Spring 2021

控制系統 Control Systems

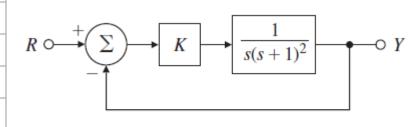
Unit 6F Stability Margins

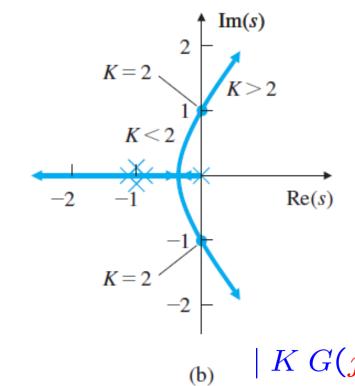
Feng-Li Lian NTU-EE Feb – Jun, 2021

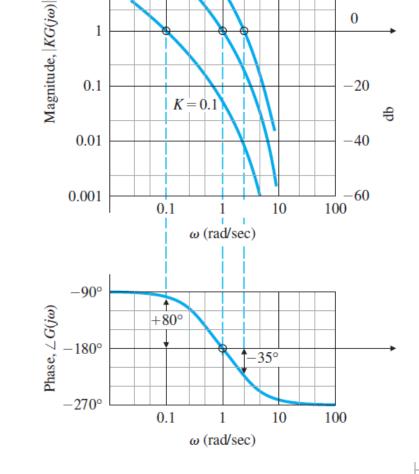
40

20

### In U6D







K = 10

K=2

100

10

|K G(jw)| < 1  $\angle G(jw) = -180^{\circ}$ 

40

- Gain Margin (GM) & Phase Margin (PM) 100
  - Another measure of stability,
     originally defined by Smith (1958)
  - Combine the two margins into

# Vector Margin / Complex Margin

$$\angle G(jw) = -180^{\circ}$$

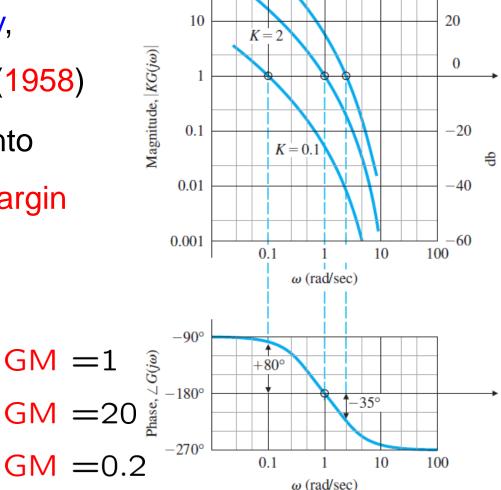
$$|KG(jw)| = 1$$

$$|\Pi \cup (jw)| -$$

$$\Rightarrow K=2 \quad |KG(jw)|=1$$

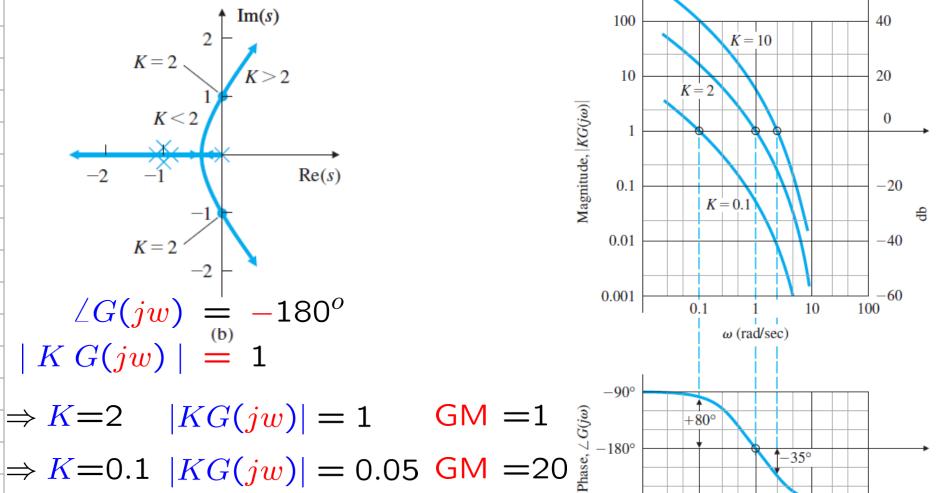
$$\Rightarrow K=0.1 |KG(jw)| = 0.05 \text{ GM} = 20 \frac{1}{8}$$

$$\Rightarrow K=10 |KG(jw)| = 5 GM = 0.2$$



K = 10

Unstable



$$\Rightarrow K=10 |KG(jw)| = 5 \text{ GM } = 0.2$$

$$T(s) = \frac{Y(s)}{R(s)} = \frac{KG(s)}{1 + KG(s)} \text{ Unstable}$$

-270°

0.1

10

 $\omega$  (rad/sec)

