}}{s^2 + \frac{g}{l}}$$

Matlab code

- `t = 0:0.02:10;`
- `m = 1; L = 1; g = 9.81;`
- `s = tf('s');`
- `sys = (1/(m*L^2))/(s^2+g/L) ;`
- `y1 = step(sys, t);`
- `y2 = impulse(sys, t);`

- `Rad2Deg = 57.3;`
- `Plot(t, Rad2Deg*y1)`
- `Plot(t, Rad2Deg*y2)`

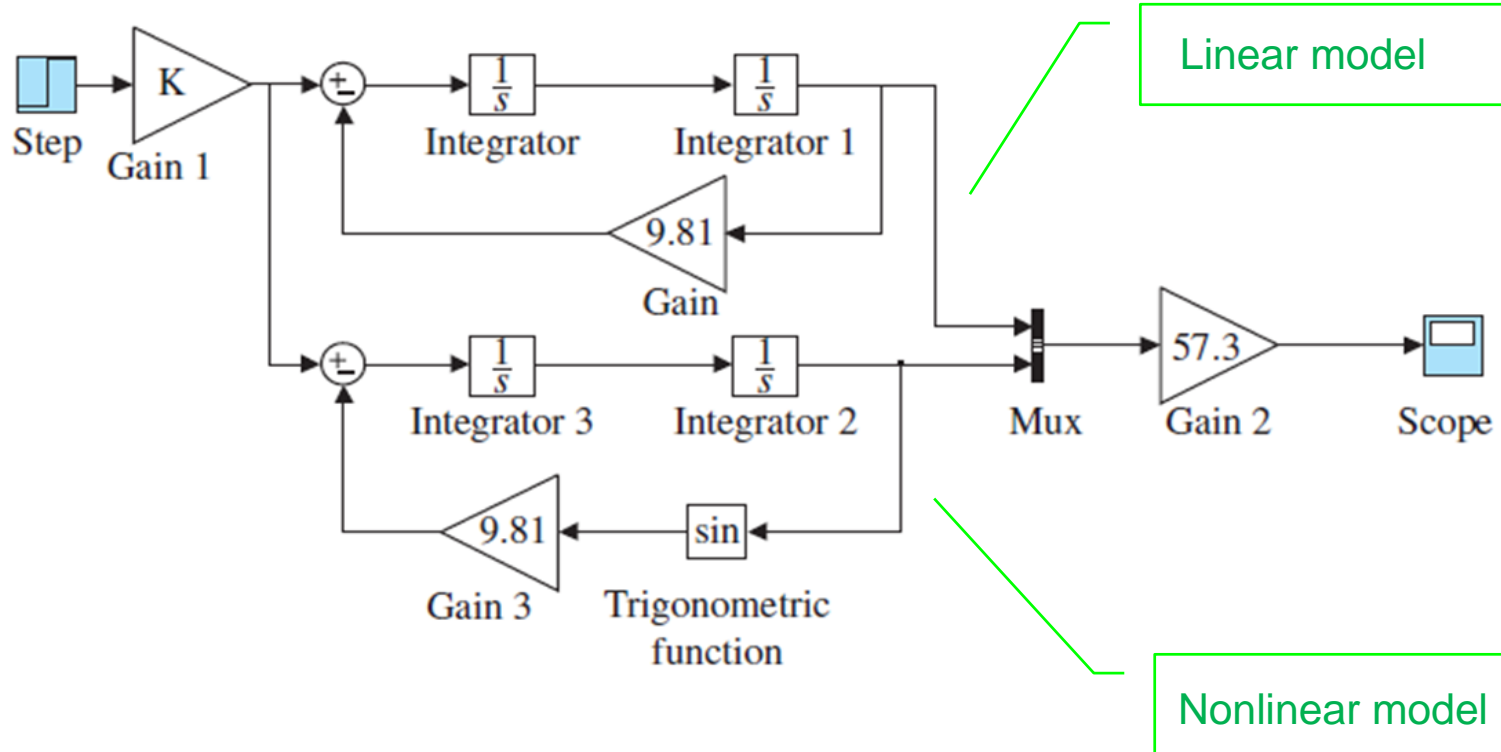


`%converts output from radians to degrees`
`%converts output from radians to degrees`

Example 2.6 Pendulum (Simulink for nonlinear motion)