100

40

20

0

-20

-40



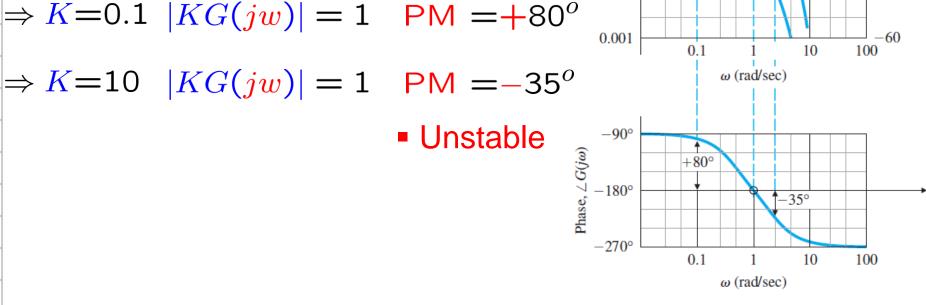
$$|KG(jw)| = 1$$

$$\Rightarrow \angle G(jw) = ?$$
 • Exceeds  $-180^{o}$   $\sqrt[o]{9}$   $\sqrt[o]{9}$ 

$$\Rightarrow K=2 \quad |KG(jw)| = 1 \quad PM = 0^{\circ}$$

$$\Rightarrow K=10 |KG(jw)| = 1 PM = -35^{\circ}$$

### Unstable



K = 10

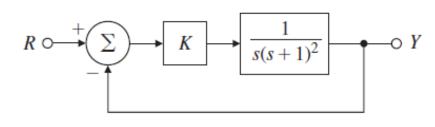
K=2

K = 0.1

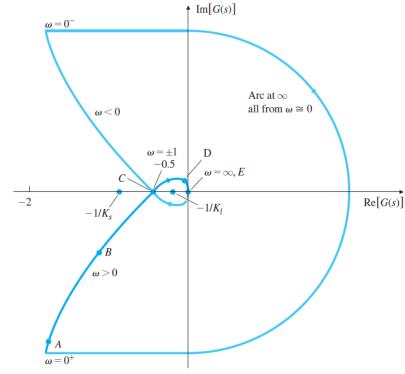
0.1

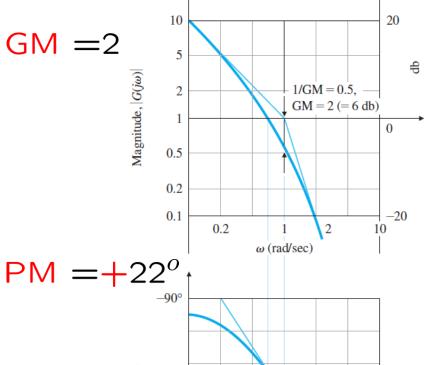
0.01

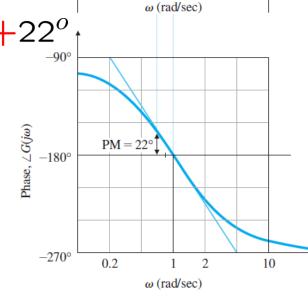
## In Example 6.9:



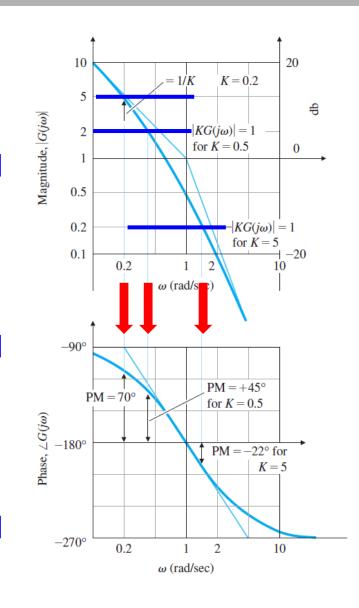
### Nyquist Plot

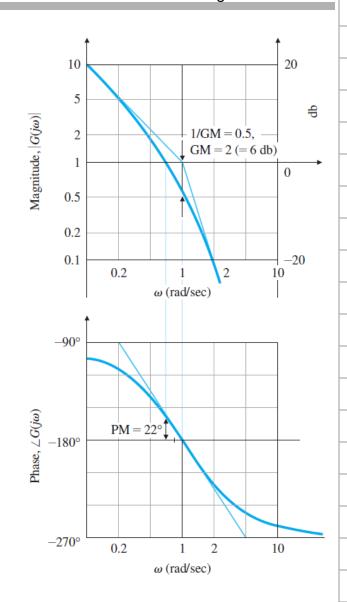






- PM vs K
- K = 5
- | KG(jw) | = 1
- $PM = -22^{o}$
- K = 0.5
- | KG(jw) | = 1
- PM = +45°
- K = 0.2
- | KG(jw) | = 1
- $PM = +70^{\circ}$





The PM is more commonly used to specify control system performance

because it is more closely to the damping ratio of the system.

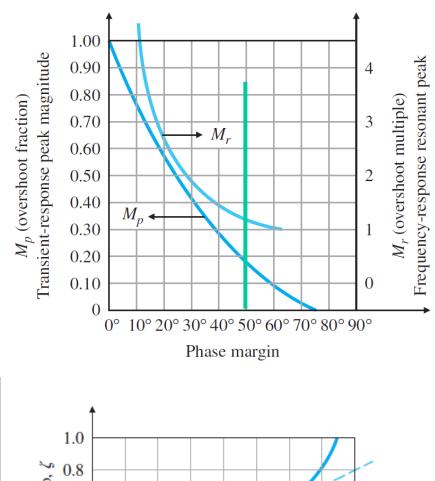
- For the open-loop 2nd-order system:  $G(s) = \frac{w_n^2}{s (s + 2 \zeta w_n)}$
- With unity feedback, produces the closed-loop system:

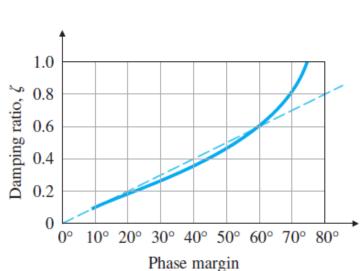
 $\mathcal{T}(s) = \frac{w_n^2}{s^2 + 2 \zeta w_n s + w_n^2}$ 

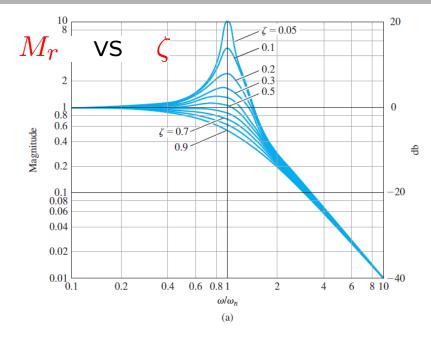
$$PM = tan^{-1} \left[ \frac{2\zeta}{\sqrt{\sqrt{1 + 4\zeta^4} - 2\zeta^2}} \right]$$

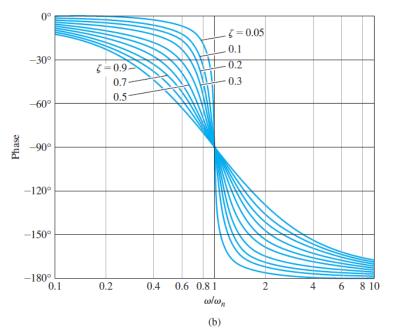
$$\frac{\mathsf{M}}{\mathsf{O}}$$
 for  $\mathsf{PM} < 60^{o}$ 