- Matlab Simulink (m=1; L=1; g=9.81)

$$\ddot{\theta} + \frac{g}{l}\theta = \frac{T_c}{ml^2}$$



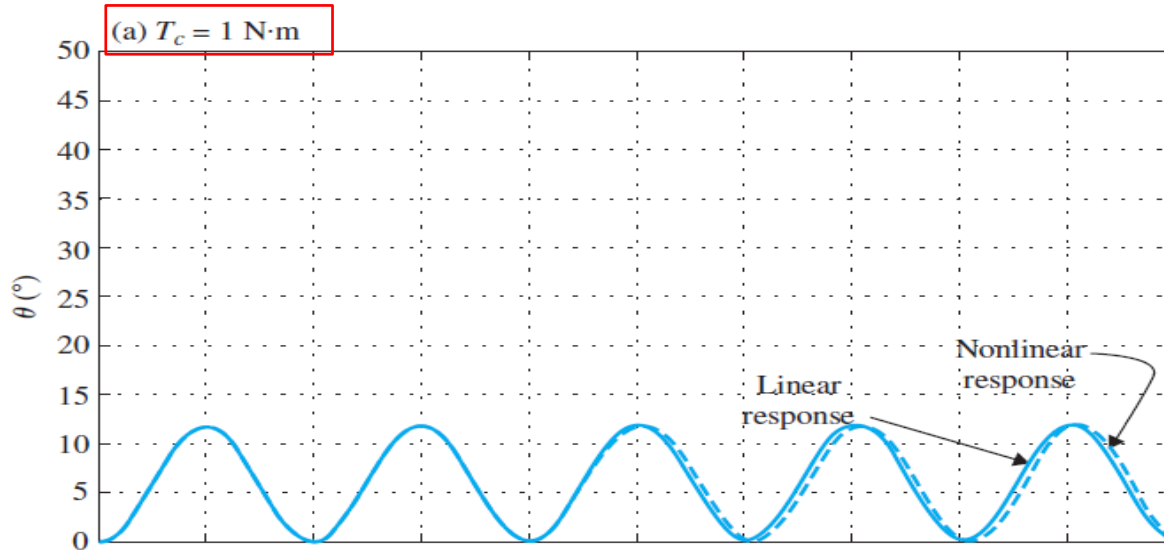
$$\ddot{\theta} + \frac{g}{l}\sin\theta = \frac{T_c}{ml^2}$$

Example 2.6 Pendulum (Simulink for nonlinear motion)

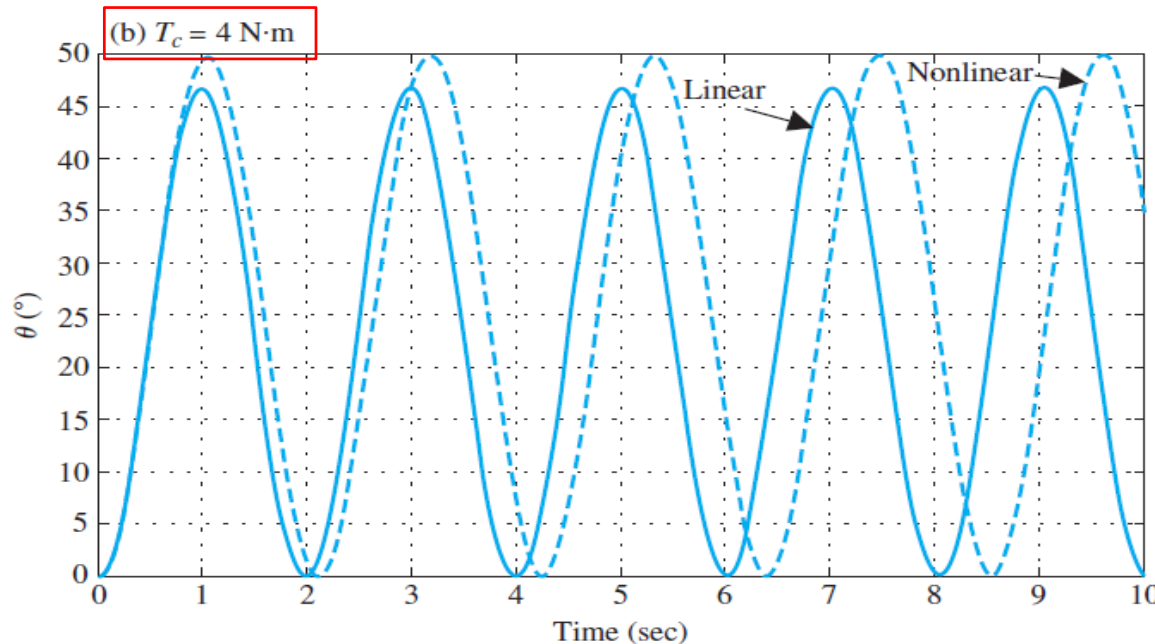
Comparisons of linear & nonlinear responses

$$\ddot{\theta} + \frac{g}{l} \sin \theta = \frac{T_c}{ml^2}$$

$$\ddot{\theta} + \frac{g}{l} \theta = \frac{T_c}{ml^2}$$



- When $T_c=1$, the output θ remains **small**, thus the approximation is **still good** ($\sin \theta \approx \theta$)



- When $T_c=4$, the output θ becomes **large**, thus the approximation is **not good** ($\sin \theta \approx \theta$ does not hold)