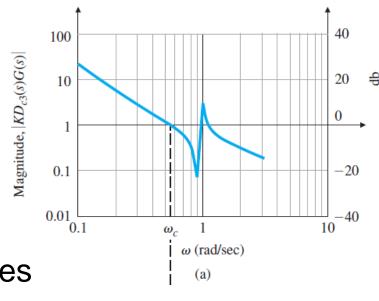


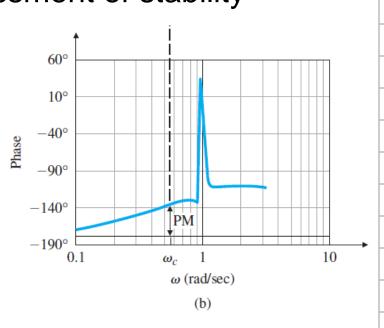


- In some cases,
  - the PM and GM are not useful indicators of stability.
  - For 1st- and 2nd-order systems,
     the phase never crosses the 180° line;
- Hence, the GM is always ∞ and not a useful design parameter.
- For higher-order systems,
- it is possible to have more than one frequency where |KG(jw)| = 1 or where  $\angle KG(jw) = 180^{\circ}$
- And the margins as previously defined need clarification.
- An example as follows:

- In Chapter 10
- The magnitude crosses 1 three times
- Define PM by the first crossing
- Because the PM at this crossing
   was the smallest of these 3 values

and thus the most conservative assessment of stability





- Vector Margin (or Complex Margin)
- The distance to the -1 point

from the closet approach of the Nyquist Plot

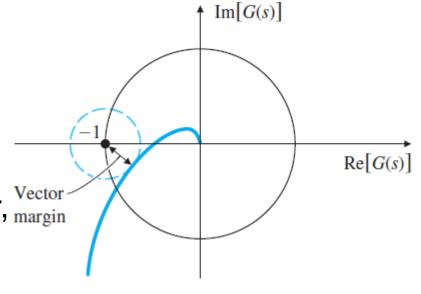
Vector margin is

a single margin parameter, vector margin

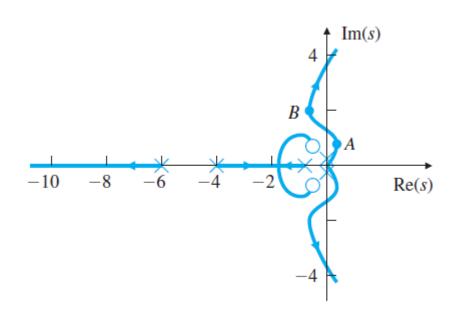
It removes all the ambiguities

in assessing stability

that come with using GM and PM in combination.



- Conditionally Stable Systems
- Point A:
- Increase gain
  - → make stable
- Point B:
- Increase/decrease gain
  - → make unstable



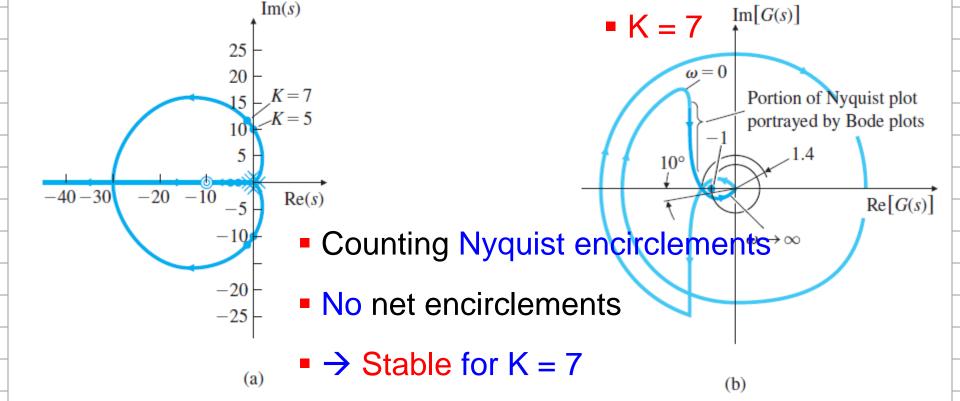
- Example 6.12: Stabili
  - Example 6.12: Stability Properties

$$K(s+10)^2$$
 for a Co

$$KG(s) = \frac{K(s+10)^2}{s^3}$$

- Unstable: K < 5
- Stable: K > 5

- for a Conditionally Stable System
  - Conflicting !!!
    - PM =  $+10^{\circ}$  (Stable)
    - GM = 0.6 (Unstable)





0.1

-20

-40

GM = 1.26

with Multiple Crossover Frequencies

$$G(s) = \frac{85 (s+1) (s^2 + 2s + 43.25)}{s^2 (s^2 + 2s + 82) (s^2 + 2s + 101)}$$

$$= \frac{85 (s+1) (s+1 \pm 6.5j)}{s^2 (s+1 \pm 9j) (s+1 \pm 10j)}$$

3 crossover frequencies 0.01 0.001 0.0001

